

City of Lemon Grove City Council Regular Meeting Agenda Tuesday, February 18, 2020, 6:00 p.m.

Lemon Grove Community Center 3146 School Lane, Lemon Grove, CA

The City Council also sits as the Lemon Grove Housing Authority, Lemon Grove Sanitation District Board, Lemon Grove Roadway Lighting District Board, and Lemon Grove Successor Agency

Call to Order

Pledge of Allegiance:

Changes to the Agenda:

Public Comment:

(Note: In accordance with State Law, the general public may bring forward an item not scheduled on the agenda; however, the City Council may not take any action at this meeting. If appropriate, the item will be referred to staff or placed on a future agenda.)

City Council Oral Comments and Reports on Meetings Attended at the Expense of the City. (GC 53232.3 (d)) (53232.3 (d)) states that members of a legislative body shall provide brief reports on meetings attended at the expense of the local agency at the next regular meeting of the legislative body.)

City Manager Report:

1. Consent Calendar:

(Note: The items listed on the Consent Calendar will be enacted in one motion unless removed from the Consent Calendar by Council, staff, or the public.)

A. Waive Full Text Reading of All Ordinances on the Agenda

Reference: Kristen Steinke, City Attorney

Recommendation: Waive the full text reading of all ordinances included in this

agenda; Ordinances shall be introduced and adopted by

title only.

B. City of Lemon Grove Payment Demands

Reference: Rod Greek, Interim Finance Manager

Recommendation: Ratify Demands

C. Approval of Meeting Minutes

Regular Meeting February 4, 2020

Reference: Shelley Chapel, City Clerk Recommendation: Approve Minutes D. Accept FY 2017-2018 Sewer CIP Project as Complete (Sanitation District Item)

Reference: Mike James, Assistant City Manager / Public Works Director Recommendation: Adopt Resolution entitled, "A Resolution of the Lemon Grove Sanitation District, California, Accepting the Fiscal Year 2017-18 Sewer Capital Improvement Project (Contract No. 2019-11) as Complete."

Continued Public Hearing:

2. Continuation of Public Hearing to Consider Conditional Use Permit Application CUP-190-0002, A Request to Establish a Medical Marijuana Dispensary at 3515-3521 Harris Street in Special Treatment Area III, Regional Commercial.

Reference: Noah Alvey, Community Development Manager Recommendation: Continue the Public Hearing for consideration of CUP-190-0002, direct staff to re-notice the public hearing based on actions by the San Diego Superior Court, and provide that no new sensitive uses shall prejudice the application.

Reports to Council:

3. Acceptance of the Drainage Master Plan Update Final Report

Reference: Mike James, Assistant City Manager / Public Works Director Recommendation: That the City Council adopt a resolution accepting the Drainage Master Plan Update.

4. Lemon Grove Homelessness Partnership Plan

Reference: Mike James, Assistant City Manager / Public Works Director Recommendation: Receive report and direction to staff regarding the Lemon Grove Homelessness Partnership Plan.

5. FY 2019-2020 Mid-Year Budget

Reference: Rod Greek, Interim Finance Manager

Recommendation:

- Adopt a resolution approving the Fiscal Year 2019-20 City of Lemon Grove Mid-Year Budget, and
- 2) Adopt a resolution approving the Fiscal Year 2019-20 Appropriations Limit, and
- 3) Authorize the transfer of \$804,924 from the FY 18-19 Fund balance to the City's 115 Trust for investment towards future CalPERS obligations.

Closed Session:

CONFERENCE WITH LEGAL COUNSEL – ANTICIPATED LITIGATION

Government Code Section 54956.9b

Number of potential cases: 1

<u>Adjournment</u>

In compliance with the Americans with Disabilities Act (ADA), the City of Lemon Grove will provide special accommodations for persons who require assistance to access, attend and/or participate in meetings of the City Council. If you require such assistance, please contact the City Clerk at (619) 825-3800 or email schapel@lemongrove.ca.gov. A full agenda packet is available for public review at City Hall.

AFFIDAVIT OF NOTIFICATION AND POSTING

STATE OF CALIFORNIA)
COUNTY OF SAN DIEGO) SS
CITY OF LEMON GROVE)

I, Shelley Chapel, MMC, City Clerk of the City of Lemon Grove, hereby declare under penalty of perjury that a copy of the above Agenda of the Regular Meeting of the City Council of the City of Lemon Grove, California, was delivered and/or notice by email not less than 72 hours before the hour of 5:00 p.m. on February 14, 2019, to the members of the governing agency, and caused the agenda to be posted on the City's website at www.lemongrove.ca.gov and at Lemon Grove City Hall, 3232 Main Street Lemon Grove, CA 91945.

/s/: Shelley Chapel
Shelley Chapel, MMC, City Clerk



CITY OF LEMON GROVE

CITY COUNCIL STAFF REPORT

			STAFF REPOR
Item No. <u>1.A</u>			
Meeting Date:	February 18, 2020		
Submitted to:	Honorable Mayor ar	nd M	embers of the City Council
Department:	City Manager's Office	е	
Staff Contact:	Kristen Steinke, City	/ Atto	orney
Item Title:	Waive the Full Te	xt R	eading of all Ordinances
	and adopted by title only	•	
Environmental Not subject to			□ Negative Declaration
		1	<u> </u>
☐ Categorical Ex	kemption, Section		☐ Mitigated Negative Declaration
Fiscal Impact: N	None.		
Public Notificat	ion: None		



Public Notification: None.

CITY OF LEMON GROVE

CITY COUNCIL STAFF REPORT

		STAIT REI ON			
Item No. <u>1.B</u>					
Meeting Date:	February 18, 2020				
Submitted to:	Honorable Mayor and M	embers of the City Council			
Departmen t:	City Manager's Office				
Staff Contact:	Rod Greek, Interim Fina	nce Manager			
Item Title:	City of Lemon Grove Payment Demands				
Recommended Environmental	Action: Ratify Demand Review:	S.			
Not subject to		☐ Negative Declaration			
	kemption, Section	☐ Mitigated Negative Declaration			
Fiscal Impact: N	Jone.				

City of Lemon Grove Demands Summary

Approved as Submitted: Rod Greek, Interim Administrative Services Director For Council Meeting: 02/18/20

ACH/AP Checks 01/23/20-02/05/20

376,815.24

Payroll - 01/28/20

124,646.28

Total Demands 501,461.52

CHECK NO	INVOICE NO	VENDOR NAME	CHECK DATE	Description	INVOICE AMOUNT	CHECK AMOUNT
ACH	63284730	WEX Bank	01/23/2020	Fuel - Fire Dept - Dec'19	74.27	74.27
ACH	Refill 1/22/20	Pitney Bowes Global Financial Services LLC	01/23/2020	Postage Usage 1/22/20	250.00	250.00
ACH	Jan15-Jan28 20	Calpers Supplemental Income 457 Plan	01/30/2020	457 Plan 1/15/20-1/28/20	8,160.63	8,160.63
ACH	Jan28 20	Employment Development Department	01/30/2020	State Taxes 1/28/20	6,828.25	6,828.25
ACH	Jan28 20	US Treasury		Federal Taxes 1/28/20	24,568.75	24,568.75
ACH	Jan20	Wage Works		FSA Reimbursement - Jan'20	2,813.60	2,813.60
ACH	Jan20	Power Pay Biz/Evo		Online Credit Card Processing - Jan'20	92.76	92.76
ACH	Feb 2020	Pers Health		Pers Health Insurance - Feb'20	48,165.58	48,165.58
ACH	Refill 2/3/20	Pitney Bowes Global Financial Services LLC		Postage Usage 2/3/20	250.00	250.00
ACH	Jan20	Authorize.Net		Merchant Fees -Jan'20	30.15	30.15
ACH	10251588	LEAF		Ricoh C3502 Copier System-PW Yard - Jan'20	160.51	160.51
12523	14172063 14221190	AT&T	01/29/2020	Phone Service- 12/13/19-1/12/20 Fire Backup Phone Line- 12/22/19-1/21/20	84.16 40.27	124.43
12524	5656001542 5656005373 5656920858	AutoZone, Inc.	01/29/2020	High Mileage Motor Oil - LGPW#17 '99 Ford F350 Windshield Wiper - LGPW Backhoe 420E Diesel Exhaust Fluid/Cleaner/Degreaser - Sanitation	15.48 17.23 43.09	75.80
12525	34592-IN	Aztec Landscaping Inc.	01/29/2020	Landscape Mgmt Svc - Dec'19	9,183.41	9,183.41
12526	1/28/20	California State Disbursement Unit	01/29/2020	Wage Withholding Pay Period Ending 1/28/20	161.53	161.53
12527	2304 2305 2315	Clark Telecom & Electric Inc.	01/29/2020	Street Light Dig-Alert Markouts - Dec'19 Street Light Repairs - Dec'19 St Light Knockdown Pole Replacement/7909 Broadway - Dec'19	255.35 3,276.05 2,708.85	6,240.25
12528	202000007	County of SD/Assessor/Recorder/Clerk	01/29/2020	Recording Services- 12/2/19	32.00	32.00
12529	20199630 20199631	Dudek	01/29/2020	Prof Svcs: Inspection Support Svc/Grove Hill Proj 11/30-12/27/19 Prof Svcs: Inspection Support Svc/Sewer CIP Proj 11/30-12/27/19	2,375.00 675.00	3,050.00
12530	INV1016984	George Hills Company	01/29/2020	TPA Claims- Adjusting/Other Services - Dec 19	1,595.50	1,595.50
12531	100000010942395	Globalstar USA, Inc.	01/29/2020	Satellite Service 12/16/19-1/15/20	172.59	172.59
12532	43581	Harris & Associates	01/29/2020	Prof Svcs:LG Rdwy & Lighting Dist-Review&Audit 11/24/19-12/28/19	13,938.75	13,938.75
12533	PS020046747	Hawthorne Machinery Co	01/29/2020	Equip Maint- CAT 420E Backhoe- Edge Cutting/Bolts/Nuts	198.91	198.91
12534	97770 97925 98410	Horton, Oberrecht, Kirkpatrick & Martha, APC	01/29/2020	Legal Svcs: GHC0019886 Legal Svcs: GHC0019886 Legal Svcs: GHC0019886	5,000.00 5,000.00 5,345.34	15,345.34
12535	00071928	Hudson Safe-T- Lite Rentals	01/29/2020	Parking Markers/Bollard Installation at 8119 Broadway	97.43	97.43
12536	Jan28 20	ICMA	01/29/2020	ICMA Deferred Compensation Pay Period Ending 1/28/20	780.77	780.77
12537	4775211	Mallory Safety and Supply, LLC	01/29/2020	HazMat Spill Kit/Safety Glasses/Hi Visibility Sign	175.35	175.35
12538	Reimb: 1/27/20	Malone, Audrey	01/29/2020	Reimb: Certificate Holders & Foil Seals - KIVA Graduation	105.51	105.51
12539	1070223	Michael Baker International	01/29/2020	Prof Svc: As-Needed Engineering Svcs thru 11/30/19	26,379.75	26,379.75
12540	19087	Norman A Traub Associates LLC	01/29/2020	Legal Svcs - 8/24/19-11/22/19	4,403.77	4,403.77
12541	WO-64752-1 WO-64752-2	Office Advantage, Inc.	01/29/2020	Office Supplies- Fire Office Supplies- Fire	89.56 12.70	102.26
12542	150918 151119	Pacific Sweeping	01/29/2020	Street Sweeping/Parking Lot - Nov'19 Street Sweeping/Parking Lot - Dec'19	6,428.55 6,428.55	12,857.10
12543	1/20/2020	SDG&E	01/29/2020	3225 Olive- 12/18/19-1/20/20	147.19	147.19
12544	Jan 2	Southern CA Firefighters Benefit Trust	01/29/2020	LG Firefighters Benefit Trust 1/2/20	830.70	2,492.10

	Jan 16 Jan 30			LG Firefighters Benefit Trust 1/16/20	830.70 830.70	
		T 0 : Will 0	04 /00 /0000	LG Firefighters Benefit Trust 1/30/20		
12545	0462-8			Graffiti Paint	144.33	144.33
12546	72460513 72468183 72468184	Vulcan Materials Company	01/29/2020	Asphalt Asphalt Asphalt	373.57 102.36 102.36	578.29
12547	1/22/2020 1900909910 4036195180 4036195180 4036778607 4037934601 4038470447 4039045552 81995051 12/1/2019 12/12/2019 12/12/2019 12/19/2019 12/19/2019 12/18/2019 11/29/2019 11/29/2019 11/29/2019 11/29/2019 11/29/2019 11/29/2019 11/29/2019 12/4/4/2019 12	Wells Fargo	01/29/2020	AT&T - Backup City Hall Internet - 12/23/19-1/22/20 Cintas - Janitorial Supplies - 11/14/19 Cintas - Janitorial Supplies - 11/27/19 Cintas - Janitorial Supplies - 12/5/19 Cintas - Janitorial Supplies - 12/19/19 Cintas - Janitorial Supplies - 12/19/19 Cintas - Janitorial Supplies - 12/19/19 Cintas - Janitorial Supplies - 12/26/2019 Cintas - Janitorial Supplies - 1/2/20 Cintas - Janitorial Supplies - 1/9/20 Corelogic - Image Requests - Nov'19 Cox - Main Phone/Fire 12/1/19-12/30/19 Cox - Calsense Modem Line: 2259 Washington 12/11/19-1/10/20 Cox - Phone/PW Yard/2873 Skyline- 12/19/19-1/18/20 Cox - Calsense Modem Line: 2259 Washington 12/11/19-1/18/20 Cox - Calsense Modem Line: 235 Mt Vernon 12/9/19-1/8/20 Cox - Calsense Modem Line: 8235 Mt Vernon 12/9/19-1/8/20 Cox - City Hall 12/1/19-12/31/19 Cox - City Manager/Copy Room Fax Line- 12/18/19-1/17/20 Cox - City Manager/Copy Room Fax Line- 12/18/19-1/17/20 Cox - City Hall Fire Alarm 11/27/19-12/26/19 Cox - PEG Circuit Svc- 11/30/19-12/29/19 Cox - Phone/Rec Ctr/3131 School Ln- 12/4/19-1/3/20 House of Automation - Service Call - PW Yard Pitney Bowes - Postage Meter Rental 9/30/19-12/29/19 Verizon - Modems- Cardiac Monitors - 11/4/19-12/3/19 Verizon - City Phone Charges- 11/13/19-12/12/19 Verizon - PW Tablets- 11/13/19-12/12/19	85.60 1,012.63 201.34 201.34 201.34 359.39 201.34 201.34 21.34 11.00 441.17 23.11 214.93 20.32 94.39 978.77 75.00 4.25 45.63 2,896.56 98.02 335.00 180.75 14.04 129.35 76.02 198.80	8,502.77
12548	2619-4 Rev	Charles King Company, Inc.	02/05/2020	2017-18 Sewer CIP Contract # 2019-11 thru 9/30/19	20,601.48	20,601.48
12549	FRS0000189 FRS0000189 FRS0000189 FRS0000189 FRS0000189 FRS0000189 FRS0000189 FRS0000189 FRS0000189 FRS0000189 FRS0000189 HCA0000303 HFTA000167	City of El Cajon	02/05/2020	Overtime Reimbursement - Hays 12/8/19 Overtime Reimbursement - Kinoshita 11/30/19 Overtime Reimbursement - Cameron 12/21/19 Overtime Reimbursement - Diaz 12/22/19 Overtime Reimbursement - Garcia 12/19/19 Overtime Reimbursement - Kelsen 12/18/19 Overtime Reimbursement - Kinoshita 12/14/19 Overtime Reimbursement - Nevin 12/14/19 Overtime Reimbursement - Paddock 12/17/19 Overtime Reimbursement - Pinson 12/20/19 Overtime Reimbursement - Sanchez 12/30/19 HCFA Assessments - QTR 3 FY19/20 HFTA Fees - QTR 3 FY19/20	1,179.09 1,208.74 1,238.93 1,269.68 1,238.93 1,301.53 1,208.74 1,443.73 1,269.68 1,238.93 1,179.09 65,300.00 4,356.00	83,433.07
12550	FY18-19 LG	County of San Diego- Dept of Public Works	02/05/2020	District Operation & Maintenance Charges FY2018-19	6,904.00	6,904.00
12551	3501 3521	County of San Diego- Registrar of Voters	02/05/2020	Petition Signature Verification - Trans & Use Tax Mar 3, 2020 Presidential Primary Election - Advance Deposit	12,007.00 19,000.00	31,007.00
12552	Cox Home	Cox Home Security	02/05/2020	Refund/Cox Home Security/Overpaid Business License Fees	190.00	190.00
12553	2020CA Election	DFM Associates	02/05/2020	2020 CA Elections Code Book/Paperback	56.84	56.84
12554	dsb20190292	Dig Safe Board	02/05/2020	State Fee/Regulatory Monthly Costs/Dig Alert 2019	57.13	57.13
12555	Oct-Dec19	Division of the State Architect	02/05/2020	State CASP Fee (\$1),(\$4) - 10/1/19-12/31/19	194.80	194.80
12556	Reissue 1/3/17	Drum, Daryn	02/05/2020	Re-issue: Data Analysis Training/San Jose/Meals/Drum 11/14-17/16	47.48	47.48
12557	Feb-20	Fidelity Security Life Insurance Company	02/05/2020	Vision Insurance -Feb20	310.26	310.26
12558	2018.024	Firewerx	02/05/2020	FireWerx Wildland Hose Pack 2+1	173.60	173.60
12559	Harris	Harris, Donald	02/05/2020	Refund/Harris, Donald/Diversion Deposit CD1-900-0066	500.00	500.00
12560	628266	League of California Cities	02/05/2020	League Membership Dues for 2020	10,682.00	10,682.00
12561	1657	League of California Cities,San Diego Division	02/05/2020	2020 League Membership Dues & Meetings- SD County Division	1,200.00	1,200.00
12562	1072956	Michael Baker International	02/05/2020	Prof Svc: As-Needed Engineering Svcs thru 12/31/19	9,301.63	9,301.63
12563	235169 235170	Ninyo & Moore	02/05/2020	6800 Mallard Ct Inspection Svcs thru 12/27/19 1963 Berry St Inspection Svcs thru 12/27/19	1,882.00 3,082.00	4,964.00
12564	Owens	Owens, Beverly	02/05/2020	Refund/Owens, Beverly/Deposit - LBH- 1/25/20	200.00	200.00
12565	INV00009759	RapidScale Inc.	02/05/2020	Virtual Hosting/Back Up Svc/Cloud Storage 1/31/20 - 2/28/20	3,675.78	3,675.78
12566	Reimb: 1/27/20	Romero, Lydia	02/05/2020	Reimb: Airfare/LCC Homeless Mtg/Sacramento/Romero 11/4/19	204.97	204.97
12567	Jan-Jun 20	San Diego County Sheriff's Department	02/05/2020	Cal-ID Program Costs 1/1/20-6/30/20	3,144.00	3,144.00
12568	8129114508	Shred-It USA	02/05/2020	Shredding Services 1/22/20	80.22	80.22

12569	CINV-007937	Trusaic	02/05/2020 2020 ACA Basic Plus Svcs - Initial Deposit	1,500.00	1,500.00
12570	120200391	Underground Service Alert of Southern Ca.	02/05/2020 59 New Ticket Charges - Jan'20	107.35	107.35
				376,815.24	376,815.24



Public Notification: None.

CITY OF LEMON GROVE

CITY COUNCIL.

THE	STAFF REPORT
Item No. <u>1.C</u>	
Meeting Date:	February 18, 2020
Submitted to:	Honorable Mayor and Members of the City Council
Department:	City Manager's Office
Staff Contact:	Shelley Chapel, City Clerk
	Schapel@lemongrove.ca.gov
Item Title:	Approval of City Council Meeting Minutes
Recommended	Action: Approval of City Council Meeting Minutes.
Environmental Not subject	Review: to review Negative Declaration
☐ Categorical 1	Exemption, Section Mitigated Negative Declaration
Fiscal Impact: N	Jone.

MINUTES OF A MEETING OF THE LEMON GROVE CITY COUNCIL TUESDAY, FEBRUARY 4, 2020

The City Council also sits as the Lemon Grove Housing Authority, Lemon Grove Sanitation District Board, Lemon Grove Roadway Lighting District Board, and Lemon Grove Successor Agency.

Call To Order:

Mayor Vasquez called the Regular Meeting to order at 6:02 p.m.

Present: Mayor Racquel Vasquez, Mayor Pro Tem Jennifer Mendoza, Councilmember Yadira Altamirano, and Councilmember Jerry Jones.

Absent: Councilmember David Arambula

Staff Members Present:

Lydia Romero, City Manager, Kristen Steinke, City Attorney, Mike James, Assistant City Manager/Public Works Director, Noah Alvey, Community Development Manager, Shelley Chapel, City Clerk, Steven Swaney, Fire Chief, Lieutenant Stranger, San Diego County Sheriff's Office - Lemon Grove Substation, and Roberto Hidalgo, Human Resources Manager.

Pledge of Allegiance:

Pledge of Allegiance to the Flag was led by Councilmember Jones.

Public Comments: No comments.

City Council Oral Comments & Reports on Meetings Attended At City Expense: (G.C. 53232.3(d))

Councilmember Y. Altamirano attended the following meetings and events:

- New City Councilmember Academy hosted by the League of CA Cities
- Young Men's Leadership Conference
- McAlister Graduation Ceremony

Mayor Pro Tem Mendoza attended the following meetings and events:

- Vice-Chair to Transportation, Communication and Public Works Committee Meeting with the League of California Cities
- East County Meeting of the SANDAG Board with Councilmember Jones
- MTS Board Meeting as Alternate

Mayor Vasquez attended the following meetings and events:

SANDAG Meeting

1. Consent Calendar:

- A. Waive Full Text Reading of All Ordinances on the Agenda.
- B. Ratification of Payment of Demands
- C. City Council Meeting Minutes for Regular Meeting January 21, 2020. Approval of Resolution No. 2020-3504, Authorizing the Submittal of a CalRecycle Local Government Waste Tire Enforcement Grant Application in Partnership with the City of San Diego – Solid Waste Local Enforcement Agency and Authorizing the City of San Diego to Act on Behalf of the City of Lemon Grove to Execute All Necessary Grant Documents.
- D. Rejection of Claim Edward Dominick
- F. Rejection of Claim Diane Ravelle
- G. Rejection of Claim Edward Wong

<u>Action</u>: Motion by Councilmember Jones, seconded by Mayor Pro Tem Mendoza to approve Consent Calendar Items A-G.

The motion passed by the following vote:

Ayes: Vasquez, Mendoza, Altamirano, Jones

Noes: Arambula

Reports to Council:

2. Adopted Resolution No. 2020-3705 entitled, "A Resolution of the City Council of the City of Lemon Grove, California, Changing the Name of Civic Center Park to Treganza Heritage Park"

Mayor Vasquez introduced Mike James, Assistant City Manager / Public Works Director who gave the report and PowerPoint presentation.

Appeared to comment were: Laura Hook, Helen Ofield, Cynthia Hughes-Doyle, Roberta Bulling,

<u>Action</u>: Motion by Councilmember Jones, seconded by Councilmember Altamirano to adopt Resolution. The motion passed by the following vote:

Ayes: Vasquez, Mendoza, Altamirano, Jones

Noes: Arambula

State of California Senate Bill 50

Mayor Vasquez introduced Noah Alvey, Community Development Manager who gave the report. This item failed on the Senate floor so not valid.

Action: Staff recommendation was to receive and file.

Closed Session:

 CONFERENCE WITH LEGAL COUNSEL – ANTICIPATED LITIGATION Government Code Section 54956.9b
 Number of potential cases: 1

2. CONFERENCE WITH LEGAL COUNSEL – EXISTING LITIGATION

Government Code Section 54956.9

Name of Case: Citrus St. Partners LLC v. City of Lemon Grove; City Council of the City of Lemon Grove

(CASE NO. 37-2019-00064690-CU-MC-CTL)

City Attorney Kristen Steinke announced the City Council will be adjourning to closed session at 6:46 p.m. for the purposes above.

City Attorney Steinke reported no reportable action on items discussed in Closed Session.

Adjournment:

There being no further business to come before the Council, the meeting was adjourned at 6:59 p.m. to a meeting to be held Tuesday, February 18, 2020, in the Lemon Grove Community Center located at 3146 School Lane, for a Regular Meeting.

Shelley Chapel, MMC	
City Clerk	



LEMON GROVE SANITATION DISTRICT

DISTRICT BOARD STAFF REPORT

Item No. 1.D

Meeting Date: February 18, 2020

Submitted to: Honorable Chair and Members of the Lemon Grove Sanitation

District

Department: Public Works Department

Staff Contact: Mike James, Assistant City Manager / Public Works Director

mjames@lemongrove.ca.gov

Stephanie Boyce, Senior Management Analyst

sboyce@lemongrove.ca.gov

Item Title: Accept the Fiscal Year 2017-18 Sewer Capital Improvement

Project (Contract No. 2019-11) as Complete

Recommended Action: Adopt a resolution accepting the Fiscal Year 2017-18 Sewer Capital Improvement Project (Contract No. 2019-11) as complete.

Summary: In support of the Sanitary Sewer Master Plan and associated capital improvement project, the Lemon Grove Sanitation District Board (District Board) awarded the Fiscal Year 2017-18 Sewer Capital Improvement Project to Charles King Company in February 2019.

Background: On February 19, 2019, Charles King Company was awarded the Fiscal Year 2017-18 Sewer Capital Improvement Project (Contract No. 2019-11) with a total bid cost of \$338,290.00 and a project budget not to exceed \$437,896.00. Since the project was awarded, there have been three (3) change orders. Change Order No.1 was issued for additional potholing, Change Order No. 2 was issued for the import and export of unsuitable backfill material, and Change Order No. 3 was issued for the deduction of items not necessary in the completion of the project including monumentation allowance, fence repair and a field order. The overall change orders reflect the deduction of items and unforeseen construction items totaled \$9,845.10. The final project cost totaled \$401,843.60 which includes bid advertisement, construction costs, material testing and inspection. On October 21, 2019, the District's inspector and staff completed the final inspection of the improvements and determined the work was completed per the contract specifications.

Staff recommends that the District Board adopt a resolution (Attachment A) accepting the work as complete, authorizes the District Manager or designee to file a Notice of Completion with the County of San Diego, and authorizes staff to release the retention no sooner than thirty (30) days after the Notice of Completion has been filed.

Environmental Review:	
Not subject to review	☐ Negative Declaration
Categorical Exemption, Section	Mitigated Negative Declaration
Fiscal Impact: Funding has been allocated for	rom the Sanitation District Capital fund.
Public Notification: None.	
Staff Recommendation: Adopt a resolution Capital Improvement Project (Contract No. 20	1 0
Attachment: Attachment A – Resolution	

RESOLUTION NO. 2020 -

A RESOLUTION OF THE LEMON GROVE SANITATION DISTRICT, CALIFORNIA, ACCEPTING THE FISCAL YEAR 2017-18 SEWER CAPITAL IMPROVEMENT PROJECT (CONTRACT NO. 2019-11) AS COMPLETE

WHEREAS, on February 19, 2019, the Lemon Grove Sanitation Board awarded the 2017-18 Sewer Capital Improvement Project (Contract No. 2019-11) to Charles King Company; and

WHEREAS, the contract bid amount was established at \$338,290.00 and a total project budget not to exceed \$437,896.00; and

WHEREAS, three change orders in the total amount of \$9,845.10 increased the original contract price of \$338,290.00 to 348,135.10; and

WHEREAS, the final project cost of \$401,843.60 was allocated for this project from the Sanitation District; and

WHEREAS, on October 21, 2019, Charles King Company completed the scope of work as defined by the original contract and change orders; and

WHEREAS, the District inspector inspected all of the improvements and determined that Charles King Company fulfilled its contractual obligations.

NOW, THEREFORE, BE IT RESOLVED that the Lemon Grove Sanitation District hereby:

- 1. Accepts the work for the FISCAL YEAR 2017-18 Sewer Capital Improvement Project (Contract No. 2019-11) as complete; and
- 2. Authorizes the District Manager or designee to file a Notice of Completion with the County of San Diego; and
- 3. Authorizes district staff to release the retention no sooner than thirty (30) days after the Notice of Completion is filed.

Attachment A

PASSED AND ADOPTED on	, 2020, the Lemon Grove Sanitation
District, California, adopted Resolution	No, passed by the following vote:
AYES:	
NOES:	
ABSENT:	
ABSTAIN:	
	Racquel Vasquez, Chair
Attest:	
Shelley Chapel, MMC, District Clerk	_
Approved as to Form:	
Kristen Steinke. District Attornev	



CITY OF LEMON GROVE

CITY COUNCIL STAFF REPORT

Item No. ___2__

Meeting Date: February 18, 2020

Submitted to: Honorable Mayor and Members of the City Council

Department: Community Development Department

Staff Contact: Noah Alvey, Community Development Department

nalvey@lemongrove.ca.gov

Item Title: Continuation of Public Hearing to Consider Conditional Use

Permit Application CUP-190-0002, A Request to Establish a Medical Marijuana Dispensary at 3515-3521 Harris Street in

Special Treatment Area III, Regional Commercial

Recommended Action: Continue the public hearing for consideration of CUP-190-0002, direct staff to re-notice the public hearing based on actions by the San Diego Superior Court, and provide that no new sensitive uses shall prejudice the application.

Summary: This is a request to establish a medical marijuana dispensary (MMD) at 3515-3521 Harris Street in General Plan Special Treatment Area III, Regional Commercial. The project proposes demolition of an existing duplex and improvements to two existing buildings to create sales and staff spaces for the MMD as well as off-site parking for dispensary staff. Proposed site improvements include new landscape and trees, commercial driveway and parking area, and city standard street improvements.

The Application is the subject of a Temporary Restraining Order (TRO) issued by the San Diego Superior Court in pending litigation entitled Citrus St Partners LLC v. City of Lemon Grove, et al. (SDSC Case No.: 37-2019-00064690-CU-MC-CTL). The TRO restricts the City and the City Council from making a final determination on the subject CUP application until the Court makes a ruling on the request for Preliminary Injunction and includes other restrictions pending the outcome of Petitioner's motion for preliminary injunction.

Prior to the adjournment of the duly noticed public hearing on January 21, 2020, City Council moved to continue the public hearing to a date certain of February 18, 2020, with the provision that no new sensitive uses shall prejudice the application.

On January 28, 2020, KIM Investments, LLC filed a peremptory challenge with the San Diego Superior Court resulting in the re-assignment of the case to a new judge and a new hearing date for the motion for a preliminary injunction of May 1, 2020.

Staff recommends that the hearing be continued and that a new public hearing notice be distributed based on the outcome of the May 1, 2020, hearing date or subsequent hearing dates, as applicable.

Environmental Review:	
■ Not subject to review	☐ Negative Declaration
Categorical Exemption, Section	Mitigated Negative Declaration

Fiscal Impact: There is no fiscal impact.

Public Notification: Notice of Public Hearing for this item was given in accordance with LGMC Section 17.28.020(F) on January 9, 2020. The item was continued at the January 21, 2020 to a date certain of February 18, 2020, without further notice pursuant to Section 17.28.020(G).

Staff Recommendation: Continue the public hearing for consideration of CUP-190-0002, direct staff to renotice the public hearing based on actions by the San Diego Superior Court, and provide that no new sensitive uses shall prejudice the application.

LEMON ROVE

CITY OF LEMON GROVE

CITY COUNCIL STAFF REPORT

Item No. 3

Meeting Date: February 18, 2020

Submitted to: Honorable Mayor and Members of the City Council

Department: Public Works Department

Staff Contact: Mike James, Assistant City Manager / Public Works Director

mjames@lemongrove.ca.gov

Item Title: Acceptance of the Drainage Master Plan Update

Recommended Action: That the City Council adopt a resolution accepting the Drainage Master Plan Update.

Summary: On June 18, 2019, the City Council received and accepted the first, of two, phases of the Citywide Drainage Master Plan (DMP) update. That first phase addressed the regulatory drivers that apply to drainage system, created a high resolution geospatial data set, assessed all drainage areas in the City, and recommended improvements based on closed circuit television results for the corrugated metal pipe (CMP) system. At that same meeting, the City Council directed staff to move forward with the second phase of the DMP update that included: researching and updating the probable construction costs and prioritizing recommended capital improvement projects.

The second phase of the DMP update is now complete and staff presents the DMP update for acceptance. The remaining portion of this report highlights the second phase activities that were added to the DMP update.

Discussion: The DMP update is a comprehensive plan and tool to highlight existing storm water conveyance system deficient along with a condition assessment of the CMP storm drains throughout the City. Like the City's pavement and sewer master plans, the DMP update prioritizes capital improvement projects with current cost estimates that will be used by the City to make future funding and construction decisions.

As a brief summary, the City is responsible for managing the public storm drain system within the City limits (approximately 3.9 square miles) and ensuring that an adequate level of service is provided to protect the public from excessive surface flooding conditions. To this end, the need for a comprehensive and high-resolution hydrologic and hydraulic (H&H) analysis to evaluate the existing storm water conveyance system level of service citywide was identified. The intent of this study and final report is to build off of past micro-studies, and provide a holistic understanding of the City's storm water infrastructure thus, allowing the City to prioritize its maintenance and repairs efforts.

The first phase of the report consisted of four areas:

- 1. <u>Regulatory Framework</u>: The City must be responsive to a number of regulatory drivers that apply to drainage, storm water infrastructure management, and water quality specific to each storm drain outfall system. These drivers focus on addressing one particular storm water related component, each with different compliance metrics, timelines, and monitoring requirements. All of these nuances are critical to develop any DMP.
- 2. <u>High Resolution Geospatial Data</u>: A high resolution geospatial dataset is essential to perform the detailed hydrologic and hydraulic drainage and water quality analyses. Geospatial data necessary for these modeling efforts include: an accurate topographic representation of the study area, ground cover/land use information, and existing storm drain inventory. This section focused on receiving and evaluating raw data layers, adjusting the data and making corrections as needed, and summarizing the revised dataset for future modeling with field verification.
- 3. <u>Drainage Assessment</u>: The assessment was accomplished using an integrated 1-D/2-D H&H model that combines surface and sub-surface drainage patterns within the study area to provide a high-resolution surface inundation and storage of storm water flow for the duration of a design storm. This study considers the 2-year, 10-year and 100-year storm events in order to understand the performance of the drainage conveyance system during storms with a higher probability of occurrence.
- 4. <u>Recommended Improvements</u>: The CMP systems were televised using closed-circuit television (CCTV) and the results were used to create a condition rating from very poor to good. With each condition a recommended repair technique was provided that include the following options:
 - a. Cured in place pipe (CIPP) lining,
 - b. CIPP sectional repairs,
 - c. Top Hat (TH) in lateral/main connection sealing,
 - d. Pressurized hydrophilic grout and urethane sealant,
 - e. Hydro-scouring, and
 - f. Pipe removal and replacement.

A summary of the pipe segments rating and quantity is provided in the report. Additionally, all repair techniques and number of repairs necessary were included. Lastly, ten regional improvement opportunities were included in the report that could provide detention or water quality benefits. The list of each location, the size and parcel ownership (in addition to the City) were included in the report.

The second phase of the DMP update focused on the following two (2) tasks:

- 1. <u>Probable Construction Costs</u>: Research available unit costs for project construction based on historical bid history or other readily available sources. Unit costs will be provided to the City. Additionally, a generalized order of magnitude opinion of probable construction cost for each of the recommended facilities will be provided to aid in the prioritization of projects.
- 2. <u>Bundling and Prioritization of Recommended Improvements</u>: Provide prioritization scores for each recommended facility to assist in ranking the benefit of each potential improvement. A matrix will consider modeling results as well as relevant fields from the existing GIS data. Areas will be bundled into relevant project areas and forecasted for a ten-year period.

The final report (**Attachment B**) now contains an updated single source of information that:

- 1. Analyzed existing storm water conveyance system deficiencies,
- 2. Completed a condition assessment of the CMP storm drainage,
- 3. Provides for prioritized drainage improvement recommendations for use in the City's capital improvement program, and
- 4. Provides surface and subsurface drainage patterns, flowrates, deficiencies, and ultimately proposed project recommendations.

The third and fourth comments above identify the critical needs that have not been consolidated prior to this current update to the Master Plan. The needs identified in the report highlight forty-two (42) projects varying in cost from \$25,000 up to \$10 million with a combined cost of \$78 million. These improvements provide storm drain capacity benefits and reduce the total volume of surface ponding from 87 acre-feet to 66 acre-feet in the 10-year storm event model. Additionally, staff asked Rick Engineering Company to look towards the City's neighbors and determine if there are areas where the City can partner with other public entities to create regional projects for future water quality best management practices. That yielded at least ten (10) potential project locations that could involve partnerships with the City of La Mesa, County of San Diego, and City of San Diego.

This DMP update successfully utilized high-resolution data with an integrated model to determine existing deficiencies and identify recommended improvements for drainage infrastructure. The results from this report will assist staff by utilizing it as a guide and a resource tool to manage the drainage Capital Improvement Projects (CIP) moving forward and will be reflected in the City's Capital Improvement Program.

Environmental Review: ☐ Not subject to review ☐ Negative Declaration ☐ Categorical Exemption, Section ☐ Mitigated Negative Declaration Fiscal Impact: \$50,000 was allocated in the Fiscal Year 2019-2020 budget from Fund 02 — Gas Tax Fund (SB-1 Roadway Maintenance and Rehabilitation Act). Public Notification: None.

Staff Recommendation: That the City Council adopt a resolution (**Attachment A**) approving the Drainage Master Plan Update.

Attachments:

Attachment A — Resolution Attachment B — Drainage Master Plan Update

RESOLUTION NO. 2020 -

A RESOLUTION OF THE CITY COUNCIL OF THE CITY OF LEMON GROVE, CALIFORNIA, APPROVING THE DRAINAGE MASTER PLAN

WHEREAS, in 1997, the City contracted with ASL Consulting Engineers to create a drainage master plan (master plan); and

WHEREAS, there was a need to perform and update to the master plan that would include data collection and compilation, CCTV of the corrugated metal pipe storm drain system, existing condition hydrologic and hydraulic analysis, recommend improvements, identifying regional improvement opportunities, and develop a final drainage master plan update; and

WHEREAS, in order to complete this update in an economically efficient process the expertise of a consulting firm that possess the knowledge, skills, and abilities in completing master plans would be needed; and

WHEREAS, Rick Engineering Company was identified by City staff as a consulting firm that has -proven experience in creating and updating master plans in the County; and

WHEREAS, in February 2020, Rick Engineering Company completed the final phase of the City's drainage master plan and submitted the final report to the City; and

WHEREAS, the City Council reviewed and accepted the final report.

NOW, THEREFORE, BE IT RESOLVED that the City Council of the City of Lemon Grove hereby:

- 1. Accepts the citywide drainage master plan update prepared by Rick Engineering Company; and
- 2. Authorizes the City Manager, or designee, to manage the project close out process.

•	
	, 2020, the City Council of the City of olution No, passed by the following
AYES:	
NOES:	
ABSENT:	
ABSTAIN:	
	Racquel Vasquez, Mayor
Attest:	
Shelley Chapel, MMC, City Clerk	_
Approved as to Form:	
Kristen Steinke, City Attorney	

DRAINAGE MASTER PLAN

City of Lemon Grove

February 2020



City of Lemon Grove Drainage Master Plan

February 12, 2020

Presented To City of Lemon Grove Public Works Department

3232 Main Street Lemon Grove, California 91945



Presented ByRick Engineering Company

5620 Friars Road San Diego, California 92110

> P: 1-619-291-0707 F: 1-619-291-4165 rickengineering.com

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- D. INUNDATION MAPS
- E. PROPOSED CONDITIONS
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- G. COSTS AND PRIORITIZATION

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Acronyms/Abbreviations

Acronym/Abbreviation	Definition			
BMP	best management practice			
cfs	cubic feet per second			
DEM	digital elevation model			
DMP	drainage master plan			
ft	foot, feet			
GIS	geographic information system			
H&H	hydrology and hydraulics			
LF	linear foot, linear feet			
LiDAR	Light Detection and Ranging			
LOS	level of service			
NOAA	National Oceanic and Atmospheric Administration			
NWP	nationwide permits			
RCB	reinforced concrete box			
RCP	reinforced concrete pipe			
ROW	right-of-way			
SANDAG	San Diego Association of Governments			
SanGIS	San Diego Geographic Information Source			
sq. mi.	square miles			
SSURGO	Soil Survey Geographic Database			
SWMM	Storm Water Management Model			
TMDL	total maximum daily load			

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Limitations:

The City of Lemon Grove Drainage Master Plan is a comprehensive plan for existing drainage needs within the City of Lemon Grove. This report has been prepared for master planning purposes only, as a guide for engineers, planners, developers, and City staff. Detailed engineering calculations and investigations should be prepared for the implementation of any of the facilities outlined in this study. In addition, coordination with adjacent municipalities or state agencies may be required to coordinate drainage improvement efforts that cross jurisdictional boundaries.

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1.0 Introduction

The *Drainage Master Plan* (DMP) has been prepared for the City of Lemon Grove (City) to significantly advance the City's storm water management goals by analyzing existing storm water conveyance system deficiencies along with a condition assessment of the CMP storm drains throughout the City in order to inform future decisions pertaining to public storm drain infrastructure improvements. The City is responsible for managing the public storm drain system within the City limits, and ensuring that an adequate level of service is provided to protect the public from excessive surface flooding conditions. To this end, the need for a comprehensive and high-resolution hydrologic and hydraulic (H&H) analysis to evaluate the existing storm water conveyance system level of service citywide was identified. The City has undergone multiple studies to address the known "hot spots" of the City. The intent of this project is to build off of these past efforts and provide a holistic understanding of the City's storm water infrastructure allowing the City to prioritize their efforts.

The City of Lemon Grove study area limit is approximately 3.9 square miles in area. However, the entire watershed area tributary to the City of Lemon Grove study area covers approximately 5.5 square miles due to areas draining into and out of the City from the City of San Diego, City of La Mesa, and Spring Valley, a community of unincorporated area in San Diego County. Most of the City is within the Chollas Sub-basin draining to the West through South Las Chollas Creek, Radio Drive Branch, Encanto Branch, and Jamacha Branch going from the north of the City to the South, respectively. The remaining portion to the east of the City drains to the east to the La Nacion Sub-basin through Brookside Branch and Spring Valley Creek from north to south respectively. Figure 1-1 and the following paragraph provide an overview of the DMP components and the overall process that was developed for this project.

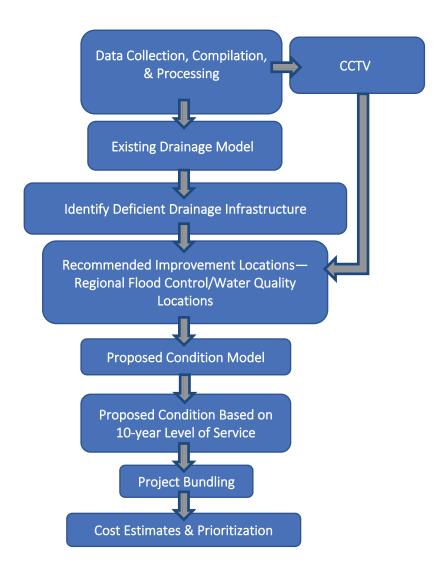
The first, and arguably most critical, component in the DMP framework is the data collection regarding the existing storm drain infrastructure and drainage conditions, including corrections to a Geographic Information System (GIS) inventory of structure and conveyance features within the study area. The second process in the DMP framework is modeling the existing drainage condition to establish a baseline and identify existing drainage issues within the study area. Results from the analysis of existing drainage conditions can then be used to review locations with problematic drainage patterns and assist in informing solutions including potential areas for detention or water quality projects. The third process includes incorporating the proposed drainage recommendations into the baseline drainage model creating the ultimate condition proposed condition model. The final process is grouping proposed improvements into bundled projects.

A total of forty-two (42) bundled projects were identified as a part of the DMP. These projects were then prioritized based on a prioritization matrix that assesses the length, CCTV rating, and severity of existing capacity among other variables and costs. **The total cost for the forty-two (42) projects is \$78,183,649 and they will remove 121 inundated structures from the 10-year storm event**. The top five (5) projects based on

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the prioritization that was established provide much needed backbone infrastructure along the Federal Boulevard system and have an estimated cost of \$15,459,541 and remove 42 inundated structures from the 10-year storm event.

The DMP along with the associated GIS data set, web tool, and spreadsheets will provide a highly detailed drainage improvement plan that will allow the City to easily assess and implement improvements for the area's current flooding issues. This DMP summarizes the recommendations and presents them within the City of Lemon Grove Drainage Master Plan Web Mapping Application (https://maps.rickengineering.com/lgdmp/).



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Figure 1-1: DMP Framework

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1.1 Regulatory Framework

When evaluating potential infrastructure improvements, the City must be responsive to a number of regulatory drivers that apply to drainage, storm water infrastructure management, and water quality specific to each storm drain outfall system. These regulatory drivers are typically focused on addressing one particular storm water-related component, each with different compliance metrics, timelines, and monitoring requirements. Understanding the nuances inherent in meeting the overall regulatory framework in the watershed was a critical component in developing the DMP and is summarized in the sections below.

1.1.1 Drainage Infrastructure Requirements

The County of San Diego maintains certain regulatory standards for storm water improvements as stipulated in the San Diego County Hydraulic Design Manual, dated September 2014. The governing design storm typically used as the basis for drainage recommendations is the 100-year storm event, which is consistent with the requirements per the 2014 San Diego County Hydraulic Design Manual. One of this study's objectives was to assess the existing drainage infrastructure to determine the current Level of Service (LOS) relative to the County's policies for drainage design. Based on the results of the existing condition models and conversations with City staff, a more frequently returning 10-year storm event was selected as the desired LOS for the recommendations of this study. The proposed improvements provide an improved system compared to the existing condition with the goal to have capacity in the pipes contain the more frequent 10-year storm event that routinely affects residents. In addition to not being economically feasible, if the system was upsized to contain the 100-year storm event flow, the downstream receiving waters would be negatively affected at every culvert, and crossing. Additionally, based on the 2014 San Diego County Hydraulic Design Manual, the storm water conveyance system shall be designed so that the combination of storm drain system capacity and overflow (streets and gutter) will be able to carry the 100-year frequency storm. Therefore, this DMP modeled the 10-year storm events to assess LOS as well as analyzed the 100-year to assess street conveyance.

2.0 High Resolution Geospatial Data

A high resolution geospatial dataset is essential to perform detailed hydrologic and hydraulic drainage and water quality analyses. Geospatial data necessary for these modeling efforts include: an accurate topographic representation of the study area, ground cover/land use information, and existing storm drain inventory. While evaluating the data initially collected, it was determined that certain data components (such as the storm drain inventory junction points and line work) did not accurately reflect the field conditions and/or did not align spatially when compared against the aerial imagery of the study area. An effort to correct and compile the data from various sources into one comprehensive dataset was undertaken. Of particular focus during this effort was to ensure a correct spatial representation of the storm drain infrastructure, and collect any missing information. A revised dataset will also be useful for any future projects that the City or other consultants undertake within the study area.

Figure 2-1 displays a snapshot of the changes that were made to the GIS inventory, which demonstrates the amount of new information that was compiled in a representative portion of the study area.

Original GIS Inventory

Updated GIS Inventory

Subcatchment Delineations

Original GIS Inventory

Correction to GIS Inventory

Inlet Scale Subcatchment
Delineations

Figure 2-1: Snapshot of New Storm Drain Information Added to GIS Inventory

The following sections of this report describe the geospatial data received, the process of correcting and compiling certain data sets, and the resultant data from the correction process.

This section presents:

- Raw data layers received and sources (Section 2.1)
- Data adjustment and correction process (Section 2.2)
- Summary of the revised dataset (Section 2.3)

2.1 Raw Geospatial Data

Rick Engineering Company (RICK) used several data sets in addition to the original data from the City for this DMP. All utilized data sets are summarized in Table 2-1 with their associated version dates.

Table 2-1: Geospatial Data Inventory

Data Layer	Version Date	Source (Agency)		
LiDAR	2014	SanGIS, SANDAG, NGA, LECC, Regional Public Safety GIS, 18 Incorporated Cities		
Aerial Imagery	2017	County of San Diego		
Topography	2014	SANGIS		
Storm Drain Network Files (Drain Conveyance, Drain Structures)	September 7, 2018	City of Lemon Grove, SanGIS, SANDAG		
Land Use	January 1, 2017	SanGIS, SANDAG		
Hydrologic Soil Groups (SSURGO)	November 11, 2013	Natural Resources Conservation Service		
Parcel Layer	February 15, 2018	SanGIS, SANDAG, Assessor/Recorder/County Clerk		
Floodplain Layers	April 7, 2016	Federal Emergency Management Agency		
Municipal Boundaries	July 25, 2011	SanGIS, SANDAG		

2.2 Corrections to GIS Inventory

Corrections to the GIS storm drain inventory were required to model the existing conditions of the City of Lemon Grove. The completeness of storm drain inventory data was critical in ensuring the effectiveness and practicality of subsequent modeling analyses. RICK was tasked with updating the City's storm drain inventory to more accurately reflect the current existing condition of the study area. For the purposes of preparing a DMP, the storm drain data necessary for this study consists of the horizontal layout of the existing storm drain system, size and material of conduits, and flowline elevations (if feasible). As displayed in Figure 2-2, storm drain inventory revisions were conducted in a two-step process; (1) desktop analyses and (2) field verification.

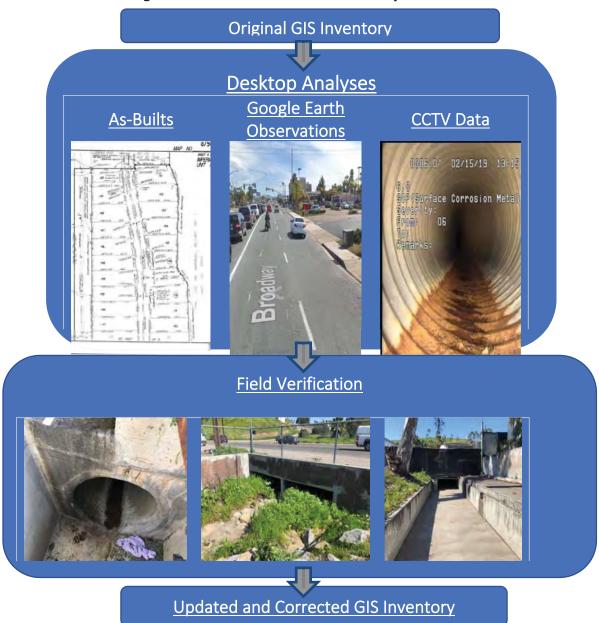


Figure 2-2: Corrections to GIS Inventory Flowchart

2.2.1 Desktop Analyses

Desktop analyses involved updating the storm drain structures and conveyance information in the City's existing GIS dataset based on previous survey data, as-built drawings, aerial imagery, CCTV data, and Google Earth observations. The horizontal location of drainage structures in the inventory was corrected to match the aerial imagery. RICK utilized survey data from previous projects to assist in assigning invert elevations to drainage structures. For structures in which depth measurements were not accessible on site and survey or as-built drawing data was not available, engineering judgment was used to assign an invert elevation based on upstream

and downstream drainage connections. A Digital Elevation Model (DEM) was utilized to update rim elevations for drainage structures not previously identified in the received data. Google Earth and Street View were used to update the location and type of each inlet and drainage structure.

2.2.2 Field Verification

Several field visits were conducted as part of the DMP effort to supplement the desktop analyses in correcting the GIS inventory. These assessments included storm drain system inventory verification to assess the status of assets including inlet locations and sizes, storm drain diameters and materials, structure depths, connectivity, and drainage patterns.

Figure 2-3: CMP conduit in the northern portion of Lemon Grove (Left).

Spillway in the northern portion of Lemon Grove (Right).





2.3 Revised Geospatial Data

The main objective of the GIS storm drain data revisions was to ensure that a complete and accurate representation of the existing drainage system was reflected on the GIS shapefiles. The revisions incorporated into the GIS shapefiles were provided back to the City for use outside of this DMP.

Table 2-2 provides a summary of the changes to the original storm drain inventory received from the City of Lemon Grove. The existing inventory was updated for storm drains that were larger than 36 inches in diameter

(or considered part of the primary backbone system). The inventory was also updated to add missing drainage structures such as inlets, pipe segments, cleanouts, and outlets. Facilities were updated through referencing survey and as-built data as well as through Google Earth and Google Street observations conducted via desktop analysis. Certain facilities were flagged to be checked in person and those facilities were assessed via site visits that were conducted over the course of about three (3) days. As shown, multiple structures and conveyance segments were added to the inventory via this process.

Table 2-2: Data Source of Drainage Asset Properties

	Desktop Analyses				et al d		
	Surveying Data	As-built Data	DEM	Google Earth/Street View Observations	Field Verification		
Structures							
Location	X	Χ		X	X		
Type of Structures	X	Х		X	X		
Rim Elevation	X	Χ	Χ		X		
Invert Elevation	X	Х	X		X		
Depth			Χ		X		
Conveyance							
Location / Orientation	X	Χ		X	X		
Type of Conveyance	X	Х		X	X		
Material	X	Χ			X		
Diameter	X	X			X		
Pipe Offsets					Х		

Below, Table 2-3, provides a summary of the changes to the original storm drain inventory received from the City.

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Table 2-3: Summary of Original and Existing (revised) Storm Drain Inventory

Asset Type	Original Data Set Provided	Existing Condition Revised Data	Change in Features	Percent Change
Structure				•
Fitting	7	0	-7	-100%
Inlet	703	782	79	11%
Manhole	85	103	18	21%
Clean out	14	44	30	214%
Discharge	173	18	-155	-90%
Channel confluence	0	77	77	100%
Conduit connection ¹	0	90	90	100%
Downstream headwall	0	152	152	100%
Flowline connection	0	21	21	100%
Headwall	0	112	112	100%
Not present	0	1	1	100%
Outlet	0	21	21	100%
Outlet, D-25	0	57	57	100%
Spillway	0	31	31	100%
Unimproved	0	37	37	100%
Total	982	1546	564	57%
Conveyance				
Culvert	3	0	-3	-100%
Ditch	51	89	38	75%
Drainage facility	698	1058	360	52%
Earthen channel	46	57	11	24%
Earthen ditch	13	13	0	0%
Open channel	52	131	79	152%
Surface flow/flowline	0	193	193	100%
swGravity Main	860	0	-860	-100%
Total	1723	1541	-182	-11%

^{1.} A conduit connection can be categorized as a structure that connects two (2) or more conduits but was not verified in the field.

In order to better define the inventory, the conveyance and structure facilities were reclassified into subcategories that are more informative for future needs while keeping the integrity of the existing inventory. While the number of assets may have reduced, the overall value of the data has increased and become more robust.

3.0 Drainage Assessment

Drainage assessment was accomplished using an integrated 1-D/2-D hydrologic and hydraulic (H&H) model that combines surface and sub-surface drainage patterns within the study area. One of the most beneficial aspects of integrated 1-D/2-D modeling is the ability to render high-resolution surface inundation and storage of storm water flow for the duration of a design storm. An existing condition model was prepared, which presented a high resolution visual rendering of the combined surface and sub-surface drainage patterns within the study area. For the purposes of this study, the 100-year storm event was used to evaluate the storm drain infrastructure to inform infrastructure improvements. Other storm events (2-year and 10-year) were also modeled in order to understand the performance of the drainage conveyance system during storms with a higher probability of occurrence.

The existing condition H&H model highlighted several areas where the existing drainage infrastructure (i.e., inlets, storm drains, and surface street conveyance) is considered deficient in terms of storm water conveyance during a 100-year storm event. These deficiencies include locations with storm water ponding above the curb and extending onto the sidewalk and into private property.

The 2-D component of the analysis allowed for the evaluation of the benefit provided to surface conveyance capacity after the addition of storm drain infrastructure (i.e. to quantify the benefit of proposed drainage improvements). A reasonable objective for future drainage improvements is to reduce flood depths in the ROW to 6 inches or less, (i.e., flood depths would be less than the standard curb height per San Diego Regional Standard Drawings – 2018 and storm water conveyance would be contained within the ROW). Additional information regarding the specific drainage H&H methodology used in this study can be found in a memo located in Appendix A.

This section presents the following:

- Overview of the existing drainage patterns (Section 3.1)
- Model Setup Methodology (Section 133.2.1)
- Modeling Results (Section 3.2.2)

3.1 Drainage Patterns

The total drainage area in the study is approximately 3,508 acres and drains in a southwesterly direction. The topography of the city is characterized by relatively flat to mild slopes in developed areas, and steeper slopes on the edge of the city boundary and the valleys formed primarily around Lemon Grove Avenue and Federal Boulevard. The drainage infrastructure is a combination of pipes and culverts that are more prevalent along main and highly utilized streets such as Broadway and Lemon Grove Avenue, and open channels and ditches that are present more in the residential areas.

3.1.1 Subcatchment Delineations

RICK utilized semi-automated delineation tools in GIS to create initial delineations of subcatchments and flow paths for each inlet. After the initial delineation, RICK modified the subcatchment areas during the QA/QC process and ended with 861 subcatchments, as seen in Figure 3-1. Due to the high resolution of the topographic data, the GIS delineation tools were able to identify flow paths along curbed roadways, through backyards, and across driveways, establishing an effective baseline for subcatchment delineations.

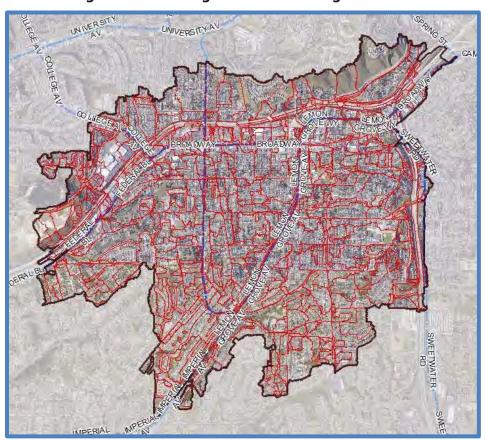


Figure 3-1: Drainage Areas of Existing Condition

These subcatchments were then combined to create five (5) overall subwatershed systems labeled 1-5 based on their location west to east. These systems, as seen in Figure 3-2, can be identified by their major road or drainage path. System 1 contains Broadway and Federal Boulevard, System 2 contains Massachusetts Avenue, System 3 contains Lemon Grove Avenue, System 4 contains part of Broadway and Sweetwater Road, and System 5 contains some of Sweetwater Road and consists of the rest of the drainage areas that do not drain to Systems 1-4. Systems 1-3 have their own unique drainage outlets; all of their respective subcatchments confluence to one (1) outfall. System 4 has two (2) outfalls. System 5 is made of a collection of drainage conveyance systems whose subcatchments do not share an outfall. System 5 consists of the remaining conveyance facilities not included in the other four (4) subwatershed drainage areas.

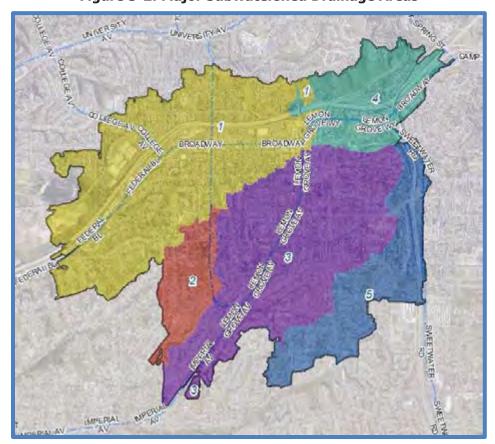


Figure 3-2: Major Subwatershed Drainage Areas

3.1.2 Surface Conveyance

An important component of the storm water conveyance system in the Lemon Grove study area is the multitude of channels and ditches connecting the conveyance behind and around buildings. There are a few open channels of note in the study area. These main channels run behind buildings, adjacent to railroad tracks, and are main portions of the backbone drainage system in their respective drainage area system. System 1 has large channels

behind the commercial buildings on Federal Boulevard. System 3 has large channels next to the railroad tracks on Lemon Grove Avenue. The 2-D mesh provided a way to visualize the surface conveyance.

Some of these open channels are smaller than the resolution of the 2-D mesh and proved to be a challenge to represent in a 2-D model. In order to properly analyze the geometry and conveyance of these open channels, they were modeled as 1-D conduits with a 2-D mesh overlay. Larger channels that could be defined solely by the DEM were modeled just with 2-D mesh.

Refer to the existing condition maps located in Appendix A for a visual overview of the surface conveyance conditions modeled.

3.2 Existing Condition

3.2.1 Existing Condition Model Methodology

The corrected GIS storm drain inventory discussed in section 2.0 was imported into PCSWMM and formed the basis of the 1-D conveyance portion of the study area model. Storm drain networks were visually inspected horizontally with reference to aerial imagery and vertically by viewing the storm drain profiles generated within the program to verify the suitability of the data.

The DEM was used to develop a 2-D model surface to represent storm water flows in streets, alleys, open channels, and open space areas. A directional 2-D mesh was applied in these areas to represent the preferential direction of flow. This surface was coupled to the 1-D storm drain inventory to match the rim elevations at points of connection to the storm drain conveyance system.

The computer modeling approach utilized has the capability to quantify the shallow surface attenuation (aka – detention) occurring in the right-of-way (ROW) and its effect to the peak flows entering the storm drain system (peak flow rates entering the system may be attenuated, which may reduce the size of required improvements).

Table 3-1 below shows a breakdown of the storm drain pipes analyzed in the existing condition model.

Table 3-1: Existing Conditions Storm Drain Pipe Diameters and Lengths Modeled

Diameter (in)	Length (ft)	Pipe and Culvert Count	%
4	614	2	0.5%
6	984	5	0.7%
8	667	4	0.5%
10	73	1	0.1%
11	62	1	0%
12	4,683	58	3.6%
15	2,147	21	1.6%
18	33,514	329	25.5%
20	425	2	0.3%
21	754	5	0.6%
24	30,791	246	23.5%
27	178	3	0.1%
30	17,432	95	13.3%
33	1,378	4	1.1%
36	15,748	82	12.0%
39	98	1	0.1%
42	5,117	22	3.9%
48	6,039	46	4.6%
54	757	5	0.6%
57	735	6	0.6%
60	2,835	12	2.2%
66	292	2	0.2%
72	4,447	20	3.4%
78	1,484	5	1.1%
Total	131,254	977	100%

See Appendix A for a summary of the hydrologic results of the single-storm model simulations at each storm drain outfall modeled within the study area.

3.2.2 Existing Condition Results

Modeling results highlighted deficiencies in the LOS of the conveyance system within the study area. This is most obvious in the storm drain networks located at Federal Boulevard, Broadway, Broadway and Sweetwater, Lemon Grove Avenue, and Madera Street, where a significant length of storm drain pipes identified in the inventory did not demonstrate capacity to convey the 100-year storm event. While reviewing the City's as-builts, it was observed that much of the storm drain conveyance currently in place was designed in the 1960's and 1970's. It is believed that those areas were not designed for the LOS currently required within the City of San Diego drainage design standards.

Model results were obtained for the 24-hour storms at the 2-, 10-, and 100-year return period from the precipitation data obtained from NOAA Atlas 14 Precipitation Frequency Data Server (PFDS) as discussed in the memo located in Appendix A of this report. The 24-hour storm events were judged to be the most pertinent storm events due to the volume of runoff generated and the peak flows generated at the main outfall of each storm drain system.

Modeling results highlighted deficiencies in the level of service (LOS) of the conveyance system within the study area and full results can be found in Appendix F.

During the 100-year storm about 38% of the conveyance distance is below or at capacity. Table 3-2 provides an overview of the results observed in the 2-, 10-, and 100-year, 24-hour storm events compared to the surcharging conduits of the storm drain network.

Figure 3-3 depicts the lengths and number of pipes in each conveyance capacity category over 100%.

Table 3-2: Existing Condition Storm Drain Conveyance Capacity Summary

Conveyance	2-Year Storm	10-Year Storm	100-Year Storm
Capacity (%)¹	Pipe Length (feet)	Pipe Length (feet)	Pipe Length (feet)
< 100	111,813	98,635	80,580
100 - 150	13,324	22,157	35,385
150 - 200	3,410	5,697	7,905
> 200	2,562	4,620	7,239
Total	131,109	131,109	131,109

1. Conveyance capacity is the max full flow in the pipe compared to the maximum flow the pipe is designed to convey.

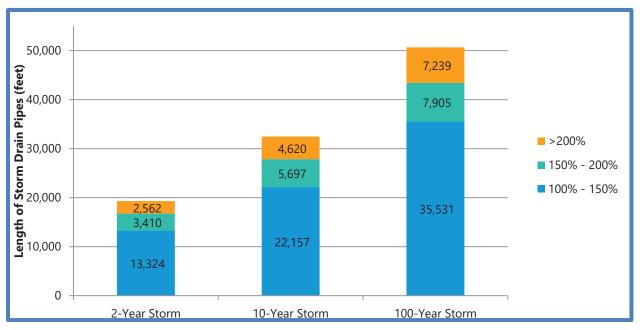


Figure 3-3: Existing Condition Storm Drain Conveyance Capacity

Undersized storm drain facilities caused a significant amount of storm water to pond on the street surfaces. In many locations water ponds in excess of one (1) foot on the surface at the low points. Table 3-3 provides a summary overview of the peak storm water stored on the 2-D surface and the overall corresponding ponding depth. The structures experiencing the various flood depths are counted alongside their respective depths.

Table 3-3: Existing Condition 2-D Cell Peak Storage Volume 24-HR Storm Events

Ponding	2-Year S	Storm	10-Year Storm		100-Year Storm	
Depth (inches)	Volume (AcFt.)	Structures (#)	Volume (AcFt.)	Structures (#)	Volume (AcFt.)	Structures (#)
0 - 6	11.42	293	43.85	409	21.99	499
6 - 12	9.83	59	13.44	89	22.34	181
> 12	34.85	61	29.84	94	105.34	139
Total	56.10	413	87.14	592	149.67	819

Refer to the existing condition maps located in Appendix C for a visual representation of the depths and limits of surface inundation within the study area. Table 3-4 presents a summary table of peak flow rate results at the storm drain outfall locations obtained from the modeling efforts.

Table 3-4: Existing Condition Storm Drain Outfall Summary

System ID	Drainage Area (ac.)	Peak Flow Rates (cfs) 2-YR 10-YR 100-YI			
1	1317.2	563.2	967.2	1724.3	
2	245.4	132.08	196.5	353.6	
3	1120.3	523.5	912	1604	
4	600.2	345.4	551	1021.6	
5	457.6	357.9	614.6	987.8	

3.3 Proposed Condition

3.3.1 Proposed Condition Model Methodology

Results from the existing condition models were evaluated in several aspects to determine an effective balanced approach to decrease the amount of surface ponding, and increase storm drain pipe capacities in the study area. The September 2014 *San Diego County Hydraulic Design Manual* states that storm drains in conjunction with surface drainage are to be designed to convey the 100-year storm. However, based on the severity of the deficiencies in the existing condition drainage infrastructure and subsequent conversations with City staff, it was decided that recommendations for the deficient infrastructure would target a 10-year level of service.

The objective of the recommended improvements aimed to reduce inundated structures during the 10-year storm event by improving storm drain pipes in the same drainage basin. The recommended pipe improvements were then bundled into CIP scale projects, providing drainage solutions for the area's most prone to drainage issues in the existing condition. The CIP projects provide city officials with the ability to streamline the drainage improvement process by providing a graphical representation of drainage needs throughout the City to be referenced during future projects of all types, thus allowing for the strategic bundling of multi-objective projects to reduce overall cost to the City and decrease the amount of time residents are impacted by construction

improvements that could be completed to collectively improve the surrounding area. The bundled projects provide city officials with a list of storm drain pipes that can be improved concurrently, decreasing the amount of time the street is impacted by construction.

Inundated structures were utilized as indicators of deficient drainage infrastructure and deficient facilities most likely resulting in the inundated structures were flagged for improvement. The combined peak flow from the surface and sub-surface conveyance model were used to size the deficient infrastructure. The improvements had to be recommended around several constraints; new alignments were not part of the process in this study, so the improvements had to stay within the existing alignments. Additionally, channels and ditches were not

recommended for improvements. With all these constraints the improvements for this study were recommended to the maximum extent practicable. Recommendations also included proposed improvements from other projects. These previous studies prepared by Rick Engineering included the August 17, 2014 "City of Lemon Grove Storm Drain Assessment of Existing Corrugated Metal Pipe (CMP) Facilities" and the July 6, 2018 "Flood Control Feasibility Analysis Report Along Federal Boulevard, Between Central Avenue and San Miguel Avenue in Lemon Grove, California."

In order to determine when additional barrels would be added in lieu of simply upsizing of the existing storm drain network, the following was considered during the evaluation process. If the proposed storm drain size was too large when proposed in conjunction with the existing invert elevations and resulted in an exposed storm pipe, additional barrels with smaller pipe diameters were recommended instead.

The proposed condition also considered the results of the CMP closed-circuit television (CCTV). Pipes that had a rating over zero (0) were replaced with RCP and any pipes upstream and downstream were also considered as candidates to be replaced. In some cases, the material of the pipe needed to be changed but the size did not in order to pass the 10-year flow.

3.3.2 Proposed Condition Results

The goal of this study was to compile and identify areas most frequently prone to flooding in order to alleviate the flooding of structures and major roadway corridors to the extent feasible through storm drain improvements. The method of improving drainage conditions throughout the City was to replace existing infrastructure, in place, with infrastructure that has the capacity to convey the selected LOS. In order to provide feasible improvements, the recommended infrastructure is to be replaced in the current alignment to reduce the probability of conflicts with other utilities during realignment. The alignments of the infrastructure can be adjusted during final design if necessary or desired. The recommended storm drain systems were sized accounting for the total flow getting to the pipe through both surface and subsurface conveyance. The decided upon Level of Service (LOS) for this study was for the storm drains to convey the 10-year event and for the combined storm drain and road way to convey larger events where feasible. The recommended improvements outlined in this study provide a significant LOS increase throughout the City and reduce the number of structures affected by stormwater inundation.

From these considerations, of the modeled 991 pipes, 277 were recommended to be upsized or replaced with RCP.

The 2-, 10-, and 100-year storm events were analyzed and Table 3-5 presents a summary overview of the impact that the replacement of storm drain infrastructure had on the entire storm drain pipe conveyance system

modeled in the proposed condition. Table 3-5 depicts the lengths and number of pipes in each conveyance capacity category over 100%.

Table 3-5: Proposed Condition Storm Drain Conveyance Capacity Summary

Conveyance	2-Year Storm	10-Year Storm	100-Year Storm
Capacity (%)¹	Pipe Length (feet)	Pipe Length (feet)	Pipe Length (feet)
< 100	126,941	115,166	89,255
100 - 150	3,787	14,036	35,097
150 - 200	1,792	1,618	4,660
> 200	466	2,166	3,975
Total	132,986	132,986	132,986

1. Conveyance capacity is the max full flow in the pipe compared to the maximum flow the pipe is designed to convey.

45,000 3.975 40,000 4,660 Tendth of Storm Drain Drain Drain Storm Drain Dr >200% **150% - 200% 100%** - 150% 35,097 2,166 1,618 14,036 5,000 3,787 2-Year Storm 10-Year Storm 100-Year Storm

Figure 3-4: Proposed Condition Storm Drain Conveyance Capacity

The storm drain facilities were upsized to reduce surface flooding and convey the 10-year storm event within the pipes and 100-year storm event within the street. Even though pipes are over 100% capacity, this does not mean

that there is flooding at each of these facilities. A pipe flowing over 100% could just indicate that that particular pipe is flowing under pressure. The results of the proposed infrastructure are more appropriately reflected in the number of flooded structures.

Table 3-6 provides a summary overview of the impact that the replacement of storm drain infrastructure had on the surface ponding conditions. The structures experiencing the various flood depths are counted alongside their respective depths.

Table 3-6: Proposed Condition 2-D Cell Peak Storage Volume 24-HR Storm Events

Ponding 2-Year S		Storm	orm 10-Year Storm		100-Year Storm	
Depth (inches)	Volume (AcFt.)	Structures (#)	Volume (AcFt.)	Structures (#)	Volume (AcFt.)	Structures (#)
0 - 6	8.94	248	34.33	317	18.58	447
6 - 12	5.79	44	9.69	67	16.79	116
> 12	30.56	59	22.41	80	71.75	121
Total	45.29	351	66.43	464	107.11	684
Decrease from Existing Condition	56.10	62	20.71	128	42.56	135

There are local sumps throughout the city and some structures have ponding around their perimeter due to a local sump. Therefore, those structures might not have a project near them and will experience local ponding in both the existing and proposed conditions.

Refer to the existing condition maps located in Appendix C for a visual representation of the depths and limits of surface inundation within the study area. Table 3-7 presents a summary table of peak flow rate results at the storm drain outfall locations obtained from the modeling efforts under the proposed conditions.

Table 3-7: Proposed Condition Storm Drain Outfall Summary

System ID	Drainage Area (ac.)	Peak Flow Rates (cfs) 2-YR 10-YR 100-YR			
1	1317.2	743	1,140	1,704	
2	245.4	131	225	356	
3	1120.3	633	1,068	1,637	
4	600.2	401	645	925	
5	457.6	353	621	1,037	

4.0 Recommended Improvements

4.1 Interim Solution for CMP Assessment

Field surveying was prepared for the CMP portion of the five (5) identified systems. Refer to Appendix B for backup information from the field survey. Refer to Attachment C for exhibits showing each CMP section.

Based on the results of the field survey, the CMP systems were televised using closed-circuit television (CCTV) by Affordable Pipeline Services.

There are 149 segments that were surveyed, and a rating system was used by Affordable Pipeline. Grades were assigned and they are as follows:

- 5 Most severe
- 4 Severe
- 3 Moderate
- 2 Minor to Moderate
- 1 Minor
- 0 Minor or No Televising Available

According to results from the televised survey, CMP conditions range from "minor" to "most severe". Many sections are classified as severe by way of debris accumulation and damage through corrosion where: the bottom half of the pipes are missing, large diameter holes are prevalent, or severe corrosion has made many small holes throughout a particular segment. Other segments are classified as severely damaged by way of deformation and deformation is characterized as severe if it restricts flow and/or the structural integrity of the pipe and prevents repair. Segments classified as moderate have light corrosion and/or debris accumulation and segments classified as minor are in good condition with no or minor corrosion and no or minor debris accumulation.

The repair techniques can be summarized into six (6) methods and they are as follows:

- Cured in Place Pipe (CIPP) Lining
- Cured in Place Pipe Sectional Repairs
- Top Hat (TH) in Lateral/Main Connection Sealing
- Pressurized Hydrophilic Grout and Urethane Sealant
- Hydro-Scouring
- Pipe Removal and Replacement

Refer to Appendix B for definitions of each of these repair techniques. The least costly repairs are those that are fully clogged with sediment and debris and they can be repaired by hydro-scour. The next least costly of the repairs are those with severe corrosion and multiple holes that are less than one (1)-foot diameter and these can be repaired with CIPP lining. The costliest set of repairs are those that are severely deformed or corroded with

sections of pipe missing or large diameter holes (greater than one (1)-foot diameter) and these will require pipe removal and replacement. Below is a summary of the CMP condition and the amount of each type of recommended repair.

Table 4-1: Summary of Pipe Segment Rating and Quantity

Grade/Rating	Number of Pipe Segments
5 – Most Severe	56
4 - Severe	14
3 - Moderate	56
2 – Minor to Moderate	5
0 – Minor or No Televising Available	18
Total	149

Table 4-2: Summary of Repair Technique, Quantity, and Length

Repair Technique	Segment Quantity	Segment Length (ft)
1 - Cured in Place Pipe (CIPP) Lining	20	1,860
2 - Cured in Place Pipe Sectional Repairs	1	430
3 - Top Hat (TH) in Lateral/Main Connection Sealing	1	-
4 - Pressurized Hydrophilic Grout and Urethane Sealant	4	895
5 - Hydro-Scouring	47	4,915
6 - Pipe Removal and Replacement	28	1,043
Total	101	9,143

About one third or 49 of the inspected CMP's require rehabilitation or replacement. Twenty-eight (28) pipes are either fully clogged with debris or have significant debris and need hydro-scouring. The remaining pipes have minor to moderated severity and do not require significant repair or maintenance.

Refer to Appendix B for backup information from the televised survey (CCTV), results, maps, and summary tables.

4.2 Regional Locations of Interest

Regional Improvement Opportunities that could provide detention or water quality benefits were identified through visual inspection. The size of the contributing drainage areas and land parcel ownership were the major contributing factors for identifying regional opportunities. A conscious effort was made to limit the identification of regional opportunities to parcels owned by the City; however, some locations on private parcels were identified as well in certain circumstances due to constraints in the public ROW, like lack of adequate space. The regional opportunities were also chosen based on their proximity to the outfall of the subwatershed system to maximize the impact of treatment.

In total ten (10) locations are currently identified as potentially viable regional improvement opportunities. The locations are listed below in Table 4-3 and refer to Appendix C for an exhibit of the locations.

Regional Improvement Opportunities Contributing **Impervious Area** ID **Parcel Ownership** Area (ac) (ac) 1 57.8 45.3 Thaidigsman Family Trust 2 324.4 201.2 Lemon Grove Alano Club 3 33.2 20.4 Retail Portfolio 30-1 LLC 7.5 4 14.4 Lemon Grove School District 5 54.6 33.4 Erickson Linda R 6 62.2 34.4 Shra Crockett Inc 7 124.3 74.1 Caltrans 8 208.5 128.2 City of Lemon Grove 9 Union Pacific Railroad Co. 35.3 17.1 Senior Community Centers/Community Health 10 32.8 19.9 **Partnerships**

Table 4-3: Regional Improvement Opportunities

4.3 Drainage Recommendations

The following sections present summaries of the various structures associated with the drainage infrastructure.

4.3.1 Storm Drain Recommendations

The recommendations for the storm drain pipe system consist of addressing deficient facilities that, based off the modeling results, caused or contributed to inundation of structures during the 10-year storm event. The 10-year storm event was targeted to improve the level of service during the more frequent storm events.

In addition to replacing storm drain pipes by their capacity, the material of the pipe was also considered. CMP rated above 0 are recommended for replacement. The CMP facilities recommended for replacement were

recommended for conversion to RCP pipe of the appropriate size to convey the 10-year flow at the location. Pipes upstream and downstream were assessed and if they were CMP, were also recommended for replacement. Table 4-4 compares the number of drainage facilities in the existing and proposed condition. For a visual representation of the proposed storm drain improvements, refer to the maps provided in Appendix E.

Junctions were edited in response to editing the pipes they were connected with but these changes were minor and the changes are not analyzed between the existing and proposed conditions.

Table 4-4: Storm Drain Recommendations Summary

	Existing Condition	Proposed Condition	
Facility type	Total	Replaced	% Replace
Storm Drain (LF) ¹	265,225	226,576	85

¹ Includes lengths from dual pipe systems.

4.3.2 Future Channel Restoration Opportunities

As previously stated, small channels were assigned dimensions and had an overlay of 2D mesh and larger channels were modeled with the 2D mesh. In the proposed condition, channels were not the focus of proposed improvements. However, as part of the effort in analyzing the proposed condition results, channels that are in flooded areas are flagged for potential improvements. Refer to Appendix E for locations of proposed channels.

4.4 Individual Improvement Costs

Appendix C has maps of results from the 2-, 10-, and 100-year storm event models. These maps visually highlight the deficiencies within the citywide drainage system encountered during the modeling efforts. A visual observation of the drainage infrastructure displayed on these maps led to the conclusion that the City's drainage deficiencies are not concentrated within one central location, but rather they are distributed throughout various neighborhoods and watersheds. This data is crucial for determination of implementation strategies.

As a goal of this study, the results from the Citywide DMP have been leveraged to develop potential Capital Improvement Program (CIP) projects to address the drainage deficiencies where they occur. This was accomplished via a series of steps:

- Hydrologic and hydraulic analysis of the backbone storm drain infrastructure throughout the City.
- Recommending storm drain pipe size improvements for infrastructure which was determined to have deficient conveyance capacity.

- Determining individual priority for the recommended storm drain infrastructure improvements based on hydrologic and hydraulic analysis results and other applicable data.
- Grouping individual infrastructure improvements into CIP project bundles based on geographic location.

This process led to the development of bundled CIP projects which were then evaluated in more detail to determine potential benefits and/or consequences that may arise during the implementation process. After these projects were vetted, the recommended improvements were entered into a hydrologic and hydraulic model to determine the extent of the benefit yielded by the recommendations. The following sections provide further explanations of this process.

4.4.1 Selection Criteria

The method for selecting potential CIP projects involved the development of scoring criteria, as outlined in Figure 4-1. These criteria were developed to rate the efficiency of all existing storm drain segments and then assess the bundled projects by their effect on inundated buildings. The first set of criteria generates a simplified ranking system ranging from a score of 0 - 55 with 55 being the highest possible score to determine the importance of providing recommendations for the system. An extra 25 points are awarded to a pipe based on its CCTV rating, represented by the CMP Score. Summing the Raw Total with the Synergy Bonus Points, the highest possible rating for a pipe is 80 points.

Once all existing storm drains were scored, the criteria were further refined to prioritize based on bundled project; each bundled project was assessed based on its effect on reducing flooding to buildings. The projects were bundled based on their proximity and connection to one another. Analyzing the area upstream and downstream from a project allowed for each individual project to be assessed based on its effect on the buildings in the area. Each project area was visually inspected to confirm that buildings were not negatively affected by a project upstream or downstream. The individual scoring and bundled project assessment were combined in a final project prioritization step that assigned values based on a project's standing in flood reduction and number of priority assets. This resulted in projects with scores between 30 and 100.

Cost was factored in to the Flood Reduction Score by including normalized values from FEMA's Estimated Flood Loss Potential into the bundled projects' flood reduction score. FEMA has loss potential costs associated with depth of flooding. The costs used in this analysis are normalized averages of three ranges: 1-6 inches, 6-12 inches, and 12-48 inches. Refer to Appendix G for the FEMA data.

This dual assessment in the prioritization process allows for the proposed improvements to be used both on the individual scale and project scale. There are costs for each of the forty-two (42) bundled projects as well as costs for each individual pipe that is proposed for improvements.

Figure 4-1: CIP Selection Criteria

Rating Criteria (per asset)	Max. Score	Subcriteria Score
Public Safety	35	
Land Use Impacts		(0 to 20)
Adjacent to High-Priority Land Use		20
Adjacent to Developed Land Use		10
Adjacent to Vacant Land Use		0
Within Major Roads		(0 to 15)
Conveyance Characteristics		
Ease of Implementation	20	
Projects within Existing City Ownership, Right- of-Way, or Easement		20
Projects Located on Unimproved Property/Vacant		15
Raw Total	55	

Synergy Bonus Points	25	
CMP Score		(0 to 25)
Score 5		25
Score 4		20
Score 3		15
Score 2		10
Score 1		5
Synergy Total	25	
Overall Project Score	80	
Project Prioritization		
Flood Reduction Score	60	(0 to 60)
Highest Ranked 10% of Projects		60
Second Ranked 30% of Projects		40
Lowest Ranked 60% of Projects		20
Normalized Project Score Per Weighted Asset Score	40	(0 to 40)
Highest Ranked 10% of Projects		40
Second Ranked 30% of Projects		20
Lowest Ranked 60% of Projects		10

4.4.2 Results

From the extensive and detailed modeling came forty-two (42) potential CIP projects that encompass all the proposed conditions modeling. However, this DMP has provided more detailed information on the top five (5) feasible CIP projects with the most favorable flood control benefits. These five (5) CIP projects are viable drainage improvements which can be implemented to provide a better level of service for their respective areas with minimal adverse effect on the connecting systems. These projects have been selected to address known hotspots within the City and reduce existing deficiencies by upsizing existing infrastructure. The projects in this section are not based on priority.

The results of the top five (5) project bundles are displayed in Table 4-5. Refer to Appendix G for the summary table of improvements and costs for all forty-two (42) projects.

The total cost of CIP projects is \$78,183,649 and remove 121 structures from experiencing inundation. The top five (5) CIP projects range in price from \$78,856.37 to \$10,026,193.78 and include storm drain and culvert improvements. The top five (5) projects remove forty-two (42) structures from experiencing flooding. This spectrum of project sizes and types allows the City a broad array of projects from which to select. The potential for storm drain improvements made System 1 the most likely to have the most desirable projects.

Table 4-6 provides a comparison of results between the existing and proposed conditions for the top five (5) projects while Table 4-7 provides a comparison of results between the existing and proposed conditions for all forty-two (42) projects. Below, Table 4-8, provides a comparison of inundated structures for the top five (5) projects while Table 4-9 provides a comparison of inundated structures for all forty-two (42) projects. The number of structures experiencing ponded water decreases in the proposed condition due to the proposed improvements.

Table 4-5: Costs of the Top 5 Prioritized Projects

Project Bundle ID	Capital Cost	Soft Cost (32% P&D)	Total Project Cost
1_1	\$ 1,173,106.71	\$ 563,091.22	\$ 1,736,197.93
1_3	\$ 53,281.33	\$ 25,575.04	\$ 78,856.37
1_11	\$ 1,623,433.18	\$ 779,247.92	\$ 2,402,681.10
1_2	\$ 6,774,455.26	\$ 3,251,738.52	\$ 10,026,193.78
1_9	\$ 821,359.05	\$ 394,252.35	\$ 1,215,611.40
SUM	\$10,445,635.52	\$5,013,905.05	\$15,459,540.58

Table 4-6: Comparison of Storm Drain Results of the Top 5 Prioritized Projects

Conduits: 2-Year Subtotal of			ity 10-Year Capacity			100-Year Capacity						
Deficiencies (LF)	<100	100- 150	150- 200	>200	<100	100- 150	150- 200	>200	<100	100-150	150- 200	>200
Existing Conditions	5,284	2,017	660	191	3,707	2,859	1,261	324	2,852	3,596	1,105	598
Proposed Conditions	4,528	4,119	260	613	6,539	2,320	564	97	4,528	4,119	260	613
Flood Reduction Benefit from Proposed Conditions	756	(2,102)	400	(422)	2,832	539	697	227	1,676	(523)	845	(15)
% Change	14%	-104%	61%	-221%	76%	19%	55%	70%	59%	-15%	76%	-3%

Table 4-7: Comparison of Storm Drain Results of All Projects

Conduits: Subtotal of	2-Year Capacity					10-Year Capacity			100-Year Capacity			
Deficiencies (LF)	<100	100-150	150- 200	>200	<100	100- 150	150- 200	>200	<100	100- 150	150- 200	>200
Existing Conditions	27,614	9,569	2,847	2,190	18,524	15,833	4,378	3,485	13,753	19,081	4,653	4,732
Proposed Conditions	42,300	1,242	495	180	35,683	7,295	564	675	24,872	16,900	1,255	1,190
Flood Reduction Benefit from Proposed Conditions	14,686	8,327	2,352	2,010	17,159	8,538	3,814	2,810	11,119	2,181	3,398	3,542
% Change	53%	87%	83%	92%	93%	54%	87%	81%	81%	11%	73%	75%

Table 4-8: Comparison of Inundated Structures of the Top 5 Prioritized Projects

	Ponding Depth	2-Year Storm	10-Year Storm	100-Year Storm	
	(inches)	Structures (#)	Structures (#)	Structures (#)	
	0 - 6	91	109	113	
Existing	6-12	21	28	49	
	> 12	17 21		31	
	Total	129 158		193	
	Ponding Depth (Inches)	Structures (#)	Structures (#)	Structures (#)	
Proposed	0 - 6	66	85	119	
	6-12	16	10	31	
	> 12	16 21		25	
	Total	98	116	175	
Comparison	Difference	31	42	18	

Table 4-9: Comparison of Inundated Structures of All Projects

	Ponding Depth	2-Year Storm	10-Year Storm	100-Year Storm	
	(inches)	Structures (#)	Structures (#)	Structures (#)	
	0 - 6	278	384	472	
Eviction	6-12	51	71	161	
Existing	> 12	45 73		112	
	Total	374	528	745	
	Ponding Depth (Inches)	Structures (#)	Structures (#)	Structures (#)	
Proposed	0 - 6	236	304	426	
	6-12	37	42	99	
	> 12	44	61	96	
	Total	317	407	621	
Comparison	Difference	57	121	124	

5.0 Conclusions

This DMP successfully utilized high-resolution data with an integrated PCSWMM modeling approach to determine existing deficiencies and identify recommended improvements for drainage infrastructure. The results from the project and subsequent prioritization provide the City of Lemon Grove with recommendations to be used in the City's planning and CIP. The results significantly advance the City's storm water management goals by not only assessing each individual pipe but by bundling recommendations into tangible projects. The value of the results of this project is that now the City has assessments for all of its storm drain pipes at its disposal with all of the results provided in a user-friendly web application tool.

The 1-D/2-D H&H model provides a visual representation of surface drainage in the City of Lemon Grove during different storm events. During the 2-, 10-, and 100-year, 24-hour storms, significant flooding occurs along Federal Boulevard and Lemon Grove Avenue. Additionally, during the 100-year, 24-hour storm a section of Broadway and the intersection of Broadway and Sweetwater Way experience significant flooding. The modeling also provides a list of deficient systems. In the 2-, 10-, and 100-year, 24-hour storm events there are 135, 227, and 347 deficient conduits, respectively.

This study provides ten (10) potential regional locations for future water quality BMPs. The delineations created for the entire watershed created the opportunity to calculate the contributing areas to each of these regional improvement opportunities. These locations were chosen based on the surrounding space and the contributing area. Additionally, channels were visually inspected and those that could be retrofitted in the future were flagged and included in the final package of these project's efforts.

Based on the results from the existing condition model, recommendations for the storm drain pipes were made and included upsizing and/or changing the material to RCP. Based on their surcharging junctions while conveying the 10-year storm event, pipes were upsized to be able to convey the flow without causing flooding. The goal was to improve the 10-year level of service, contain the flow within the street during the 100-year storm event, and decrease the amount of structures flooding in the 2-, 10-, and 100-year storm events. The drainage modeling and recommendations outlined in this report were able to reduce the total volume of surface ponding from approximately 87.14 acre-feet to 66.43 acre feet in the 10-year storm event. The drainage recommendations consist of storm drain replacement based on existing capacity and material. Based on location and system, recommendations were bundled into projects and resulted in forty-two (42) projects that vary in cost from \$25,343 to \$10,026,194. The combined cost for all the recommendations for these projects totals approximately \$78,183,649. These costs can be looked at on an individual pipe level or project level. In addition to this, each individual pipe is prioritized based on its location and CCTV rating. On a project scale, the project is prioritized based on its effect on the structures upstream and downstream of its location. The five top priority projects range

from \$78,856 to \$10,026,194 and remove forty-two (42) structures from experiencing flooding in the 10-year storm event and 121 structures in the 100-year storm event.

In summary, this study provides improvement costs for each individual pipe and bundles and prioritizes them into CIP-level projects. The City now has forty-two (42) bundled projects to support the City's CIP, paving the way for city staff to use each project to apply for grant money funding. Additionally, the City has a list of flagged channels recommended for future improvements in order to pursue water quality benefits that will be experienced by both the City of Lemon Grove and downstream receiving waters. Rather than reacting to problems when they arise, the City aims to take a proactive approach by moving forward with the information provided in the bundled projects. With the utilization of grant funding and local taxes, the City can use the list of bundled implementation ready projects this study produced to efficiently implement improvements. All the information collected and assessed during the study can be referenced within a user-friendly web-application for years to come.

6.0 References

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A. H&H Backup

1.0 Hydrologic Methodology and Modeling

PCSWMM uses EPA's SWMM Version 5 (SWMM5) engine, which uses the nonlinear reservoir model methodology to estimate the rainfall-runoff relationship for a subarea. Nonlinear reservoir modeling uses a combination of mass conservation and the Manning Equation to determine the volumetric flow rate from a subcatchment. SWMM5 requires several parameters to calculate runoff from each subcatchment. The parameters include area (in acres), characteristic width of the subcatchment, slope, percent impervious, Manning's "n" values for pervious and impervious overland surfaces, depression storage for pervious and impervious surfaces, percent of impervious area with no depression storage, and infiltration parameters.

1.1 Rainfall

Point precipitation data for the City of Lemon Grove study area was obtained from the National Oceanic and Atmospheric Administration (NOAA) Atlas 14 Precipitation Frequency Data Server (PFDS) (NOAA 2011). This data was selected because it has a longer period of record than the data presented in the *County of San Diego Hydrology Manual* (2003) to best reflect the historical rainfall and flooding events specific to the study area. Point rainfall data (total rainfall depth) was obtained for two rain gages nearest to the study area: Chollas Reservoir and La Mesa to compare with precipitation data obtained at the centroid of the study area (See Table 1-1).

Table 1-1: San Diego County local 24-Hour NOAA precipitation depth (inches)

Gage	Lat.	Long.	2-YR, 24-HR Precip. (in.)	10-YR, 24-HR Precip. (in.)	100-YR, 24-HR Precip. (in.)
Chollas Reservoir	32.7333	-117.0667	1.85	2.95	4.55
La Mesa	32.7675	-117.0233	1.97	3.19	5.03
City of Lemon Grove Study Area	32.7333	-117.0344	1.89	2.97	4.11

Source: NOAA 2011.

Notes: in. = inches; Lat. = latitude; Long. = longitude.

Based on this comparison, the rainfall precipitation depth data obtained at the centroid of the City of Lemon Grove study area is within range of nearby rain gages for the 2-, 10-, and 100-year storm events.

1.1.1 Rainfall Pattern

Setting up a storm simulation in EPA's Storm Water Management Model (SWMM) requires a hyetograph to distribute rainfall over time throughout the storm duration. Two options were considered:

• (2/3, 1/3) distribution as presented in the *County of San Diego Drainage Design Manual* (2003).

• Center distribution, (1/2, 1/2), based on USACE's HEC TD-15 guidance, *Hydrologic Analysis of Ungaged Watersheds Using HEC-1* (USACE 1982).

The 24-hour storm duration was selected for the study. The center storm distribution was selected because it meets this study's goals. The center storm distribution provides the peak intensities necessary to assess drainage infrastructure at the inlet scale (up to 5-minute rainfall intensities) while preserving the total volume of runoff generated from the storm duration. The two options generate the same precipitation volume however the (2/3, 1/3) storm distribution generates a greater volume leading up to the peak of the storm.

1.1.2 Rainfall Hyetograph Development

To develop the unit intensity duration relationship for the City of Lemon Grove study area, NOAA precipitation depth data from three rain gage stations within the study area were obtained for the 2-, 10-, and 100-year, 24-hour storm events. The point rainfall depth data obtained from the NOAA PFDS was used to generate intensity-duration pairs for the given durations. These intensity-duration pairs are incorporated into the rainfall intensity hyetographs. The 100-year precipitation depth data from these rain gages and the City of Lemon Grove study area are shown in Figure 1-1 (NOAA 2011).

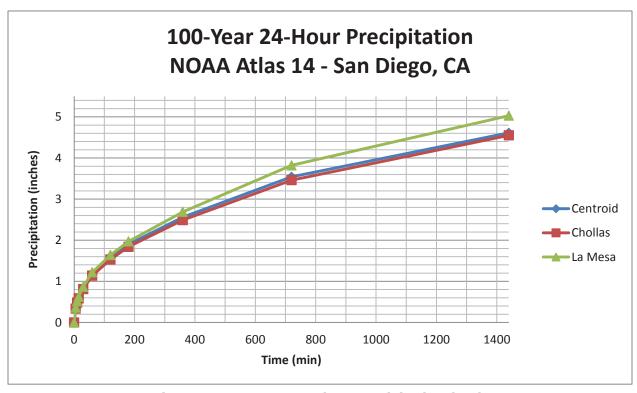


Figure 1-1: 100-year, 24-hour precipitation depth

The resulting rainfall intensity-duration data points generated from the NOAA precipitation depth data were reviewed and plotted for comparison (NOAA 2011). This was done to visually identify any discrepancy in the intensity-duration pairs when plotted. The intensity-duration pairs will appear linear on a log-log scale. The graphs showed that the rainfall intensity-duration relationship yielded a linear relationship for the rainfall data collected at the rain gages, and the precipitation data for the centroid of

the study area was within range of the 2 nearby rain gages (Figure 1-2). This comparison provides a check to verify that the rainfall data obtained directly at the centroid of the City of Lemon Grove study area from the NOAA PFDS correlates with the data at the nearest rain gages in the vicinity of the study area.

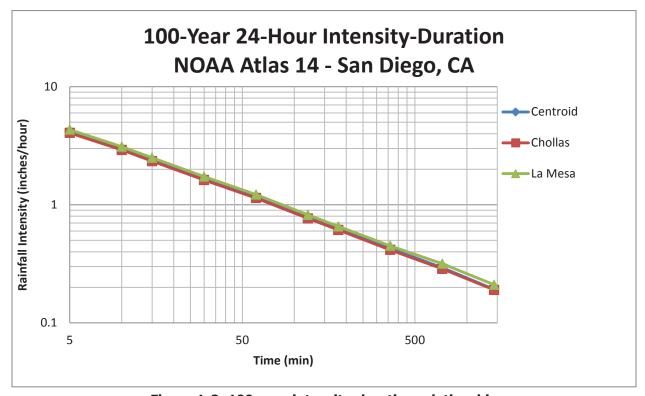


Figure 1-2: 100-year intensity-duration relationship

Since the intensities plotted showed similar patterns for the two gages and the data for the City of Lemon Grove area within range of the data obtained at the rain gages, it was determined that the rainfall data aggregated for the study area would be appropriate for modeling purposes. The precipitation was entered in 5-minute increments. Precipitation depths at certain durations were obtained directly from NOAA Atlas 14 as seen in the rainfall data shown in Appendix A (NOAA 2011). Precipitation depths bounded by the given values were determined by log-log interpolation at 5 minute increments.

The incremental precipitation data was then arranged into a center-distributed rainfall intensity hyetograph with the peak of the storm centered at 12 hours, as seen in Figure 1-3. A (2/3, 1/3) rainfall distribution with the storm peak occurring at 16 hours, as described in the 2003 *San Diego County Hydrology Manual* was considered and ultimately not selected for this study. This approach delivers a greater volume of rainfall prior to the peak of the storm, which has a significant impact on storage volumes on street surfaces and storm drain facilities, compared to the center-distributed balanced storm (1/2, 1/2 distribution). A storm distribution with the peak rainfall intensity arranged at 12 hours generates the necessary peak flows while delivering the full rainfall volume with a symmetric distribution during the 24-hour storm event.

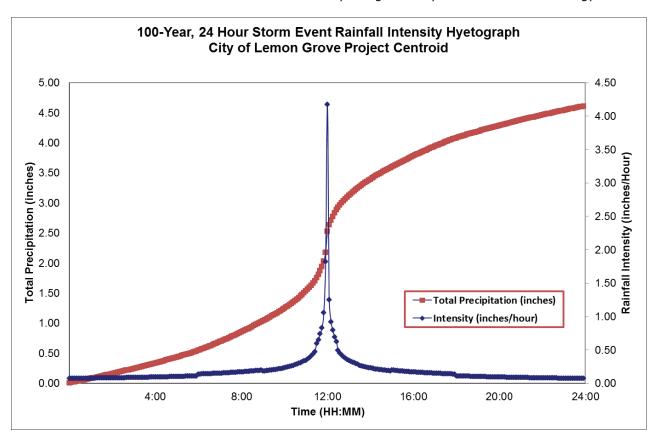


Figure 1-3: 100-year, 24-hour intensity hyetograph

1.1.3 Rainfall Losses

The Green-Ampt Method was used to estimate infiltration potential, which requires the following parameters: soil capillary suction head, soil saturated hydraulic conductivity, and initial moisture deficit (i.e., the difference between soil porosity and initial moisture content). This method is consistent with the guidance presented in the *County of San Diego BMP Design Manual* (2019) for hydromodification management SWMM modeling efforts in San Diego, and further documented in the *Storm Water Management Model User's Manual Version 5.1* (Rossman & Huber, 2015).

Soil parameters were obtained using the listed values in table G.1-4, from Appendix G of the 2019 *County of San Diego BMP Design Manual*. These Green-Ampt soil parameters listed in the table were established by the manual for use in the San Diego Region, and are within the acceptable ranges specified in Tables A.2 and A.3 of the SWMM User's Manual. The distribution of hydrologic soil groups within the City of Lemon Grove study area is based on SANDAG's ArcGIS feature class for National Resources Conservation Service hydrologic soil groups (refer to Appendix A-4 for an exhibit documenting the mapped NRCS hydrologic soil groups within the study area). Areas with an "unknown" soil classification were assumed to be type D soils for this analysis.

The land cover feature class was used to determine the percentage of impervious area for each subcatchment based on assigned impervious percentages to each land use. The land use shapes were intersected with the inlet drainage area delineations to perform an area-weighting analysis of the average impervious cover using GIS tools. Refer to Appendix C for a map which documents the land uses throughout the study area and the assigned impervious percentage for each land use.

To determine the overland Manning's "n" values and percent impervious parameters, the guidance in Appendix G of the 2019 *County of San Diego BMP Design Manual* was followed. The "n" values are: 0.012 for impervious cover, and 0.15 for pervious cover. These values were established by the BMP Design Manual for use in the San Diego region, and are within the acceptable ranges documented in Table 3-5 of the *Storm Water Management Model Reference Manual Volume I – Hydrology* (Rossman 2016).

1.2 Hydrologic Routing

Each subcatchment is connected via a conveyance node and link network (inlets and storm drain pipes), which routes runoff generated towards the storm drain system outfall. Refer to Section 2.0 for more information regarding the hydraulic analysis methodology and modeling procedures.

2.0 Hydraulic Methodology and Modeling

2.1 Flow Routing

The PCSWMM platform uses SWMM5 to perform hydraulic calculations and presents the same flow routing options as the EPA SWMM computer application. This ensures that the input parameters and results obtained are directly compatible between the proprietary PCSWMM program and the public domain EPA SWMM program. Flow routing is governed by the equations of continuity, mass, and momentum—also known as the St. Venant Flow equations—with flexibility offered to the modeler regarding the complexity of the terms considered in the equations. The program allows the modeler to select from the Steady Flow, Kinematic Wave, and Dynamic Wave routing options. The normal depth equation is used in all routing options to relate flow depth, flow rate, and surface friction.

Steady Flow routing was judged to be inappropriate for modeling this study area as it does not actually represent flow routing per a defined time step during the simulation. It is the simplest computation method that translates the inflow hydrographs directly downstream without any change in shape and simply uses the normal depth equations to relate flow rates, depths, and cross-sectional areas of the conveyance network. This method does not represent any backwater effects or pressurized flow, and does not take into account the user-defined computational time steps during the storm simulation.

Kinematic Wave routing was not selected for this study as it was incompatible with the 2-D analysis. It employs a simplified form of the momentum equation but does not take into account all of the equation's terms. This routing method does not account for any backwater effects or pressurized flow.

Dynamic Wave routing was the option selected for all analyses performed in this study. The purpose of this study was to produce a model that would most closely relate the actual conditions of the dynamic relationship between surface and subsurface conveyance, and potential flooding concerns. This routing option considers all terms of the St. Venant Flow equations and presents the most theoretically correct results accounting for backwater effects, pressurized flow, flow attenuation, and reversal of flow. The caveat in selecting this routing option, however, was maintaining numerical stability in the model by using extremely small computational time steps that resulted in significant simulation times for 2-D analyses.

2.2 Conveyance Material and Manning's Roughness Coefficients

The study area was mainly comprised of Reinforced Concrete Pipe (RCP) and cast-in-place concrete pipe (CIPCP) storm drain systems, although a few other storm drain materials (asbestos cement, corrugated metal, and polyvinyl chloride) were also present in the existing inventory. This was determined through examination of the GIS storm drain inventory provided by the City, which was reviewed and updated during the course of the data collection and compilation process described in Section 2 of the DMP.

In PCSWMM (and EPA SWMM), the Manning roughness values are associated with a conveyance material database. Each channel, pipe, and conduit in the 1-D portion of the model must have a material code assigned to it; in that way, the resistance to flow and energy losses along the conduit length can be calculated.

Table 2-1 lists all the material types present within the study area and the associated Manning's "n" value assigned to each material code in the models.

Table 2-1: Conveyance material abbreviations and Manning's roughness coefficients

Material Code	Material Description	Roughness Coefficient
ABS	Acrylonitrile butadiene styrene	0.013
ACP	Asbestos Cement Pipe	0.013
CIPCP	Cast-in-Place Concrete Pipe	0.019
CMP	Corrugated Metal Pipe	0.024
HDPE	High-density polyethylene	0.013
PVC	Polyvinyl Chloride	0.013
RCP/RCB	Reinforced Concrete Pipe/Box	0.013
SP	Steel Pipe	0.024
VCP	Vitrified clay pipe	0.014

The Manning's conduit roughness values were assigned based on Chapter 3 of the *San Diego Hydraulic Design Manual* (2014).

2.3 Storm Water Inlet Modeling

The GIS storm water conveyance dataset which was revised and updated during the course of the data collection and compilation process includes 23 inlet or catch basin structures for the collection of surface runoff from streets, ditches, swales, and overland flow. Undersized storm water inlets can limit the efficiency of the existing conveyance infrastructure to collect and convey runoff during storm events. The flow interception capacity of each inlet type was estimated based on the inlet structure type, location, street slope, and structure dimensions, following the 2014 *County of San Diego Hydraulic Design Manual* guidance (CSDDPW 2014). Note that the 50-percent clogging reduction factor was not applied for grated catch basin inlets. Flow interception at each inlet was included in the PCSWMM model with inflow rating curves as a function of street flow depth. The portion of storm water flows exceeding the capacity of the inlet was bypassed to the street conveyance in the 2-D models.

2.4 Coupled 1-D/2-D Model

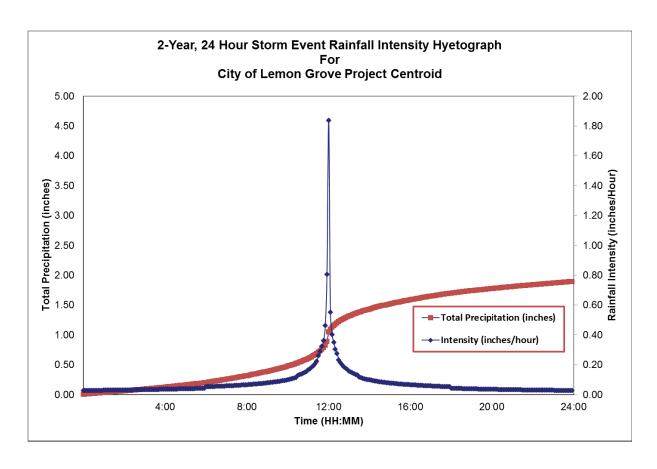
The development of the 1-D hydraulic model includes the pipe/open channel drainage network for all pipes 36 inches and larger. Pertinent pipes having less than 36-inch diameters also were included in the model if they were considered part of the primary backbone storm drain systems. Key hydraulic structures that control the flow entering or discharging from the primary system such as inlets, culverts, outfalls, and pipes also were included in the 1-D model.

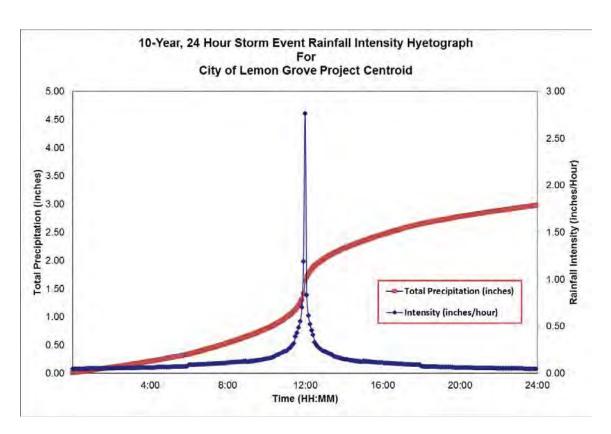
The surface storage and conveyance represented by the streets and other surfaces are accounted for in the 2-D hydraulic model of the City of Lemon Grove study area. The 2-D model was generated from an array of mesh (or grids) with a 10-ft. and 30 ft. resolutions to represent the surface conveyance. A 10-ft. resolution directional mesh was used to define the drainage patterns of streets and roads, and a 30-ft. resolution hexagonal mesh was applied globally to the remaining sections of the study area. The directional mesh generates 2-D surface cells which are forced along a defined preferential flow path, such as a street gutter flowline or alleyway centerline. This is useful for streets and channels. The hexagonal mesh generates 2-D surface cells which have six (6) defined flow directions in order to represent more possible flow directions across surfaces with less defined flow paths. This option is useful for flatter areas that do not have clearly defined flow paths.

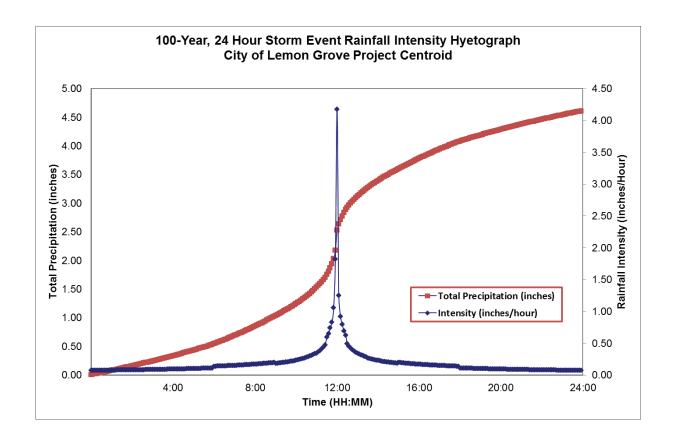
The overall 2-D mesh was developed from a high-resolution DEM data set by sampling elevation data at points with a 10-ft. or 30-ft. spatial resolution and was used to preserve the preferential flow paths and street conveyance that are part of the overall storm water conveyance system.

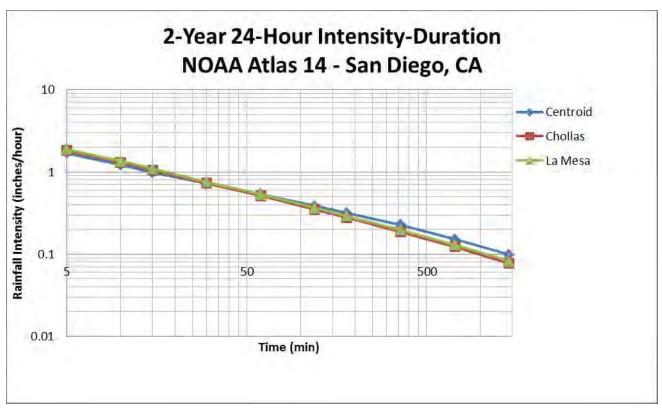
The two systems were coupled together at points where exchange of storm water between the surface conveyance system and the engineered storm water conveyance system could occur—typically at storm drain inlets, and outlet structures. The models were linked between nodes in the 1-D minor system (subsurface) and the 2-D major system (surface). The coupled models were then run and solved simultaneously, representing the storm water conveyance and storage on the street and in the storm water collection and conveyance system. The coupling of the 1-D and 2-D models allowed for bidirectional exchange of volume between the 2-D surface conveyance system and the engineered 1-D storm water system. By coupling the models together and solving the hydraulics simultaneously, the dynamic exchange of runoff between the surface flow and storm water conveyance system facilities is described.

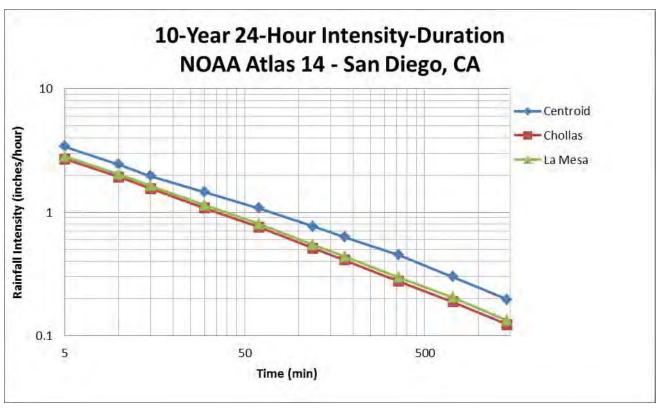
The coupled 1-D/2-D model was executed using the runoff hydrographs resulting from NOAA rainfalls for the 2-, 10-, and 100-year storm events based on existing land uses to assess the current system's deficiencies.

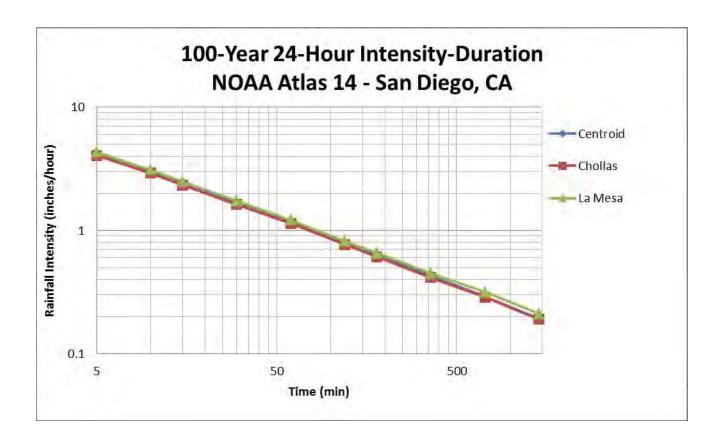












Centroid Data



NOAA Atlas 14, Volume 6, Version 2 Location name: Lemon Grove, California, USA* Latitude: 32.7333°, Longitude: -117.0344° Elevation: 420.08 ft**



* source: ESRI Maps ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS	S-based p	oint preci	ipitation fi	equency	estimates	with 90%	confiden	ce interva	als (in inc	hes) ¹
Duration				Avera	ge recurren	ce interval (years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.121 (0.101-0.146)	0.153 (0.128-0.185)	0.195 (0.163-0.236)	0.230 (0.190-0.280)	0.276 (0.221-0.349)	0.312 (0.244-0.403)	0.348 (0.266-0.462)	0.386 (0.286-0.527)	0.437 (0.309-0.622)	0.476 (0.326-0.703)
10-min	0.173 (0.145-0.209)	0.220 (0.184-0.265)	0.280 (0.234-0.339)	0.329 (0.273-0.402)	0.396 (0.317-0.501)	0.447 (0.350-0.578)	0.500 (0.381-0.662)	0.553 (0.409-0.755)	0.626 (0.444-0.892)	0.682 (0.467-1.01)
15-min	0.210 (0.176-0.253)	0.266 (0.222-0.320)	0.339 (0.283-0.410)	0.398 (0.330-0.486)	0.479 (0.383-0.605)	0.541 (0.423-0.699)	0.604 (0.460-0.801)	0.669 (0.495-0.913)	0.757 (0.536-1.08)	0.825 (0.564-1.22)
30-min	0.291 (0.244-0.350)	0.368 (0.308-0.445)	0.470 (0.392-0.569)	0.553 (0.457-0.674)	0.664 (0.531-0.840)	0.751 (0.587-0.970)	0.838 (0.639-1.11)	0.928 (0.687-1.27)	1.05 (0.744-1.50)	1.15 (0.783-1.69)
60-min	0.409 (0.343-0.493)	0.518 (0.434-0.625)	0.661 (0.552-0.800)	0.777 (0.643-0.949)	0.935 (0.747-1.18)	1.06 (0.825-1.36)	1.18 (0.898-1.56)	1.31 (0.966-1.78)	1.48 (1.05-2.11)	1.61 (1.10-2.38)
2-hr	0.565 (0.474-0.681)	0.710 (0.595-0.857)	0.900 (0.751-1.09)	1.05 (0.872-1.29)	1.26 (1.01-1.60)	1.42 (1.11-1.84)	1.59 (1.21-2.10)	1.75 (1.30-2.39)	1.98 (1.40-2.82)	2.16 (1.48-3.19)
3-hr	0.678 (0.568-0.816)	0.851 (0.713-1.03)	1.08 (0.900-1.31)	1.26 (1.05-1.54)	1.51 (1.21-1.91)	1.70 (1.33-2.20)	1.90 (1.45-2.52)	2.10 (1.55-2.87)	2.37 (1.68-3.38)	2.58 (1.76-3.81)
6-hr	0.894 (0.749-1.08)	1.13 (0.947-1.37)	1.44 (1.20-1.74)	1.69 (1.40-2.07)	2.03 (1.63-2.57)	2.29 (1.79-2.96)	2.56 (1.95-3.39)	2.83 (2.09-3.86)	3.20 (2.27-4.55)	3.48 (2.38-5.14)
12-hr	1.16 (0.971-1.40)	1.50 (1.26-1.81)	1.95 (1.63-2.36)	2.31 (1.91-2.82)	2.79 (2.23-3.53)	3.16 (2.47-4.09)	3.54 (2.69-4.69)	3.92 (2.90-5.35)	4.43 (3.14-6.32)	4.83 (3.30-7.14)
24-hr	1.42 (1.25-1.65)	1.89 (1.65-2.19)	2.49 (2.17-2.90)	2.97 (2.58-3.49)	3.62 (3.05-4.39)	4.11 (3.40-5.08)	4.61 (3.73-5.82)	5.12 (4.03-6.63)	5.80 (4.40-7.81)	6.33 (4.65-8.79)
2-day	1.75 (1.54-2.04)	2.34 (2.05-2.73)	3.10 (2.71-3.62)	3.71 (3.22-4.37)	4.53 (3.81-5.49)	5.15 (4.25-6.36)	5.77 (4.66-7.28)	6.40 (5.04-8.29)	7.24 (5.49-9.74)	7.89 (5.80-11.0)
3-day	1.98 (1.74-2.30)	2.66 (2.33-3.09)	3.52 (3.08-4.11)	4.22 (3.66-4.96)	5.15 (4.33-6.23)	5.85 (4.83-7.22)	6.55 (5.29-8.27)	7.26 (5.72-9.40)	8.21 (6.23-11.0)	8.94 (6.56-12.4)
4-day	2.16 (1.90-2.51)	2.90 (2.54-3.38)	3.85 (3.37-4.50)	4.61 (4.00-5.42)	5.63 (4.74-6.82)	6.39 (5.28-7.90)	7.16 (5.79-9.04)	7.94 (6.25-10.3)	8.98 (6.81-12.1)	9.77 (7.18-13.6)
7-day	2.55 (2.24-2.97)	3.42 (3.00-3.98)	4.54 (3.97-5.29)	5.43 (4.72-6.39)	6.63 (5.58-8.03)	7.54 (6.23-9.31)	8.45 (6.83-10.7)	9.38 (7.39-12.2)	10.6 (8.06-14.3)	11.6 (8.51-16.1)
10-day	2.82 (2.47-3.27)	3.77 (3.30-4.39)	5.00 (4.37-5.83)	5.98 (5.19-7.03)	7.30 (6.15-8.84)	8.30 (6.86-10.2)	9.31 (7.52-11.8)	10.3 (8.14-13.4)	11.7 (8.87-15.7)	12.8 (9.37-17.7)
20-day	3.45 (3.03-4.01)	4.62 (4.05-5.38)	6.12 (5.35-7.14)	7.31 (6.35-8.60)	8.90 (7.50-10.8)	10.1 (8.35-12.5)	11.3 (9.13-14.3)	12.5 (9.86-16.2)	14.1 (10.7-19.0)	15.4 (11.3-21.4)
30-day	4.14 (3.63-4.81)	5.53 (4.84-6.43)	7.29 (6.38-8.51)	8.70 (7.55-10.2)	10.6 (8.89-12.8)	11.9 (9.87-14.8)	13.3 (10.8-16.8)	14.7 (11.6-19.1)	16.6 (12.6-22.3)	18.0 (13.2-25.0)
45-day	4.88 (4.28-5.67)	6.48 (5.68-7.54)	8.50 (7.43-9.92)	10.1 (8.76-11.9)	12.2 (10.3-14.8)	13.7 (11.4-17.0)	15.3 (12.3-19.3)	16.8 (13.3-21.8)	18.9 (14.3-25.4)	20.4 (15.0-28.3)
60-day	5.69 (5.00-6.62)	7.52 (6.59-8.75)	9.80 (8.57-11.4)	11.6 (10.1-13.6)	13.9 (11.7-16.9)	15.6 (12.9-19.3)	17.3 (14.0-21.9)	19.0 (15.0-24.6)	21.2 (16.1-28.6)	22.9 (16.8-31.8)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

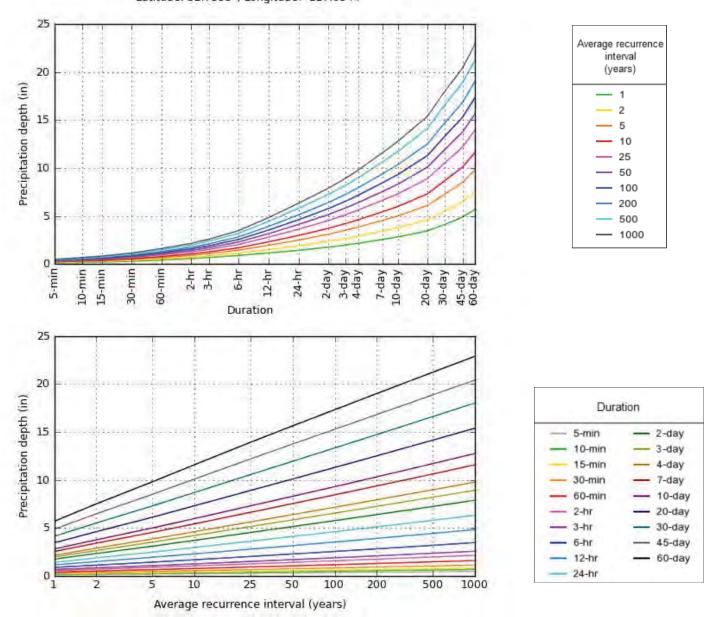
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 32.7333°, Longitude: -117.0344°

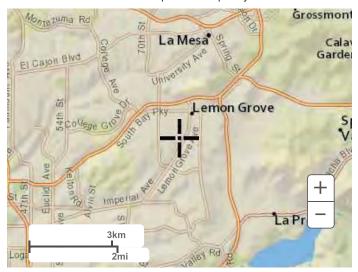


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NOAA Atlas 14, Volume 6, Version 2 Location name: Lemon Grove, California, USA* Latitude: 32.7333°, Longitude: -117.0344° Elevation: 420.08 ft**

.0344°

* source: ESRI Maps ** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹												
					ge recurren				•	<u> </u>			
Duration	1	2	5	10	25	50	100	200	500	1000			
5-min	1.45 (1.21-1.75)	1.84 (1.54-2.22)	2.34 (1.96-2.83)	2.76 (2.28-3.36)	3.31 (2.65-4.19)	3.74 (2.93-4.84)	4.18 (3.19-5.54)	4.63 (3.43-6.32)	5.24 (3.71-7.46)	5.71 (3.91-8.44)			
10-min	1.04 (0.870-1.25)	1.32 (1.10-1.59)	1.68 (1.40-2.03)	1.97 (1.64-2.41)	2.38 (1.90-3.01)	2.68 (2.10-3.47)	3.00 (2.29-3.97)	3.32 (2.45-4.53)	3.76 (2.66-5.35)	4.09 (2.80-6.05)			
15-min	0.840 (0.704-1.01)	1.06 (0.888-1.28)	1.36 (1.13-1.64)	1.59 (1.32-1.94)	1.92 (1.53-2.42)	2.16 (1.69-2.80)	2.42 (1.84-3.20)	2.68 (1.98-3.65)	3.03 (2.14-4.32)	3.30 (2.26-4.88)			
30-min	0.582 (0.488-0.700)	0.736 (0.616-0.890)	0.940 (0.784-1.14)	1.11 (0.914-1.35)	1.33 (1.06-1.68)	1.50 (1.17-1.94)	1.68 (1.28-2.22)	1.86 (1.37-2.53)	2.10 (1.49-2.99)	2.29 (1.57-3.38)			
60-min	0.409 (0.343-0.493)	0.518 (0.434-0.625)	0.661 (0.552-0.800)	0.777 (0.643-0.949)	0.935 (0.747-1.18)	1.06 (0.825-1.36)	1.18 (0.898-1.56)	1.31 (0.966-1.78)	1.48 (1.05-2.11)	1.61 (1.10-2.38)			
2-hr	0.282 (0.237-0.340)	0.355 (0.298-0.428)	0.450 (0.376-0.544)	0.527 (0.436-0.643)	0.632 (0.504-0.798)	0.712 (0.556-0.919)	0.793 (0.604-1.05)	0.877 (0.649-1.20)	0.990 (0.702-1.41)	1.08 (0.738-1.59)			
3-hr	0.226 (0.189-0.272)	0.283 (0.237-0.342)	0.359 (0.300-0.435)	0.421 (0.348-0.513)	0.504 (0.403-0.637)	0.567 (0.444-0.733)	0.632 (0.482-0.838)	0.699 (0.517-0.954)	0.789 (0.559-1.13)	0.859 (0.587-1.27)			
6-hr	0.149 (0.125-0.180)	0.189 (0.158-0.228)	0.241 (0.201-0.291)	0.283 (0.234-0.345)	0.340 (0.271-0.429)	0.383 (0.299-0.495)	0.427 (0.325-0.566)	0.472 (0.350-0.645)	0.534 (0.378-0.761)	0.581 (0.397-0.859)			
12-hr	0.096 (0.081-0.116)	0.125 (0.104-0.150)	0.162 (0.135-0.196)	0.191 (0.159-0.234)	0.232 (0.185-0.293)	0.262 (0.205-0.339)	0.293 (0.224-0.389)	0.325 (0.241-0.444)	0.368 (0.261-0.524)	0.401 (0.274-0.592)			
24-hr	0.059 (0.052-0.069)	0.079 (0.069-0.091)	0.104 (0.091-0.121)	0.124 (0.107-0.146)	0.151 (0.127-0.183)	0.171 (0.142-0.212)	0.192 (0.155-0.243)	0.213 (0.168-0.276)	0.242 (0.183-0.325)	0.264 (0.194-0.366)			
2-day	0.036 (0.032-0.042)	0.049 (0.043-0.057)	0.065 (0.057-0.075)	0.077 (0.067-0.091)	0.094 (0.079-0.114)	0.107 (0.089-0.132)	0.120 (0.097-0.152)	0.133 (0.105-0.173)	0.151 (0.114-0.203)	0.164 (0.121-0.228)			
3-day	0.028 (0.024-0.032)	0.037 (0.032-0.043)	0.049 (0.043-0.057)	0.059 (0.051-0.069)	0.071 (0.060-0.087)	0.081 (0.067-0.100)	0.091 (0.073-0.115)	0.101 (0.079-0.131)	0.114 (0.086-0.153)	0.124 (0.091-0.172)			
4-day	0.023 (0.020-0.026)	0.030 (0.027-0.035)	0.040 (0.035-0.047)	0.048 (0.042-0.056)	0.059 (0.049-0.071)	0.067 (0.055-0.082)	0.075 (0.060-0.094)	0.083 (0.065-0.107)	0.094 (0.071-0.126)	0.102 (0.075-0.141)			
7-day	0.015 (0.013-0.018)	0.020 (0.018-0.024)	0.027 (0.024-0.032)	0.032 (0.028-0.038)	0.039 (0.033-0.048)	0.045 (0.037-0.055)	0.050 (0.041-0.064)	0.056 (0.044-0.072)	0.063 (0.048-0.085)	0.069 (0.051-0.096)			
10-day	0.012 (0.010-0.014)	0.016 (0.014-0.018)	0.021 (0.018-0.024)	0.025 (0.022-0.029)	0.030 (0.026-0.037)	0.035 (0.029-0.043)	0.039 (0.031-0.049)	0.043 (0.034-0.056)	0.049 (0.037-0.066)	0.053 (0.039-0.074)			
20-day	0.007 (0.006-0.008)	0.010 (0.008-0.011)	0.013 (0.011-0.015)	0.015 (0.013-0.018)	0.019 (0.016-0.022)	0.021 (0.017-0.026)	0.024 (0.019-0.030)	0.026 (0.021-0.034)	0.029 (0.022-0.040)	0.032 (0.024-0.045)			
30-day	0.006 (0.005-0.007)	0.008 (0.007-0.009)	0.010 (0.009-0.012)	0.012 (0.010-0.014)	0.015 (0.012-0.018)	0.017 (0.014-0.020)	0.019 (0.015-0.023)	0.020 (0.016-0.026)	0.023 (0.017-0.031)	0.025 (0.018-0.035)			
45-day	0.005 (0.004-0.005)	0.006 (0.005-0.007)	0.008 (0.007-0.009)	0.009 (0.008-0.011)	0.011 (0.010-0.014)	0.013 (0.011-0.016)	0.014 (0.011-0.018)	0.016 (0.012-0.020)	0.017 (0.013-0.024)	0.019 (0.014-0.026)			
60-day	0.004 (0.003-0.005)	0.005 (0.005-0.006)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.010 (0.008-0.012)	0.011 (0.009-0.013)	0.012 (0.010-0.015)	0.013 (0.010-0.017)	0.015 (0.011-0.020)	0.016 (0.012-0.022)			

 $^{^{1}}$ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

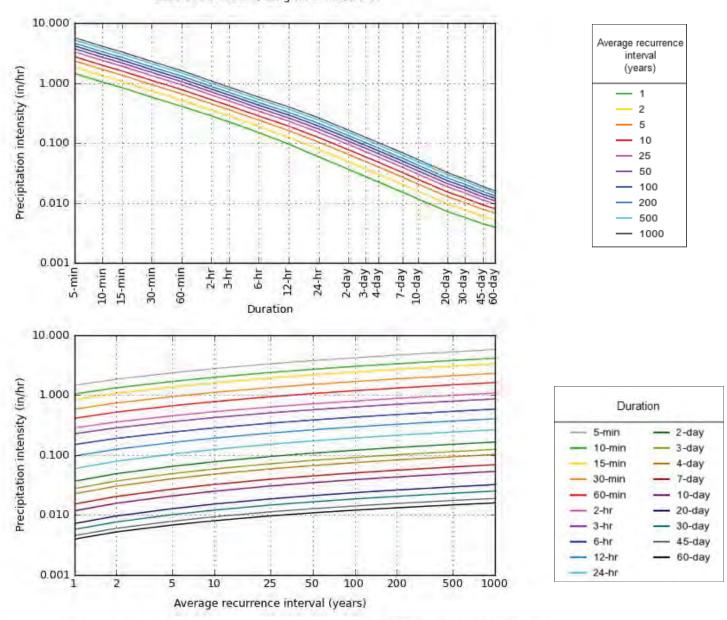
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based intensity-duration-frequency (IDF) curves Latitude: 32.7333°, Longitude: -117.0344°

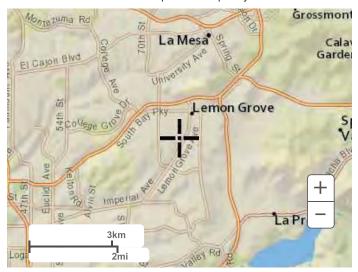


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Chollas Data

NOAA Atlas 14, Volume 6, Version 2 CHOLLAS RESERVOIR



Station ID: 92-0510 Location name: San Diego, California, USA* Latitude: 32.7333°, Longitude: -117.0667°





POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

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PF tabular

-	FF tabulal												
PD	S-based p	oint prec	ipitation f			with 90%		ce interva	als (in inc	hes) ¹			
Duration				Avera	ge recurren	ce interval (years)						
Duration	1	2	5	10	25	50	100	200	500	1000			
5-min	0.120 (0.101-0.145)	0.152 (0.127-0.183)	0.192 (0.160-0.232)	0.225 (0.186-0.275)	0.269 (0.215-0.341)	0.304 (0.237-0.392)	0.338 (0.258-0.448)	0.374 (0.277-0.510)	0.422 (0.299-0.601)	0.459 (0.314-0.678)			
10-min	0.173 (0.145-0.208)	0.217 (0.182-0.262)	0.275 (0.230-0.333)	0.322 (0.267-0.394)	0.386 (0.309-0.488)	0.435 (0.340-0.562)	0.485 (0.369-0.643)	0.536 (0.396-0.731)	0.604 (0.428-0.861)	0.657 (0.449-0.972)			
15-min	0.209 (0.175-0.252)	0.263 (0.220-0.317)	0.333 (0.278-0.403)	0.390 (0.323-0.476)	0.467 (0.373-0.591)	0.526 (0.411-0.680)	0.586 (0.447-0.777)	0.648 (0.479-0.884)	0.731 (0.518-1.04)	0.795 (0.544-1.18)			
30-min	0.289 (0.242-0.349)	.289 0.364 0.461 0.540 0.647 0.729		0.729 (0.570-0.942)	0.812 (0.619-1.08)	0.897 (0.664-1.23)	1.01 (0.717-1.44)	1.10 (0.753-1.63)					
60-min	0.407		1.14 (0.870-1.51)	1.26 (0.934-1.72)	1.42 (1.01-2.03)	1.55 (1.06-2.29)							
2-hr	0.562 (0.471-0.677)	0.699 (0.585-0.843)	0.878 (0.733-1.06)	1.02 (0.847-1.25)	1.22 (0.977-1.55)	1.38 (1.08-1.78)	1.53 (1.17-2.03)	1.69 (1.25-2.31)	1.91 (1.36-2.73)	2.08 (1.42-3.08)			
3-hr	0.673 (0.564-0.811)	0.837 (0.700-1.01)	1.05 (0.878-1.27)	1.23 (1.02-1.50)	1.47 (1.17-1.86)	1.65 (1.29-2.13)	1.84 (1.40-2.44)	2.03 (1.50-2.77)	2.29 (1.63-3.27)	2.50 (1.71-3.69)			
6-hr	0.884 (0.741-1.07)	1.11 (0.931-1.34)	1.41 (1.18-1.71)	1.65 (1.37-2.02)	1.98 (1.58-2.50)	2.23 (1.74-2.88)	2.49 (1.90-3.30)	2.75 (2.04-3.75)	3.11 (2.20-4.43)	3.38 (2.31-5.00)			
12-hr	1.13 (0.950-1.37)	1.48 (1.24-1.78)	1.92 (1.60-2.32)	2.27 (1.88-2.77)	2.74 (2.19-3.47)	3.10 (2.42-4.01)	3.46 (2.64-4.59)	3.82 (2.83-5.22)	4.31 (3.05-6.14)	4.68 (3.20-6.92)			
24-hr	1.37 (1.20-1.60)	1.85 (1.63-2.16)	2.47 (2.16-2.88)	2.95 (2.56-3.47)	3.59 (3.03-4.36)	4.07 (3.37-5.03)	4.55 (3.67-5.74)	5.03 (3.96-6.51)	5.65 (4.29-7.61)	6.13 (4.50-8.52)			
2-day	1.68 (1.47-1.95)	2.29 (2.00-2.66)	3.06 (2.67-3.57)	3.67 (3.18-4.32)	4.47 (3.77-5.42)	5.08 (4.19-6.27)	5.67 (4.58-7.16)	6.27 (4.93-8.12)	7.05 (5.35-9.49)	7.65 (5.62-10.6)			
3-day	1.90 (1.67-2.21)	2.59 (2.27-3.02)	3.47 (3.03-4.04)	4.16 (3.61-4.89)	5.07 (4.27-6.15)	5.75 (4.75-7.11)	6.43 (5.19-8.12)	7.11 (5.60-9.21)	8.00 (6.06-10.8)	8.67 (6.37-12.0)			
4-day	2.08 (1.82-2.42)	2.83 (2.48-3.30)	3.79 (3.31-4.42)	4.54 (3.94-5.34)	5.54 (4.67-6.72)	6.29 (5.20-7.77)	7.03 (5.68-8.88)	7.77 (6.12-10.1)	8.75 (6.64-11.8)	9.49 (6.97-13.2)			
7-day	2.46 (2.16-2.86)	3.33 (2.92-3.88)	4.44 (3.88-5.19)	5.33 (4.62-6.27)	6.50 (5.48-7.88)	7.39 (6.10-9.12)	8.26 (6.68-10.4)	9.15 (7.21-11.9)	10.3 (7.83-13.9)	11.2 (8.24-15.6)			
10-day	2.72 (2.38-3.16)	3.67 (3.21-4.27)	4.88 (4.26-5.69)	5.85 (5.07-6.87)	7.13 (6.00-8.64)	8.10 (6.69-10.00)	9.06 (7.32-11.4)	10.0 (7.90-13.0)	11.3 (8.59-15.2)	12.3 (9.04-17.1)			
20-day	3.34 (2.93-3.89)	4.49 (3.93-5.23)	5.95 (5.20-6.94)	7.11 (6.17-8.36)	8.64 (7.27-10.5)	9.78 (8.08-12.1)	10.9 (8.82-13.8)	12.1 (9.51-15.6)	13.6 (10.3-18.3)	14.7 (10.8-20.5)			
30-day	4.01 (3.52-4.66)	5.36 (4.70-6.24)	7.07 (6.18-8.25)	8.41 (7.30-9.89)	10.2 (8.57-12.3)	11.5 (9.50-14.2)	12.8 (10.3-16.2)	14.1 (11.1-18.3)	15.8 (12.0-21.3)	17.1 (12.6-23.8)			
45-day	4.73 (4.15-5.50)	6.26 (5.49-7.29)	8.19 (7.16-9.56)	9.70 (8.42-11.4)	11.7 (9.83-14.1)	13.1 (10.8-16.2)	14.6 (11.8-18.4)	16.0 (12.6-20.7)	17.8 (13.5-24.0)	19.2 (14.1-26.7)			
60-day	5.55 (4.87-6.45)	7.28 (6.38-8.48)	9.45 (8.26-11.0)	11.1 (9.66-13.1)	13.3 (11.2-16.1)	14.9 (12.3-18.4)	16.5 (13.3-20.8)	18.0 (14.2-23.3)	20.0 (15.2-26.9)	21.5 (15.8-29.9)			

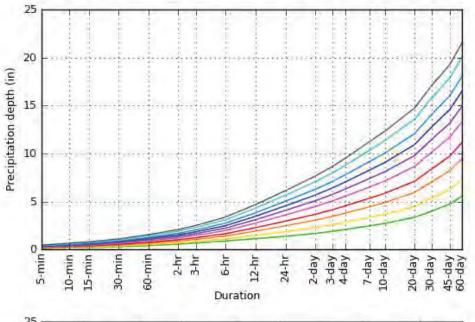
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

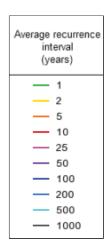
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

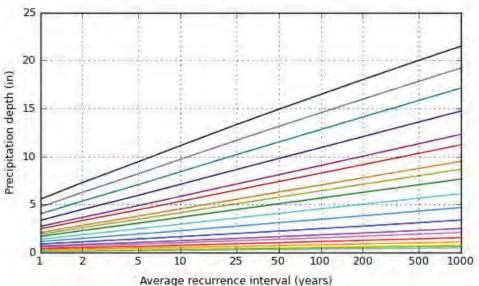
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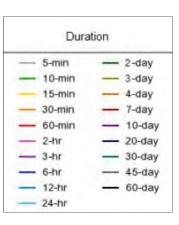
PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 32.7333°, Longitude: -117.0667°









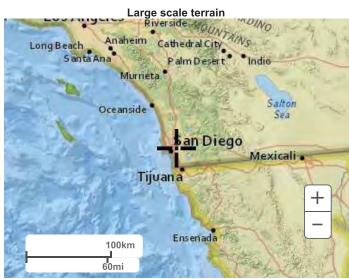
NOAA Atlas 14, Volume 6, Version 2

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NOAA Atlas 14, Volume 6, Version 2 Location name: San Diego, California, USA* Latitude: 32.7333°, Longitude: -117.0667° Elevation: 445.15 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹												
Duration				Avera	ge recurren	ce interval (years)						
Duration	1	2	5	10	25	50	100	200	500	1000			
5-min	1.44 (1.21-1.74)	1.82 (1.52-2.20)	2.30 (1.92-2.78)	2.70 (2.23-3.30)	3.23 (2.58-4.09)	3.65 (2.84-4.70)	4.06 (3.10-5.38)	4.49 (3.32-6.12)	5.06 (3.59-7.21)	5.51 (3.77-8.14)			
10-min	1.04 (0.870-1.25)	1.30 (1.09-1.57)	1.65 (1.38-2.00)	1.93 (1.60-2.36)	2.32 (1.85-2.93)	2.61 (2.04-3.37)	2.91 (2.21-3.86)	3.22 (2.38-4.39)	3.62 (2.57-5.17)	3.94 (2.69-5.83)			
15-min	min 0.836 (0.700-1.01) 1.05 (0.880-1.27) 1.33 (1.11-1.61) 1.29-1.90)		1.87 (1.49-2.36)	2.10 (1.64-2.72)	2.34 (1.79-3.11)	2.59 (1.92-3.54)	2.92 (2.07-4.17)	3.18 (2.18-4.70)					
30-min	0.578 (0.484-0.698)	0.728 (0.608-0.878)	0.922 (0.770-1.12)	1.08 (0.894-1.32)	1.29 (1.03-1.64)	1.46 (1.14-1.88)	1.62 (1.24-2.15)	1.79 (1.33-2.45)	2.02 (1.43-2.89)	2.20 (1.51-3.25)			
60-min	0.407 (0.341-0.490)	0.511 (0.428-0.617)	0.648 (0.541-0.785)	0.759 (0.628-0.927)	0.910 (0.727-1.15)	1.02 (0.801-1.33)	1.14 (0.870-1.51)	1.26 (0.934-1.72)	1.42 (1.01-2.03)	1.55 (1.06-2.29)			
2-hr	0.281 (0.236-0.338)	0.350 (0.292-0.422)	0.439 (0.366-0.532)	0.512 (0.424-0.625)	0.612 (0.488-0.773)	0.688 (0.538-0.890)	0.766 (0.584-1.02)	0.847 (0.627-1.16)	0.956 (0.678-1.36)	1.04 (0.712-1.54)			
3-hr	0.224 (0.188-0.270)	0.279 (0.233-0.336)	0.350 (0.292-0.424)	0.409 (0.338-0.499)	0.489 (0.390-0.618)	0.550 (0.430-0.710)	0.612 (0.466-0.812)	0.676 (0.500-0.923)	0.764 (0.541-1.09)	0.832 (0.569-1.23)			
6-hr	0.148 (0.124-0.178)	0.186 (0.155-0.224)	0.235 (0.196-0.285)	0.276 (0.228-0.337)	0.331 (0.264-0.418)	0.373 (0.291-0.482)	0.415 (0.316-0.551)	0.459 (0.340-0.627)	0.519 (0.367-0.739)	0.565 (0.386-0.834)			
12-hr	0.094 (0.079-0.113)	0.123 (0.103-0.148)	0.159 (0.133-0.193)	0.188 (0.156-0.230)	0.228 (0.182-0.288)	0.257 (0.201-0.333)	0.287 (0.219-0.381)	0.317 (0.235-0.433)	0.358 (0.253-0.510)	0.389 (0.266-0.574)			
24-hr	0.057 (0.050-0.067)	0.077 (0.068-0.090)	0.103 (0.090-0.120)	0.123 (0.107-0.145)	0.150 (0.126-0.182)	0.170 (0.140-0.210)	0.190 (0.153-0.239)	0.209 (0.165-0.271)	0.236 (0.179-0.317)	0.255 (0.188-0.355)			
2-day	0.035 (0.031-0.041)	0.048 (0.042-0.055)	0.064 (0.056-0.074)	0.076 (0.066-0.090)	0.093 (0.078-0.113)	0.106 (0.087-0.131)	0.118 (0.095-0.149)	0.131 (0.103-0.169)	0.147 (0.111-0.198)	0.159 (0.117-0.221)			
3-day	0.026 (0.023-0.031)	0.036 (0.032-0.042)	0.048 (0.042-0.056)	0.058 (0.050-0.068)	0.070 (0.059-0.085)	0.080 (0.066-0.099)	0.089 (0.072-0.113)	0.099 (0.078-0.128)	0.111 (0.084-0.150)	0.120 (0.088-0.167)			
4-day	0.022 (0.019-0.025)	0.029 (0.026-0.034)	0.039 (0.034-0.046)	0.047 (0.041-0.056)	0.058 (0.049-0.070)	0.066 (0.054-0.081)	0.073 (0.059-0.092)	0.081 (0.064-0.105)	0.091 (0.069-0.123)	0.099 (0.073-0.137)			
7-day	0.015 (0.013-0.017)	0.020 (0.017-0.023)	0.026 (0.023-0.031)	0.032 (0.028-0.037)	0.039 (0.033-0.047)	0.044 (0.036-0.054)	0.049 (0.040-0.062)	0.054 (0.043-0.071)	0.061 (0.047-0.083)	0.067 (0.049-0.093)			
10-day	0.011 (0.010-0.013)	0.015 (0.013-0.018)	0.020 (0.018-0.024)	0.024 (0.021-0.029)	0.030 (0.025-0.036)	0.034 (0.028-0.042)	0.038 (0.030-0.048)	0.042 (0.033-0.054)	0.047 (0.036-0.064)	0.051 (0.038-0.071)			
20-day	0.007 (0.006-0.008)	0.009 (0.008-0.011)	0.012 (0.011-0.014)	0.015 (0.013-0.017)	0.018 (0.015-0.022)	0.020 (0.017-0.025)	0.023 (0.018-0.029)	0.025 (0.020-0.033)	0.028 (0.021-0.038)	0.031 (0.023-0.043)			
30-day	0.006 (0.005-0.006)	0.007 (0.007-0.009)	0.010 (0.009-0.011)	0.012 (0.010-0.014)	0.014 (0.012-0.017)	0.016 (0.013-0.020)	0.018 (0.014-0.022)	0.020 (0.015-0.025)	0.022 (0.017-0.030)	0.024 (0.017-0.033)			
45-day	0.004 (0.004-0.005)	0.006 (0.005-0.007)	0.008 (0.007-0.009)	0.009 (0.008-0.011)	0.011 (0.009-0.013)	0.012 (0.010-0.015)	0.013 (0.011-0.017)	0.015 (0.012-0.019)	0.017 (0.013-0.022)	0.018 (0.013-0.025)			
60-day	0.004 (0.003-0.004)	0.005 (0.004-0.006)	0.007 (0.006-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.011)	0.010 (0.009-0.013)	0.011 (0.009-0.014)	0.013 (0.010-0.016)	0.014 (0.011-0.019)	0.015 (0.011-0.021)			

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

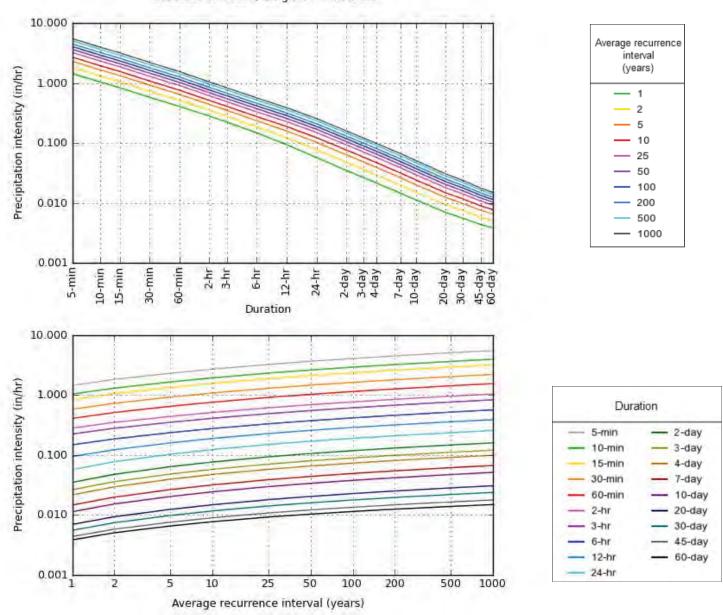
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based intensity-duration-frequency (IDF) curves Latitude: 32.7333°, Longitude: -117.0667°



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La Mesa Data



NOAA Atlas 14, Volume 6, Version 2 Location name: La Mesa, California, USA* Latitude: 32.7675°, Longitude: -117.0233° Elevation: 533.01 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

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PF tabular

PD	S-based p	oint preci	pitation f	requency	estimates	with 90%	confider	ce interva	als (in inc	hes) ¹
Duration				Avera	ge recurren	ce interval (years)			
Burution	1	2	5	10	25	50	100	200	500	1000
5-min	0.123 (0.103-0.148)	0.157 (0.132-0.189)	0.201 (0.168-0.243)	0.237 (0.196-0.289)	0.286 (0.229-0.361)	0.323 (0.253-0.417)	0.360 (0.275-0.478)	0.399 (0.295-0.544)	0.451 (0.320-0.643)	0.491 (0.336-0.725)
10-min	0.176 (0.148-0.212)	0.225 (0.189-0.271)	0.289 (0.241-0.349)	0.340 (0.282-0.415)	0.410 (0.328-0.517)	0.463 (0.362-0.598)	0.517 (0.394-0.685)	0.572 (0.423-0.780)	0.646 (0.458-0.921)	0.704 (0.481-1.04)
15-min	0.213 (0.179-0.257)	0.272 (0.228-0.328)	0.349 (0.292-0.422)	0.411 (0.341-0.502)	0.495 (0.396-0.626)	0.560 (0.438-0.723)	0.625 (0.476-0.828)	0.692 (0.512-0.944)	0.782 (0.554-1.11)	0.851 (0.582-1.26)
30-min	0.296 (0.248-0.356)	0.378 (0.316-0.455)	0.484 (0.404-0.585)	0.571 (0.473-0.696)	0.687 (0.550-0.868)	0.777 (0.608-1.00)	0.867 (0.661-1.15)	0.960 (0.710-1.31)	1.08 (0.769-1.55)	1.18 (0.807-1.75)
60-min	0.417 (0.350-0.502)	0.532 (0.446-0.642)	0.682 (0.570-0.825)	0.804 (0.666-0.981)	0.969 (0.775-1.22)	1.09 (0.856-1.41)	1.22 (0.931-1.62)	1.35 (1.00-1.85)	1.53 (1.08-2.18)	1.66 (1.14-2.46)
2-hr	0.577 (0.484-0.694)	0.730 (0.611-0.880)	0.929 (0.776-1.12)	1.09 (0.903-1.33)	1.31 (1.05-1.65)	1.47 (1.15-1.90)	1.64 (1.25-2.17)	1.81 (1.34-2.48)	2.05 (1.45-2.92)	2.22 (1.52-3.29)
3-hr	0.691 (0.580-0.833)	0.875 (0.733-1.06)	1.12 (0.931-1.35)	1.31 (1.08-1.60)	1.57 (1.25-1.98)	1.77 (1.38-2.28)	1.97 (1.50-2.61)	2.18 (1.61-2.97)	2.45 (1.74-3.50)	2.67 (1.82-3.94)
6-hr	0.916 (0.769-1.10)	1.17 (0.982-1.41)	1.50 (1.26-1.82)	1.77 (1.47-2.16)	2.13 (1.71-2.69)	2.41 (1.88-3.11)	2.69 (2.05-3.56)	2.97 (2.20-4.05)	3.35 (2.38-4.78)	3.65 (2.49-5.39)
12-hr	1.18 (0.989-1.42)	1.56 (1.31-1.89)	2.06 (1.72-2.49)	2.46 (2.04-3.00)	3.00 (2.40-3.79)	3.41 (2.66-4.40)	3.82 (2.91-5.06)	4.24 (3.14-5.78)	4.80 (3.40-6.84)	5.23 (3.58-7.73)
24-hr	1.44 (1.27-1.68)	1.97 (1.72-2.29)	2.64 (2.31-3.08)	3.19 (2.77-3.74)	3.92 (3.30-4.74)	4.47 (3.70-5.52)	5.03 (4.07-6.35)	5.60 (4.42-7.26)	6.37 (4.83-8.57)	6.96 (5.11-9.67)
2-day	1.82 (1.60-2.12)	2.43 (2.13-2.83)	3.22 (2.82-3.76)	3.87 (3.36-4.54)	4.74 (3.99-5.74)	5.40 (4.47-6.67)	6.07 (4.91-7.67)	6.76 (5.33-8.76)	7.69 (5.84-10.4)	8.41 (6.18-11.7)
3-day	2.09 (1.83-2.43)	2.75 (2.41-3.20)	3.61 (3.16-4.21)	4.32 (3.75-5.07)	5.27 (4.44-6.38)	6.00 (4.96-7.40)	6.74 (5.45-8.51)	7.50 (5.91-9.71)	8.53 (6.47-11.5)	9.33 (6.85-13.0)
4-day	2.29 (2.01-2.66)	3.00 (2.63-3.49)	3.93 (3.44-4.58)	4.68 (4.07-5.50)	5.71 (4.81-6.91)	6.49 (5.37-8.02)	7.29 (5.90-9.21)	8.12 (6.40-10.5)	9.24 (7.00-12.4)	10.1 (7.42-14.0)
7-day	2.72 (2.39-3.17)	3.56 (3.13-4.14)	4.66 (4.08-5.43)	5.56 (4.83-6.53)	6.78 (5.71-8.20)	7.71 (6.38-9.52)	8.67 (7.01-10.9)	9.65 (7.61-12.5)	11.0 (8.33-14.8)	12.0 (8.84-16.7)
10-day	2.99 (2.63-3.47)	3.92 (3.44-4.57)	5.15 (4.51-6.00)	6.15 (5.34-7.22)	7.50 (6.32-9.08)	8.54 (7.06-10.5)	9.60 (7.76-12.1)	10.7 (8.43-13.9)	12.2 (9.24-16.4)	13.3 (9.79-18.5)
20-day	3.63 (3.19-4.22)	4.82 (4.23-5.60)	6.36 (5.57-7.42)	7.62 (6.62-8.95)	9.32 (7.85-11.3)	10.6 (8.78-13.1)	11.9 (9.65-15.1)	13.3 (10.5-17.2)	15.1 (11.5-20.3)	16.5 (12.1-22.9)
30-day	4.31 (3.79-5.01)	5.76 (5.05-6.70)	7.64 (6.69-8.91)	9.16 (7.96-10.8)	11.2 (9.44-13.6)	12.8 (10.5-15.8)	14.3 (11.6-18.1)	15.9 (12.6-20.6)	18.1 (13.7-24.3)	19.7 (14.5-27.4)
45-day	5.04 (4.42-5.85)	6.77 (5.94-7.87)	9.00 (7.88-10.5)	10.8 (9.37-12.7)	13.2 (11.1-16.0)	15.0 (12.4-18.5)	16.8 (13.6-21.2)	18.6 (14.7-24.2)	21.1 (16.0-28.4)	23.0 (16.9-31.9)
60-day	5.83 (5.12-6.77)	7.85 (6.89-9.13)	10.4 (9.13-12.2)	12.5 (10.9-14.7)	15.3 (12.9-18.5)	17.3 (14.3-21.4)	19.4 (15.7-24.5)	21.5 (16.9-27.8)	24.2 (18.4-32.6)	26.3 (19.4-36.6)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

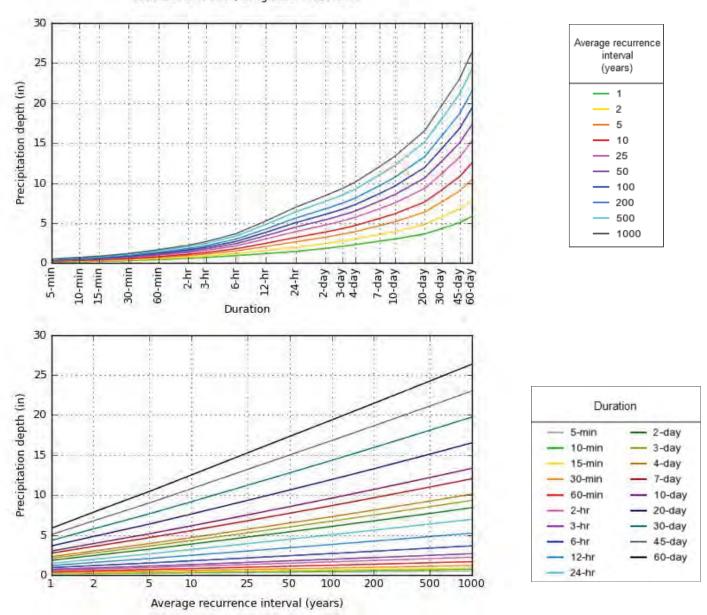
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Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 32.7675°, Longitude: -117.0233°



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NOAA Atlas 14, Volume 6, Version 2 LA MESA Station ID: 04-4735 Location name: La Mesa, California, USA* Latitude: 32.7675°, Longitude: -117.0233° Elevation:



Elevation (station metadata): 530 ft**

* source: ESRI Maps

** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

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PF tabular

DD0:	S-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹												
PDS-b	ased poir	nt precipit	ation freq					intervals	(in inches	s/hour) '			
Duration	1	2	5	10	25	ce interval (100	200	500	1000			
E main	1.48	1.88	2.41	2.84	3.43	3.88	4.32	4.79	5.41	5.89			
5-min	(1.24-1.78)	(1.58-2.27)	(2.02-2.92)	(2.35-3.47)	(2.75-4.33)	(3.04-5.00)	(3.30-5.74)	(3.54-6.53)	(3.84-7.72)	(4.03-8.70)			
10-min	1.06 (0.888-1.27)	1.35 (1.13-1.63)	1.73 (1.45-2.09)	2.04 (1.69-2.49)	2.46 (1.97-3.10)	2.78 (2.17-3.59)	3.10 (2.36-4.11)	3.43 (2.54-4.68)	3.88 (2.75-5.53)	4.22 (2.89-6.24)			
15-min	0.852 (0.716-1.03)	1.09 (0.912-1.31)				2.24 (1.75-2.89)	2.50 (1.90-3.31)	2.77 (2.05-3.78)	3.13 (2.22-4.46)	3.40 (2.33-5.03)			
30-min	0.592 0.756 0.968 1.14 1.37 (0.496-0.712) (0.632-0.910) (0.808-1.17) (0.946-1.39) (1.10-1.74) (3.406-1.39)		1.55 (1.22-2.01)	1.73 (1.32-2.30)	1.92 (1.42-2.62)	2.17 (1.54-3.09)	2.36 (1.61-3.49)						
60-min	0.417 0.532 0.682 0.804 0.969 1.09		1.22 (0.931-1.62)	1.35 (1.00-1.85)	1.53 (1.08-2.18)	1.66 (1.14-2.46)							
2-hr	0.288 (0.242-0.347)	0.365 (0.306-0.440)	0.464 (0.388-0.562)	0.545 (0.452-0.664)	0.654 (0.523-0.826)	0.737 (0.576-0.952)	0.821 (0.626-1.09)	0.907 (0.672-1.24)	1.02 (0.725-1.46)	1.11 (0.760-1.64)			
3-hr	0.230 (0.193-0.277)	0.291 (0.244-0.352)	0.371 (0.310-0.449)	0.436 (0.361-0.531)	0.523 (0.418-0.660)	0.589 (0.461-0.761)	0.656 (0.500-0.869)	0.725 (0.536-0.989)	0.817 (0.579-1.16)	0.888 (0.607-1.31)			
6-hr	0.153 (0.128-0.184)	0.196 (0.164-0.236)	0.251 (0.210-0.304)	0.296 (0.245-0.361)	0.356 (0.285-0.450)	0.402 (0.315-0.519)	0.449 (0.342-0.594)	0.496 (0.367-0.677)	0.560 (0.397-0.798)	0.609 (0.416-0.900			
12-hr	0.098 (0.082-0.118)	0.130 (0.109-0.156)	0.171 (0.143-0.207)	0.204 (0.169-0.249)	0.249 (0.199-0.314)	0.283 (0.221-0.365)	0.317 (0.242-0.420)	0.352 (0.260-0.480)	0.398 (0.282-0.568)	0.434 (0.297-0.641			
24-hr	0.060 (0.053-0.070)	0.082 (0.072-0.095)	0.110 (0.096-0.128)	0.133 (0.115-0.156)	0.163 (0.138-0.198)	0.186 (0.154-0.230)	0.210 (0.170-0.265)	0.234 (0.184-0.302)	0.265 (0.201-0.357)	0.290 (0.213-0.403			
2-day	0.038 (0.033-0.044)	0.051 (0.044-0.059)	0.067 (0.059-0.078)	0.081 (0.070-0.095)	0.099 (0.083-0.119)	0.113 (0.093-0.139)	0.127 (0.102-0.160)	0.141 (0.111-0.182)	0.160 (0.122-0.216)	0.175 (0.129-0.243			
3-day	0.029 (0.025-0.034)	0.038 (0.034-0.044)	0.050 (0.044-0.059)	0.060 (0.052-0.070)	0.073 (0.062-0.089)	0.083 (0.069-0.103)	0.094 (0.076-0.118)	0.104 (0.082-0.135)	0.118 (0.090-0.159)	0.130 (0.095-0.180			
4-day	0.024 (0.021-0.028)	0.031 (0.027-0.036)	0.041 (0.036-0.048)	0.049 (0.042-0.057)	0.059 (0.050-0.072)	0.068 (0.056-0.083)	0.076 (0.061-0.096)	0.085 (0.067-0.110)	0.096 (0.073-0.129)	0.105 (0.077-0.146			
7-day	0.016 (0.014-0.019)	0.021 (0.019-0.025)	0.028 (0.024-0.032)	0.033 (0.029-0.039)	0.040 (0.034-0.049)	0.046 (0.038-0.057)	0.052 (0.042-0.065)	0.057 (0.045-0.074)	0.065 (0.050-0.088)	0.072 (0.053-0.099			
10-day	0.012 (0.011-0.014)	0.016 (0.014-0.019)	0.021 (0.019-0.025)	0.026 (0.022-0.030)	0.031 (0.026-0.038)	0.036 (0.029-0.044)	0.040 (0.032-0.051)	0.045 (0.035-0.058)	0.051 (0.038-0.068)	0.056 (0.041-0.077			
20-day	0.008 (0.007-0.009)	0.010 (0.009-0.012)	0.013 (0.012-0.015)	0.016 (0.014-0.019)	0.019 (0.016-0.024)	0.022 (0.018-0.027)	0.025 (0.020-0.031)	0.028 (0.022-0.036)	0.031 (0.024-0.042)	0.034 (0.025-0.048			
30-day	0.006 (0.005-0.007)	0.008 (0.007-0.009)	0.011 (0.009-0.012)	0.013 (0.011-0.015)	0.016 (0.013-0.019)	0.018 (0.015-0.022)	0.020 (0.016-0.025)	0.022 (0.017-0.029)	0.025 (0.019-0.034)	0.027 (0.020-0.038			
45-day	0.005 (0.004-0.005)	0.006 (0.005-0.007)	0.008 (0.007-0.010)	0.010 (0.009-0.012)	0.012 (0.010-0.015)	0.014 (0.011-0.017)	0.016 (0.013-0.020)	0.017 (0.014-0.022)	0.020 (0.015-0.026)	0.021 (0.016-0.030			
60-day	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.007 (0.006-0.008)	0.009 (0.008-0.010)	0.011 (0.009-0.013)	0.012 (0.010-0.015)	0.013 (0.011-0.017)	0.015 (0.012-0.019)	0.017 (0.013-0.023)	0.018 (0.013-0.025			

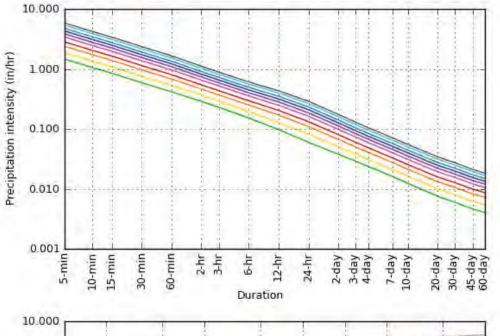
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

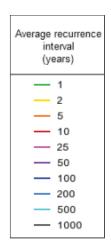
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

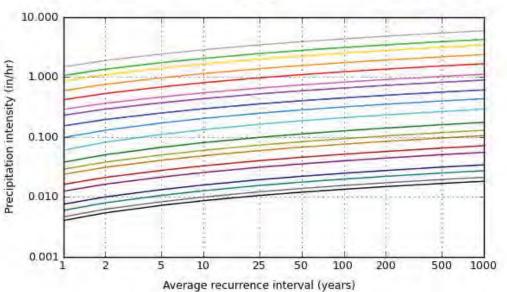
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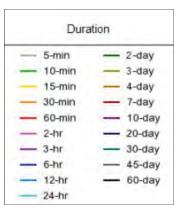
PF graphical

PDS-based intensity-duration-frequency (IDF) curves Latitude: 32.7675°, Longitude: -117.0233°









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Large scale aerial



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B. CCTV Data

CCTV PACP Rating and Repair Recommendation Summary Table

Item	Setup	PSR	From MH	То МН	Length (ft)	Diameter (in)	Structural Rating	Operation & Maintenance Rating	Overall Rating	* Recommended Repair (See repair technique form for numerical definitions)	Notes/Comments/Recommendations
1	115	ST-STR-871	ST-STR-871	ST-STR-973	204.5	42	573G	3222	573G	5,1	Pipe in bad condition, rehabilitation is recommended.
2	120	ST-STR-1047	ST-STR-1430	ST-STR-1047	155.7	18	523E	0	523E	6	Large hole in pipe, so replacement is recommended.
3	77	ST-STR-373	ST-STR-373	ST-STR-61	117.7	30	523C	3122	523C	5,1	
4	1	ST-STR-849	ST-STR-851	ST-STR-849	233.7	24	3G00	5131	513H	6	Large hole in pipe, so replacement is recommended.
5	93	ST-STR-609	ST-STR-609	ST-STR-612	222	24	513H	3121	513H	5,1	
6	92	ST-STR-610	ST-STR-610	ST-STR-609	188.4	24	513F	2100	513F	5,1	Medium sized hole at end of pipe.
7	85	ST-STR-993	ST-STR-993	ST-STR-311	103.9	30	3COO	5131	513C	5	Remove large debris. Visible portions of pipe look good.
8	80	ST-STR-321	ST-STR-320	ST-STR-321	29.1	18	513A	0	513A	5,1	
9	156 81	ST-STR-781 ST-STR-320	ST-STR-781 ST-STR-320	ST-STR-159 ST-STR-45	103.8 11.2	18	5738 5532	0 5100	5738 5632	5,1 6	Large holes in pipe, so replacement is recommended.
11	67	ST-STR-64	ST-STR-390	ST-STR-64	65.1	18	553A	4121	5541	6	Large holes in pipe, so replacement is recommended.
12	142	ST-STR-558	ST-STR-558	ST-STR-557	26.1	18	5400	3221	5432	6	Replace pipe, entire bottom half of pipe is missing.
13	171	ST-STR-393	ST-STR-393	ST-STR-394	65.2	20	5338	3100	5338	6	Large holes in pipe, so replacement is recommended.
14	83	ST-STR-346	ST-STR-346	ST-STR-347	17.9	18	5334	0	5334	6	Large holes in pipe, so replacement is recommended.
15	148	ST-STR-479	ST-STR-479	ST-STR-213	17	18	5333	0	5333	6	Replace pipe, entire bottom half of pipe is missing.
16	35	ST-STR-603	ST-STR-593	ST-STR-603	6.0	18	5331	2100	5331	6	Replace pipe, entire bottom half of pipe is missing.
17	21	ST-STR-936	ST-STR-936	ST-STR-1021	8.9	18	5241	0	5241	6	Large hole in pipe, so replacement is recommended.
18	34	ST-STR-593	ST-STR-593	ST-STR-591	2.0	18	5241	0	5241	6	Pipe deformed, therefore replacement recommended.
19	61	ST-STR-496	ST-STR-496	ST-STR-498	220.4	36	523G	4131	5241	5,1	Remove large debris at downstream end, and CIPP line entire pipe.
20	43	ST-STR-697	ST-STR-697	ST-STR-698	38.4	30	5239	0	5239	6	Large hole in pipe, so replacement is recommended.
21	63	ST-STR-774	ST-STR-774	ST-STR-775	69.4	18	5238	0	5238	5,1	
22	70	ST-STR-195	ST-STR-195	ST-STR-390	21.9	30	5234	0	5234	6	Large hole in pipe, so replacement is recommended.
23	150	ST-STR-213	ST-STR-213	ST-STR-93	21.2	18	5234	0	5234	6	Large holes in pipe, so replacement is recommended.
24	30	ST-STR-598	ST-STR-598	ST-STR-118	8.0	18	5231	3100	5232	5,1	Remove large debris at downstream end, and CIPP line entire pipe.
25	60	ST-STR-738	ST-STR-147	ST-STR-738	9.7	18	5232	2100	5232	6	Replace pipe, entire bottom half of pipe is missing.
26	158	ST-STR-773	ST-STR-773	ST-STR-157	3	18	5231	3100	5232	5,1	Remove large debris at downstream end, re-establish pipe outfall, and CIPP
27	39	ST-STR-592	ST-STR-592	ST-STR-588	1	18	5231	2100	5231	6	entire pipe. Replace pipe, entire bottom half of pipe is missing.
28	145	ST-STR-198	ST-STR-198	ST-STR-199	3	18	5231	0	5231	6	Replace pipe, entire bottom half of pipe is missing.
29	161	ST-STR-994	ST-STR-358	ST-STR-994	3	18	5131	5100	5231	5,1 or 6	Half full of debris and can't see condition of bottom of pipe.
30	40	ST-STR-1029	ST-STR-1029	ST-STR-692	450.8	24	3Q00	5142	5142	5,2	CIPP line CMP portion of pipe for 430-feet.
											Pipe overall in good condition, a couple small holes and medium deformati
31	76	ST-STR-254	ST-STR-254	ST-STR-203	70	18	5132	4200	5142	4	blocking 20% of flow area.
32	17	ST-STR-656	ST-STR-658	ST-STR-656	206.0	18	513G	4100	5141	5,1	Remove large debris. Corrosion and medium sized hole at end of pipe.
33	32	ST-STR-1018	ST-STR-1017	ST-STR-1018	174.5	24	5130	4131	5141	5,1	Remove large debris, and CIPP line entire pipe.
34	84	ST-STR-346	ST-STR-347	ST-STR-346	3	18	5131	4100	5141	6	Large holes in pipe, so replacement is recommended.
35	136	ST-STR-701	ST-STR-701	ST-STR-135	1.1	15	5100	4100	5141	5	Inspection abandoned, pipe full of debris, clean and re-inspect.
36	13	ST-STR-868	ST-STR-868	ST-STR-976	30.9	18	3800	5131	5139	5,3,1	Lateral protruding into mainline and will need to be made flush in order to
37	87	ST-STR-311	ST-STR-313	ST-STR-311	47.6	24	5139	2900	5139	5,1	rehabilitate entire pipe. Remove large debris, and CIPP line entire pipe.
38	124	ST-STR-201	ST-STR-201	ST-STR-927	74.1	16	5138	3121	5138	6	Pipe deformed, replacement is recommended.
39	53	ST-STR-714	ST-STR-714	ST-STR-715	33.9	18	5137	0	5137	5,1	Remove large debris, and CIPP line entire pipe.
40	14	ST-STR-867	ST-STR-867	ST-STR-975	26.6	18	5135	0	5135	5,1	Corrosion and medium size hole.
41	15	ST-STR-659	ST-STR-659	ST-STR-660	27.2	18	5134	0	5134	6	Pipe collapsing and deformed, replacement is recommended.
42	126	ST-STR-202	ST-STR-202	ST-STR-201	16.4	12	5132	3121	5133	6	Pipe collapsing, replacement is recommended.
43	19	ST-STR-626	ST-STR-626	ST-STR-936	12.3	18	5132	0	5132	5,1	Pipe heavily corroded, and medium deformation blocking 20% of flow area.
44	38	ST-STR-591	ST-STR-592	ST-STR-591	8.4	18	5131	2100	5131	6	Large hole in pipe, so replacement is recommended.
45	119	ST-STR-591 ST-STR-432	ST-STR-592 ST-STR-431	ST-STR-591 ST-STR-432	53.3	18	0	5131	5131	5	Pipe completely clogged with sediment.
46	134	ST-STR-710	ST-STR-710	ST-STR-138	2.0	12	5131	2100	5131	6	Large holes in pipe, so replacement is recommended.
47	162	ST-STR-359	ST-STR-359	ST-STR-58	2.8	18	5131	0	5131	6	Large hole in pipe, so replacement is recommended.
47	166	ST-STR-370	ST-STR-359 ST-STR-371	ST-STR-370	74.0	18	5131	0	5131	6	Large hole in pipe, so replacement is recommended. Large hole in pipe, so replacement is recommended.
49	5	ST-STR-850	ST-STR-850	ST-STR-849	127.4	21	5130	0	5130	6	Corrosion and large hole in pipe, so replacement is recommended.
	105										Pipe in ok condition and is too large to to CIPP line. Hydrophilic grout and
50	105	ST-STR-1045	ST-STR-813	ST-STR-1045	136.4	60	5130	2200	5130	4	urethane sealant is recommended to repair several small holes.
51 52	147 28	ST-STR-482 ST-STR-410	ST-STR-199 ST-STR-410	ST-STR-482 ST-STR-409	18.2 47.6	18 18	5100 5100	2200 0	5122 5100	5	Significant amount of debris and sediment. Pipe in ok condition. Pipe in good to ok condition.
53	65	ST-STR-387	ST-STR-410	ST-STR-386	1.0	18	0	5100	5100	5	Pipe full of debris, clean and re-inspect, signs of corrosion present.
54	69	ST-STR-390	ST-STR-390	ST-STR-94	3.0	30	5100	0	5100	6	Large hole in pipe, so replacement is recommended.
55	90	ST-STR-779	ST-STR-779	ST-STR-778	1	18	0	5100	5100	5	Inspection abandoned, pipe full of debris, clean and re-inspect.
											Inspection abandoned, pipe has water and debris, corrosion can be seen, a
56	143	ST-STR-502	ST-STR-502	ST-STR-1009	2.0	12	5100	0	5100	5	minimum CIPP lining will be required, however, condition of bottom of pip unknown, clean and re-inspect.
57	97	ST-STR-617	ST-STR-617	ST-STR-122	258.6	52	0	4238	4238	5	Pipe in overall good condition, some debris and standing water.
58	7	ST-STR-864	ST-STR-864	ST-STR-865	291.2	30	0	4231	4231	5	Pipe appears in good condition, remove sediment and debris.
59	99	ST-STR-413	ST-STR-413	ST-STR-68	140.2	24	0	4200	4200		Pipe in overall good condition.
60	130	ST-STR-272	ST-STR-272	ST-STR-271	2.0	12	0	4200	4200	5	Pipe appears in ok condition, remove sediment and debris.
61	50	ST-STR-715	ST-STR-715	ST-STR-713	148.7	24	3400	4100	4134	1	Pipe has some corrosion and small holes.
62	12	ST-STR-881	ST-STR-873	ST-STR-881	208.4	48	3100	4131	4132	5	Pipe appears in good condition, remove sediment and debris.
63	139	ST-STR-560	ST-STR-560	ST-STR-559	9.5	12	3200	4100	4132	5,1	Pipe has some corrosion and small holes. Remove sediment and debris.
						-					<u> </u>
64 65	6 123	ST-STR-863 ST-STR-927	ST-STR-864 ST-STR-1013	ST-STR-863 ST-STR-927	57.6 119.4	30 15	0	4131 4131	4131 4131	5	Pipe in good condition, remove sediment and debris. Pipe in ok condition, remove sediment and debris
66	123	ST-STR-927 ST-STR-815	ST-STR-1013 ST-STR-815	ST-STR-1044	28.7	24	0	4131 4100	4131	3	Pipe in ok condition, remove sediment and debris. Pipe in overall good condition.
67	74	ST-STR-203	ST-STR-203	ST-STR-204	227.1	30	0	4100	4100	5	Standing water in pipe. Remove sediment and debris and locate downstrea
											manhole. Pipe over half full of sediment and debris. Clean and re-inspect to see conc
68	100	ST-STR-405	ST-STR-405	ST-STR-406	1	14	0	4100	4100	5	of pipe.
69	167	ST-STR-382	ST-STR-215	ST-STR-382	1.0	18	0	4100	4100	5	Pipe over half full of sediment and debris. From what can be seen, pipe in condition. Clean and re-inspect to see condition of rest of pipe.
70	100	CT CTD 215	CT CTD 245	CT CTD CC	4.0	40	^	4400	4400	E	Pipe over half full of sediment and debris. Clean and re-inspect to see condition
/11	168	ST-STR-215	ST-STR-215	ST-STR-63	1.0	18	0	4100	4100	5	of pipe.
				1	1	1	3M00	3100	3M00	E 4	State of the State
71	101	ST-STR-977	ST-STR-977	ST-STR-872	354.8	48	SIVIOU	3100	SIVIOU	5,4	Pipe in ok condition. Consider hydrophilic grout on bottom of pipe.
	101 114	ST-STR-977 ST-STR-986	ST-STR-977 ST-STR-972	ST-STR-872 ST-STR-986	354.8 333.2	48 36	3L00	0	3L00	5,4	Pipe in ok condition. Consider hydrophilic grout on bottom of pipe. Pipe in ok condition. Consider hydrophilic grout on bottom of pipe.

Item	Setup	PSR	From MH	То МН	Length (ft)	Diameter (in)	Structural Rating	Operation & Maintenance Rating	Overall Rating	* Recommended Repair (See repair technique form for numerical definitions)	Notes/Comments/Recommendations
74	95	ST-STR-613	ST-STR-613	ST-STR-614	234.1	36	3H00	3100	3H00	5	Some sediment and debris, pipe in ok condition.
75	128	ST-STR-955 ST-STR-693	ST-STR-955 ST-STR-693	ST-STR-142 ST-STR-948	162.3	29	3F00 3E00	3200	3F00 3E00	5	Some sediment and debris, pipe in ok condition. The remaining segments with overall scores of 3 and 2 broadly represent minor maintenance and/or repair that may require hydroscour and/or grout. An indepth review of the inspection of these segments is not done at this time. More emphasis and focus should be geared towards the above segments with overall ratings of 4's and 5's and those segments include recommendations to rehabilitate or replace.
77	107	ST-STR-1052	ST-STR-961	ST-STR-1052	156	57	3E00	0	3E00		
78	25	ST-STR-612	ST-STR-612	ST-STR-611	97.3	24	3COO	0	3COO		
79	113	ST-STR-972	ST-STR-854	ST-STR-972	100.3	57	3COO	0	3COO		
80	153	ST-STR-754	ST-STR-754	ST-STR-155	118.7	24	3COO	0	3COO		
81	51	ST-STR-718	ST-STR-718	ST-STR-717	178.8	24	3COO	3121	3C21		
82	23	ST-STR-210	ST-STR-211	ST-STR-210	56.2	18	3A00	0	3A00		
83	56	ST-STR-952	ST-STR-952	ST-STR-953	182.0	30	3A00	0	3A00		
84	62	ST-STR-497	ST-STR-496	ST-STR-497	49.6	18	3900	3100	3A00		
85	118	ST-STR-431	ST-STR-431	ST-STR-77	68.9	18	3A00	0	3A00		
86	27	ST-STR-192	ST-STR-614	ST-STR-192	56.6	36	3A00	2100	3A21		
87	52	ST-STR-716	ST-STR-716	ST-STR-717	34.6	18	3900	0	3900		
88	103	ST-STR-870	ST-STR-870	ST-STR-871	97.2	36	3800	2300	3823		
89	46	ST-STR-688	ST-STR-688	ST-STR-687	36.8	18	3800	0	3800		
90	106	ST-STR-961	ST-STR-1045	ST-STR-961	42.3	57	3800	0	3800		
91	109	ST-STR-1053	ST-STR-1052	ST-STR-1053	92.8	57	3800	0	3800		
92	111	ST-STR-1055	ST-STR-971	ST-STR-1055	80.9	57	3800	0	3800		
93	8	ST-STR-865	ST-STR-865	ST-STR-974	41.0	24	3700	0	3700		
94	18	ST-STR-1021	ST-STR-1021	ST-STR-625	32.6	30	3700	0	3700		
95	24	ST-STR-628	ST-STR-628	ST-STR-210	34.6	18	3700	0	3700		
96	117	ST-STR-422	ST-STR-74	ST-STR-422	32.4	24	3600	3100	3700		
97	47	ST-STR-947	ST-STR-132	ST-STR-947	13.7	22	3500	2100	3521		
98	151	ST-STR-750	ST-STR-752	ST-STR-750	22.6	15	3500	2100	3521		
99	64	ST-STR-383	ST-STR-383	ST-STR-384	40.4	14	3500	0	3500		
100	94	ST-STR-609	ST-STR-612	ST-STR-609	23.8	24	3500	0	3500		
101	96	ST-STR-616	ST-STR-617	ST-STR-616	25	52	3500	0	3500		
102	86	ST-STR-311	ST-STR-313	ST-STR-311	13.2	24	3300	3123	3423		
103	157	ST-STR-764	ST-STR-765	ST-STR-764	21.2	12	3400	2100	3421		
104	29	ST-STR-998	ST-STR-998	ST-STR-913	150.2	42	3400	0	3400		
105	42	ST-STR-699	ST-STR-697	ST-STR-699	8.4	30	3400	0	3400		
106	82	ST-STR-321	ST-STR-321	ST-STR-320	2.2	18	3300	3100	3400		
107	59	ST-STR-738	ST-STR-738	ST-STR-147	11.4	18	3300	2100	3321		
108	138	ST-STR-677	ST-STR-678	ST-STR-677	14.3	18	3300	2100	3321		
109	2	ST-STR-851	ST-STR-851	ST-STR-1052	24.2	18	3300	0	3300		
110	3	ST-STR-1046	ST-STR-1046	ST-STR-815	117.7	24	3200	3100	3300		
111 112	71 55	ST-STR-395	ST-STR-395	ST-STR-995	15.1	18 30	3300	0	3300		
113	89	ST-STR-713 ST-STR-778	ST-STR-713 ST-STR-778	ST-STR-952 ST-STR-957	207.9 61.7	18	3200 0	2100 3200	3221 3200		
114	116	ST-STR-823	ST-STR-823	ST-STR-1051	3	18	3100	3100	3200		
115	125	ST-STR-202	ST-STR-201	ST-STR-202	2	12	3100	3100	3200		
116	9	ST-STR-866	ST-STR-974	ST-STR-866	43.4	18	3100	2100	3121		
117	49	ST-STR-718	ST-STR-717	ST-STR-718	56.9	24	0	3121	3121		
118	78	ST-STR-372	ST-STR-373	ST-STR-372	206	18	3100	2100	3121		
119	146	ST-STR-198	ST-STR-199	ST-STR-198	7.5	18	3100	2100	3121		
120	11	ST-STR-873	ST-STR-1056	ST-STR-873	39.5	48	0	3100	3100		
121	48	ST-STR-717	ST-STR-715	ST-STR-717	390.1	24	3100	0	3100		
122	73	ST-STR-985	ST-STR-995	ST-STR-985	169	30	3100	0	3100		
123	110	ST-STR-971	ST-STR-1053	ST-STR-971	263	57	3100	3100	3100		
124 125	57 22	ST-STR-806 ST-STR-211	ST-STR-806 ST-STR-211	ST-STR-173 ST-STR-627	124.8 120.3	18 18	3000 3000	2100 0	3021 3000		
126	112	ST-STR-854	ST-STR-1055	ST-STR-854	138.5	57	3000	0	3000		
127	10	ST-STR-1056	ST-STR-977	ST-STR-1056	38.4	48	0	2100	2100		
128	122	ST-STR-451	ST-STR-450	ST-STR-451	12.5	12	0	2100	2100		
129	137	ST-STR-677	ST-STR-677	ST-STR-678	21.2	18	0	2100	2100		
130	144	ST-STR-481	ST-STR-198	ST-STR-481	29.0	18	0	2100	2100		
131	163	ST-STR-369	ST-STR-369	ST-STR-368	8.2	18	0	2100	2100		
132	26	ST-STR-619	ST-STR-618	ST-STR-619	16.5	18	0	0	0		Pipe in good condition.
133 134	45	ST-STR-948	ST-STR-948	ST-STR-690	3.3	18	0	0	0		Pipe in good condition.
134	58 72	ST-STR-739 ST-STR-995	ST-STR-738 ST-STR-203	ST-STR-739 ST-STR-995	42.3 30.3	18 30	0	0	0		Pipe in good condition. Pipe in good condition.
136	79	ST-STR-376	ST-STR-203	ST-STR-374	9.9	24	0	0	0		Pipe in good condition.
137	104	ST-STR-814	ST-STR-813	ST-STR-814	18	24	P 0000	0	0		Pipe in good condition.
138	121	ST-STR-78	ST-STR-433	ST-STR-78	0.1	18	0	0	0		Drop connection, unable to video pipe.
139	127	ST-STR-726	ST-STR-726	ST-STR-955	27.7	29	0	0	0		Pipe in good condition.
140	131	ST-STR-720	ST-STR-720	ST-STR-722	1.0	18	0	0	0	5	Pipe underwater, outfall not found, clean and re-inspect.
141	132	ST-STR-721	ST-STR-721	ST-STR-720	1.0	18	0	0	0	5	Pipe underwater, clean and re-inspect.
142 143	135 141	ST-STR-701 ST-STR-553	ST-STR-135 ST-STR-553	ST-STR-701 ST-STR-928	1.0 25.5	15 16	0	0	0	6	Collapsed pipe, repair or replace. Pipe in good condition.
144	152	ST-STR-751	ST-STR-751	ST-STR-754	83.7	24	0	0	0		Pipe in good condition.
145	154	ST-STR-295	ST-STR-294	ST-STR-295	1	18	0	0	0	5	Pipe full of debris, clean and re-inspect.
146	155	ST-STR-340	ST-STR-341	ST-STR-340	1	12	0	0	0	5	Pipe full of sediment and debris, clean and re-inspect.
147	160 164	ST-STR-53 ST-STR-369	ST-STR-896 ST-STR-368	ST-STR-53 ST-STR-369	1.0	12	0	0	0	5	Pipe in good condition. Camera blocked by sediment and debris. Pipe in ok condition.
149	165	ST-STR-368	ST-STR-368	ST-STR-190	1.0	15	0	0	0		Pipe in good condition.





PACP© Condition Grading System

The Pipeline Assessment and Certification Program (PACP) developed by NASSCO provides a mechanism for creating reliable descriptions of pipe conditions. NASSCO has also developed a system based on the PACP codes to assign a condition rating to pipelines. Requirements of the grading system were as follows:

- 1. Like the PACP, the grading system should be direct and objective.
- Provide the ability to qualitatively identify differences in pipe condition between one inspection and subsequent inspections, and to prioritize based on the significance of the defects different pipe segments.

Many other approaches to sewer pipe grading have been used in the United States as well as in other parts of the World. These approaches generally use some type of defect grading that is then used to calculate an overall pipe rating.

It is problematic to develop a single pipe segment rating that fully describes all of the important aspects of a pipe. Therefore the PACP Condition Grading System uses more than one method of rating pipe segment condition including a rating that considers the number of total defects within the pipe segment and a rating that considers the most severe defects within the pipe segment.

The PACP Condition Grading System only considers internal pipe conditions obtained from TV inspection. While other factors such as pipe material, depth, soils, and surface conditions also affect pipe survivability, those factors have not been included in the PACP Condition Grading System. The PACP Condition Grading System should be used only as a tool for screening pipe segment inspections, allowing the User to quickly determine which pipe segments have significant defects. It is expected that as the PACP further develops the PACP Condition Grading System will expand to include other factors.

The PACP Condition Grading System provides condition ratings for Structural Defects and Operation and Maintenance Defects.

Approach

Using the PACP Code Matrix, Each PACP defect code is assigned a condition grade of from 1 to 5. Grades are assigned based on the significance of the defect, extent of

D-1





damage, percentage of flow capacity restriction, or the amount of wall loss due to deterioration.

The PACP Condition Grading System alone is inadequate for determining if a pipe segment should be rehabilitated or replaced. Many other factors in addition to the internal condition of the segment should be considered. The fact that a segment has significant Grade 4 or Grade 5 defects does not necessarily mean the pipe segment should be immediately rehabilitated. Recent experience by PACP Users has shown that pipe segments with serious defects such as hinge failures may remain largely unchanged for many decades if no deterioration factors such as surcharging, roots, or groundwater are present.

What is needed is improved estimates of remaining life or mean time before failure that are based on close monitoring of pipe segments over time. Once we know how much change occurs in pipe segments we can better understand the relationship between defects, deterioration factors, and pipe segment life expectancy. PACP continues to be an excellent tool for benchmarking pipe condition between one inspection and subsequent inspections of the same pipe.

Grades are assigned for two categories, Structural, and O&M defects. Grades are as follows:

- 5 Most significant defect grade
- 4 Significant
- 3 Moderate defect grade
- 2 Minor to Moderate
- 1 –Minor defect grade

The PACP Condition Grading System results are entirely dependent on the quality of the PACP defect coding. Errors in the coding will directly result in errors in the Grading. All utilities, engineers, and contractors should make sure the data they are using was coded by experienced technicians who have successfully demonstrated their competence through a formal or informal apprenticeship program. PACP data from inexperienced technicians should be checked and corrected as needed. Errors found in coding should be corrected and the errors brought to the attention of the technician.





Grading of Continuous Defects

The PACP continuous defect feature is used to denote where long portions of a sewer pipe are affected by the same defect, without the User having to repetitively enter point defects. However to develop a grade for the pipe segment, a mechanism is needed to translate a continuous defect into an equivalent number of point defects.

The equivalent number (quantity) of "uninterrupted" and "joint repeating" continuous defects is calculated by dividing the length of the continuous defect by 5. Example, a 6-meter long continuous defect, grade 3, should equate to four Grade 3 defects. Fractions are rounded to the nearest whole number.

Pipe Ratings

The pipe rating is based on the number of occurrences for each condition grade. Ratings are calculated separately for **Structural Defects** and **O&M Defects**. Several ways of expressing pipe segment condition are used by the PACP Condition Grading System as follows.

Segment Grade Scores - Each pipe segment will have a Segment Grade Score for each of the five grades. The number of occurrences of each pipe grade is multiplied by the pipe grade to calculate the segment grade score. Example, six Grade 5 defects would be 6 times 5 and equates to a Segment Grade 5 Score of 30. If a pipe segment had no defects of a particular grade, then the Segment Grade Score for that grade would be 0.

Overall Pipe Rating –The five Segment Grade Scores are added together to calculate the Overall Pipe Rating. Structural Pipe Ratings are calculated using only Structural Defect grades, while O&M Pipe Ratings are calculated using only O&M Defect grades.





PACP Quick Rating – The PACP Quick Rating is a shorthand way of expressing the number of occurrences for the two highest severity grades. The PACP Quick Rating is a four character score as follows:

- 1. The first character is the highest severity grade occurring along the pipe length.
- 2. The second character is the total number of occurrences of the highest severity grade. If the total number exceeds 9, then alphabetic characters are used as follows- 10 to 14 A; 15 to 19 B; 20 to 24 C; etc.
- 3. The third character is the next highest severity grade occurring along the pipe length.
- 4. The fourth character is the total number of the second highest severity grade occurrences, derived as in item 2 above.

For Example

4B27

This immediately shows that no grade 5 defects or grade 3 defects, however 15 to 19 grade 4 defects and seven grade 2 defects were found.

Another Example

3224

Two grade 3 defects and four grade 2 defects, however no grade 5 or grade 4 defects were found.

If a pipe segment only has defects of one grade, the first two characters are the grade and the quantity of defects, and the last two characters are 00 (denoting no other defect grades). A pipe segment with no defects would have a Quick Score of 0000 (all zeros).

The PACP Quick Rating provides the ability to summarize the number and severity of defects found within a pipe segment. As with the Pipe Rating, Quick Structural Ratings





are calculated using only Structural Defect Grades, and Quick O&M Ratings are calculated using only O&M Defect Grades.

The Quick Rating is an excellent screening tool to determine which pipe segments require closer scrutiny. If a pipe has not defects greater than Grade 1 or 2, then the pipe segment probably does not need any further investigation.

Pipe Ratings Index – This is an indicator of the distribution of defect severity. The Pipe Ratings Index is calculated by dividing the Pipe Rating by the number of defects. For example, the Structural Pipe Ratings Index would be the Structural Pipe Rating divided by the number of structural defects. Pipe Ratings Indexes are calculated for Structural, O&M, and Overall. A pipe segment with a Pipe Rating of zero (0) would have a Pipe Rating Index of zero (0).

Summary

The following procedures are used to calculate pipe segment ratings using the PACP Condition Grading System:

- Determine the number of occurrences for each condition grade within the pipe segment. Calculate separately for Structural Defect Grades and O&M Defect Grades.
- Calculate the Segment Grade Score by multiplying the number of occurrences by the respective grade 1 through 5. Calculate the Structural Segment Grade Score and the O&M Segment Grade Score separately, and then add together for the Overall Segment Grade Score.
- 3. Calculate the Pipe Rating for the pipe segment by adding the Segment Grade Scores. Add all five Structural Segment Grade Scores for the Structural Pipe Rating, and add all five O&M Segment Grade Scores for the O&M Pipe Rating. Add all five Overall Segment Grade Scores for the Overall Pipe Rating.
- Determine the PACP Quick Rating by calculating the number of occurrences of the two highest severity grades.





- Calculate the Pipe Ratings Index by dividing the Pipe Rating by the number of defects. If the pipe has no defects, the Pipe Ratings Index is zero.
- Verify the PACP defect data used in accurate. The grading is a direct calculation from the defect data, and coding errors will be reflected in grading errors.

Family	Group	Descriptor	Modifier	Code	Structural Grade	O&M Grade
Structural	Crack (C)	Circumferential (C)		00	1	
		Longitudinal (L)		ъ	2	
		Multiple (M)		CM	ю	
		Hinge (CH2)		CH2	4	
		Hinge (CH3)		CH3	22	
		Hinge (CH4)		CH4	ú	
		Spiral (S)		CS	2	
Christinal	Fracture (F)	Circumferential (C)		FC	2	
on deciding.	() () () () ()			료	3	
		Multiple (M)		FM	4	
		Hinge (H2)		FH2	4	
		Hinge (H3)		FH3	2	
		Hinge (H4)		FH4	വ	
		Spiral (S)		FS	9	
	Ciloro College	Broken (B)		۵	1 clock pos - 3, 2 clock pos - 4,	
Structural	ripe railates (Siletti)	Broken (B)	Soil Visible (SV)	BSV	5	
		Broken (B)	Void Visible (V V)	BVV	5	
		Hole (H)		I	1 clock pos - 3, 2 clock pos - 4, >= 3 clock pos - 5	
		Hole (H)	Soil Visible (SV)	HSV	. 5.	
		Hole (H)	Void Visible (V V)	AM	5	
Structural	Collapse (X)	Pipe (P)		Ϋ́	2	
		Brick (B)		XB	5	
Structural	Deformed (D)	(Pipe)		۵	<=10% - 4,>10% - 5	
		(Brick)	Horizontally (H)	H 2	ນ ດ	
	100	(Differ) (displaced) (O)	Med (M)	NO.		
Structural	Joint (J)	Ollser (displaced) (O)	Large (L)	JOF	2	
		Separated (open) (S)	Med (M)	JSM		
			Large (L)	JSL	2	
		Angular (A)	Med (M)	JAM		
			Large (L)	JAL	8	
Structural	Surface Damage Chemical (S)	Roughness Increased (RI)	ပ	SRIC	- 0	
		Surface Spalling (SS)	သ	2222	\u030	
		Aggregate Visible (AV)	5 C	SAVC	200	
		A COLOGICAL DISCONOR	2	CARO	9	

ramily	Group	Descriptor	Modifier	Code	Structural Grade	O&M Grade
				SRVC	2	
		Reinforcement Projecting (RP)	O	SRPC	n	
		Reinforcement Corroded (RC)	O	SRCC	2	
		Missing Wall (MW)	U	SMWC	2	
i		Other (Z)	O	SZC		
Structural	Surface Damage Mechanical (M)	Roughness Increased (RI)	Σ	SRIM	+	
		Surface Spalling (SS)	≥	SSSM	45)	
		Aggregate Visible (AV)	Σ	SAVM	, l,	
		Aggregate Projecting (AP)	Σ	SAPM	Con	
		Aggregate Missing (AM)	Σ	SAMM	4	
		Reinforcement Visible (RV)	Σ	SRVM	مار	
		Reinforcement Projecting (RP)	Σ	SRPM	على ا	
		Reinforcement Corroded (RC)	Σ	SRCM	200	
		Missing Wall (MW)	Σ	SMWM	l se	
		Other (Z)	Σ	SZM	N/A S	
Structural	Surface Damage Not Evident (Z)	Roughness Increased (RI)	7	SRIZ	-	
		Surface Spalling (SS)	2	SSSZ	2	
		Aggregate Visible (AV)	2	SAVZ	1 60	
		Aggregate Projecting (AP)	2	SAPZ	0 00	
		Aggregate Missing (AM)	Z	SAMZ	4	
		Reinforcement Visible (RV)	7	SRVZ	. 2	
		Reinforcement Projecting (RP)	2	SRPZ	e co	
		Reinforcement Corroded (RC)	<u>Z</u>	SRCZ	n (c	
		Missing Wall (MW)	2	SMWZ	ı ıci	
		Other (Z)	2	SZZ	N/A	
Structural	Surface Damage (Metal Pipes)	Corrosion (CP)		SCP	m	
Structural	Lining Features (LF)	Detached (D)		LFD	m	
		Defective End (DE)		LFDE	m	
		Blistered (B)		LFB	m	
		Service Cut Shifted (CS)		LFCS	n	
		Abandoned Connection (AC)		LFAC		
		Overcut Service (OC)		LFOC	က	
		Undercut Service (UC)		LFUC	8	
				LFBK	က	
		Annular Space (AS)		LFAS	m	
		Bulges (BU)		LFBU	m	
		Discoloration (DC)		LFDC	m	
		Delamination (DL)		LFDL	ന	
		Pinholes (PH)		LFPH) ന	
		Resin Slug (RS)		LFRS	ന	
		Wrinkled (W)		LFW) m	
		Other (Z)		LFZ	N/A	
Structural	Weld Failure (WF)	Circumfrential (C)		WFC	2	
		I was the all and All		-		

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Family	Group	Multiple (M)	Modifier	Code	Structural Grade	O&M Grade
		Spiral (S)		WFS	N	
Structural	Point Benair (BP)	Localized Pipeliner (L)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RPL		
on non-non-non-non-non-non-non-non-non-n	() modern min	Localized Pipeliner (L)	Defective (D)	RPLD	4	
		Patch Repair (P)		ВРР	0	
		Patch Repair (P)	Defective (D)	RPPD	4	
		Pipe Replaced (R)		RPR		
		Pipe Replaced (R)	Defective (D)	RPRD	4	
		Other (Z)		RPZ		
		Other (Z)	Defective (D)	RPZD		
	Ordelands (Otland)	Displaced (DB)		DB	m	
Structural	Dischaus (Silenis)	Missing (MB)		MB	4	
		Dropped Invert (DI)		ō	വ	
		Missing Mortar	Small	MMS	2	
		, and a second	Medium	MMM	e	
			Large	MML	က	
N N	Denosits (D)	Deposits Attached (DA)	Encrustation (E)	DAE		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Grease (G)	DAGS		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Ragging (R)	DAR		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Other (Z)	DAZ		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
		Deposits Settled (DS)	Hard/Compacted (C)	DSC		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Fine silt/sand (F)	DSF	4	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Gravel (G)	DSGV		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Other (Z)	ZSQ		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
		Deposits Ingress (DN)	Fine silt/sand (F)	DNF		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Gravel (GV)	DNGV		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5

						O&M				O&M														0&M		Family
						Obstacles/Obstructions (OB)				Infiltration (I)	Roots (R) at a Joint			Hoots (H) at a Joint				Roots (R) at a Joint			Hoots (H) at a Joint	į		Roots (R)		Group
Built Into Structure (S)	External Pipe or Cable In Sewer (P)	Object Thru Connection (C)	Object Wedged in Joint (J)	Object Intruding Thru Wall (I)	Pipe Material in Invert (M)	Brick or Masonry (B)	Stain (S)	Gusher (G)	Bunner (B)	Weeper (W)			Can (C)	Ball (B)			Medium (M)			(ab (1)	T. (T)			Fine (F)		Descriptor
											N/A	Connection (C)	Lateral (L)	Rarrel (R)	Connection (C)		Barrel (B)	- 1	Connection (C)	Lateral (L)	N/A	Connection (C)		Barrel (B)	Other (Z)	Modifier
OBS	OBP	ОВС	OB	OBI	OBM	OBB	S	ត	ī ā	5 8	RBJ	RBC	RBL	BBB	RMC	RML	RMB	RTJ	RTC	BIL	D I I	3 7 7	RFL	RFB	DNZ	Code
																					in sollware will a J					Structural Grade
<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5		თ .	4 (ω N	4	4	4	У Л (w cu	ω	4	2	2	N (-	N	<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5	O&M Grade

Family	Group	Descriptor	Modifier	Code	Structural Grade	O&M Grade
		Construction Debris (N)		OBN		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
		Rocks (R)		OBR		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
		Other Objects (Z)		OBZ		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
ORM	Vermin (V)	Rat (R)		VR		7
	(4)	Cockroach (C)		VC		-
		Other (Z)		ZA		-
O&M	Grout Test and Seal (G)	Grout Test Pass (GTP)				
	/		Joint (J)	GTPJ		
			Lateral (L)	GTPL		
		Grout Test Fail (GTF)				
			Joint (J)	GTEJ		
		WITO test of class test to con-	raierai (L)	7.5		
		Grout Test Unable to Test (GTU)	loint (1)	GTILI		
			Lateral (L)	GTUL		
		(TBT) (Apply (ABT)	(a) minima	GRT		
		Grout at a Eccanor (not a joint) (con)		i		
tion	(F)	Eastern Made (E)		4		
reaures	(ap (1)	י מכנסו ל ואומסכ (ו)	Capped (C)	TFC		
			Abandoned (B)	TFB		
			Defective (D)	TFD		2
			Intrudina (1)	TFI		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Activity (A)	TFA		
		Break-In/Hammer (B)		118		
			Capped (C)	TBC		2
			Abandoned (B)	TBB		
			Defective (D)	TBD		ဇာ
			Intruding (I)	TBI		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Activity (A)	TBA		
		Saddle (S)		TS		
			Capped (C)	TSC		
			Abandoned (B)	TSB		

NASSCO PACP Condition Grading System Code Matrix

Family	Group	Descriptor	Modifier	Code	Structural Grade	O&M Grade
			Defective (D)	TSD		N
			Intruding (I)	TSI		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Activity (A)	TSA		
		Rehabilitated (R)		TT.		
			Defective (D)	TRD		2
			Intruding (I)	TRI		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
Construction Features	Intruding Seal Material (IS)			S		
		Sealing Ring (SR)		ISSR		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Hanging (H)	ISSRH		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
			Broken (B)	ISSRB		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
		Loose, Poorly Fitting (SRL)		ISSRL		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
		Grout (GT)		ISGT		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
		Other (Z)		ZSI		<=10% - 2, <=20% - 3, <=30% - 4, >30% - 5
Construction Features	Line (L)	Leff (L)		7		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4
		Left/Up (LU)		חוח		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4
		Left/Down (LD)		TLD		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4
		Right (R)		FB		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4

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Constitution Access Points (A) Elgipt/Up (RU) Elg	Family	Group	Descriptor	Modifier	Code	Structural Grade	O&M Grade
Down (BD) LED			Right/Up (RU)		LRU		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4
uction Access Points (A) Cleanout (CO) Mainfine (M) ACO Notes of Points (A) Cleanout (CO) Mainfine (M) ACOM Discharge Point (DP) Property (P) ACOM Discharge Point (DP) Property (P) ACOM Discharge Point (DP) Property (P) ACOM Discharge Point (DP) ACOM ACOM Discharge Point (DP) ACOM ACOM Other Special Chamber (CO) AM AM Other Special Chamber (CO) AM AM Other Special Chamber (CO) AM AM WWA Access Davice (WH) AM ACC WWA Access Davice (WH) AM ACC Cach Basin (CB) ACC AW Cach Basin (CB) ACC ACC Cach Basin (CB) ACC ACC Cach Basin (CB) ACC ACC Cannera Underwater (CU) ACC ACC Cannera Underwater (CU) ACC ACC Cannera Underwater (CD) ACC ACC Canne			Right/Down (RD)		LRD		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4
Down (D)			Up (U)		E		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4
Maintine (M)			Down (D)		rp		<=10 Deg - 1, <=20 Deg 2, >20 Deg - 4
ACOM		cess Points (A)					
Mainline (M) ACOM			Cleanout (CO)		ACO		
Property (P) ACOP ACOP				Mainline (M)	ACOM		
Miscellaneous (M) Discharge Point (DP) ADP				Property (P)	ACOP		
Discharge Point (DP)				House (H)	ACOH		
Marticle (MH)			Discharge Point (DP)		ADP		
Mater (M)			Junction Box (JB)		AJB		
Manhole (MH)			Meter (M)		AM		
Other Special Chamber (OC)			Manhole (MH)		AMH		
Tee Connection (TC)			Other Special Chamber (OC)		AOC		
WWW Access Device (WA) AWW Wet Well (WW) ACB End of Pipe (EP) AEP End of Pipe (EP) AEP Miscellaneous (M) Camera Underwater (CU) Dimension/Diam/Shape Change (SC) MSC General Observation (GO) MGO General Photograph (GP) MGO Material Change (MC) MGC Ining Change (LC) MLC Pipe Joint Length Change (LC) MLC Pipe Joint Length Change (LC) MLC Pipe Joint Level (WL) MSA Water Level (WL) Sag (S) WWLS <=30% - 2, <=50% - 3, >50% - 4 Water Mark (WM) MY MAY MY			Tee Connection (TC)		ATC		
Wet Well (WW) ACB End of Pipe (EP) ACB End of Pipe (EP) ACB End of Pipe (EP) ACB Dimension/Diam/Shape Change (SC) MSC General Observation (GO) MGO General Photograph (GP) MGO Material Change (MC) MMC Ining Change (LC) MMC Pipe Joint Length Change (JL) MILC Pipe Joint Length Change (JL) MSA Water Level (WL) Sag (S) Water Level (WL) Sag (S) Water Level (WL) MWKLS Dye Test (Y) MXY MAYN MXY			WW Access Device (WA)		AWA		
Miscellaneous (M)			Wet Well (WW)		AWW		
Miscellaneous (M) Camera Underwater (CU) MCU			Catch Basin (CB)		ACB		
Miscellaneous (M) Camera Underwater (CU) MCU Dimension/Diam/Shape Change (SC) MSC General Observation (GO) MGO General Photograph (GP) MGP Material Change (MC) MMC Lining Change (LC) MMC Pipe Joint Length Change (JL) MMLC Survey Abandoned (SA) MWL Water Level (WL) Sag (S) Water Mark (WM) MW Dye Test (Y) Visible (V) MAYY MAYY			End of Pipe (EP)		AEP		
Hange (SC) MGO MGP MMC MLC MLC MLC MJL MML MML Sag (S) MWMLS MWM MWM MWM MWM MWM MWM M		cellaneous (M)	Camera Underwater (CU)		MCU		4
(JL) MGP MMC MMC MMC MMC MMC MMC MMC MMC MMC MM			Dimension/Diam/Shape Change (SC)	9	MSC		
(JL) MMC MMC MMC MMC MMC MMC MMC MMC MMC MM			General Observation (GO)		MGO		
(JL) MMC MLC MJL MSA MWL Sag (S) MWMS <=30% - 2, <=50% - 3, >50% - 4 MWM MWM MWM MWM MWM MWM MWM MWM MWM M			General Photograph (GP)		MGP		
(JL) MLC MJL MSA MWL Sag (S) MWL < =30% - 2, <=50% - 3, >50% - 4 MWM			Material Change (MC)		MMC		
MJL MSA MWL Sag (S) MWLS <=30% - 2, <=50% - 3, >50% - 4 MWM NY MYW MYW MYW MYW MYW MYW MYW MYW MYW MY			Lining Change (LC)		MLC		
MWL Sag (S) MWLS <=30% - 2, <=50% - 3, >50% - 4 MWM NY MY			Pipe Joint Length Change (JL)		MJL		
) MWLS <=30% · 2, <=50% · 3, >50% · 4) MWM			Survey Abandoned (SA)		MSA		
) MWLS <=30% - 2, <=50% - 3, >50% - 4 MWM			Water Level (WL)				
Visible (V) MYV				Sag (S)	9	=30% - 2, <=50% - 3, >50% - 4	
Visible (V) MYV			Water Mark (WM)		MWM		>=50% 4, >=75% 5
NYV N			Dye Test (1)	VE-ILL AA	YM.		
				Visible (v)	MYV		Ω

REPAIR TECHNIQUES

1. Cured In Place Pipe (CIPP) Lining

The CIPP lining process involves inserting a resin-saturated flexible lining into the existing pipe. The lining looks like a very large sock or flexible tube. Air or water under pressure is forced into the tube, which turns the lining inside out and causes it to fit tightly to the existing pipe walls. Hot air or water is circulated throughout the tube to harden the resin, completing the curing process. When the curing process is completed, a new pipe has been created that is free of cracks and holes that allow rainwater and roots to enter the pipe and cause operational problems such as stoppages and overflows. The finished product has a 50-year design life, the same as that of a brand new pipe.

2. Cured In Place Pipe (CIPP) Sectional Repairs

Sectional CIPP repairs apply to facilities that do not require the entire pipe to be rehabilitated. If a particular pipe is damaged in isolated locations, then CIPP sectional repairs can typically be applied and the repairs range from three to thirty feet in length with diameters ranging from six inches to forty-eight inches. Unlike full-length liners, a sectional repair may be any distance from the manhole.

3. Top Hat (TH) In Lateral/Main Connection Sealing

This utilizes a specially shaped liner, which looks just like a Top Hat (TH) or inverted 'T'. The stem of the TH forms the section of liner that is placed into the lateral pipe while the TH crossbar sits against the inner wall of the main. Resin impregnation of the liner material allows it to be positioned using a specially designed remote control robotic installer and held in position for curing of the resin. Once cured, the robot and retention system are removed leaving the 'T'-shaped liner forming a seal across the lateral/main joint. The TH stem can be made to pass as deep into the lateral if necessary.

4. Pressurized Hydrophilic Chemical Grout and Urethane Sealant

Pressurized hydrophilic grout is primarily used for the repair of defects in water environments. The grout is typically injected under pressure, as a liquid into and/or around a leak. Once in contact with water, the grout reacts, filling voids and sealing defects. Hydrophilic grout requires water for the reaction to occur and creates flexible, resilient repairs. It can bond to wet surfaces, and has the ability to expand or contract within the voids.

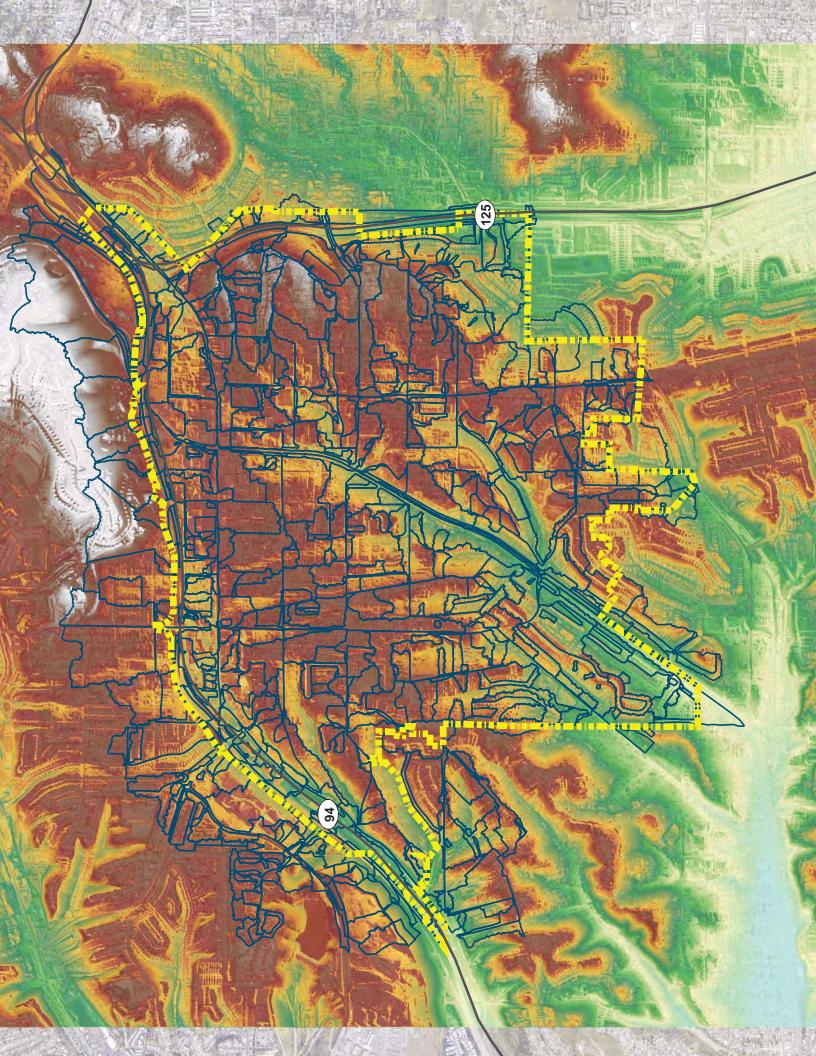
5. Hydro-Scouring

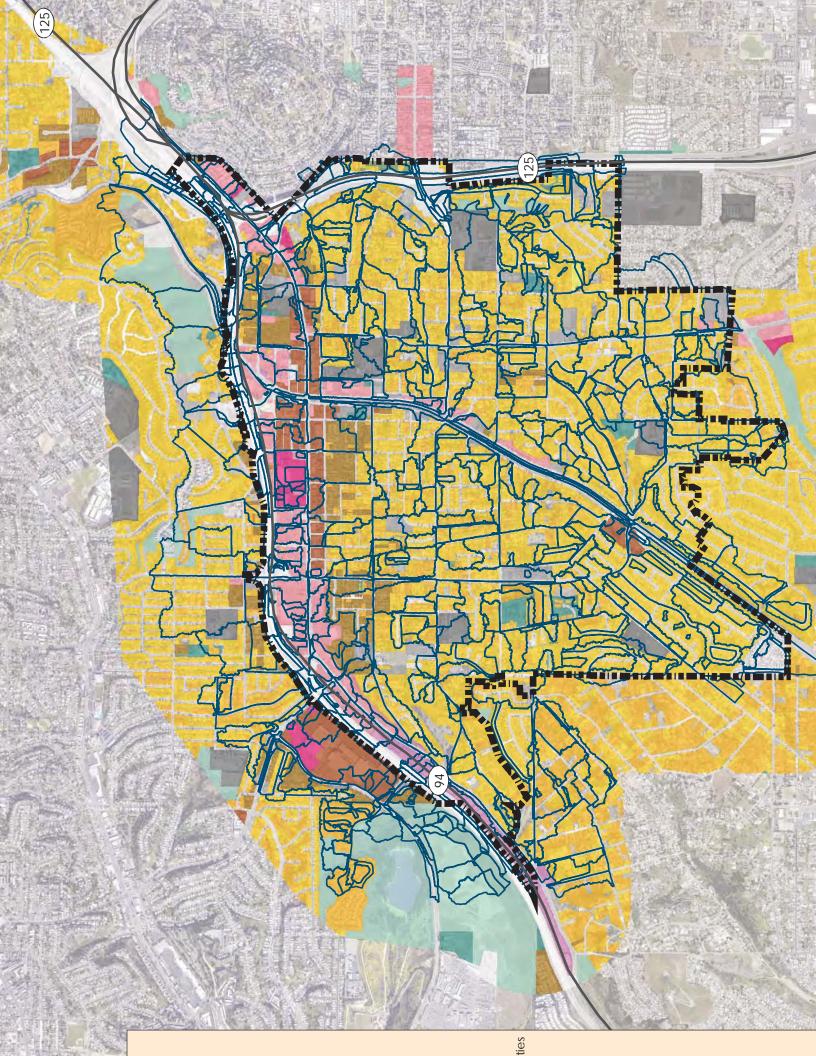
The hydro scouring method effectively removes grit and grease accumulation from sewer lines. High water pressure scours the inside of the sewer pipelines, restoring the hydraulic capacity.

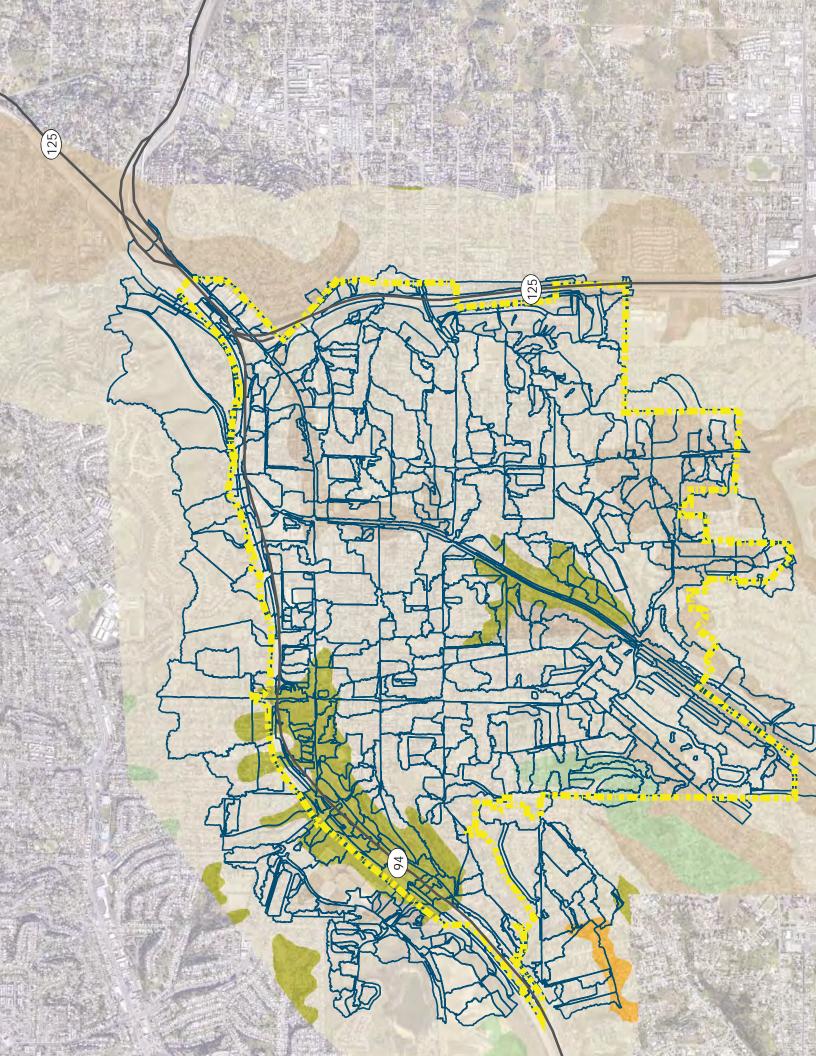
6. Pipe Removal and Replacement

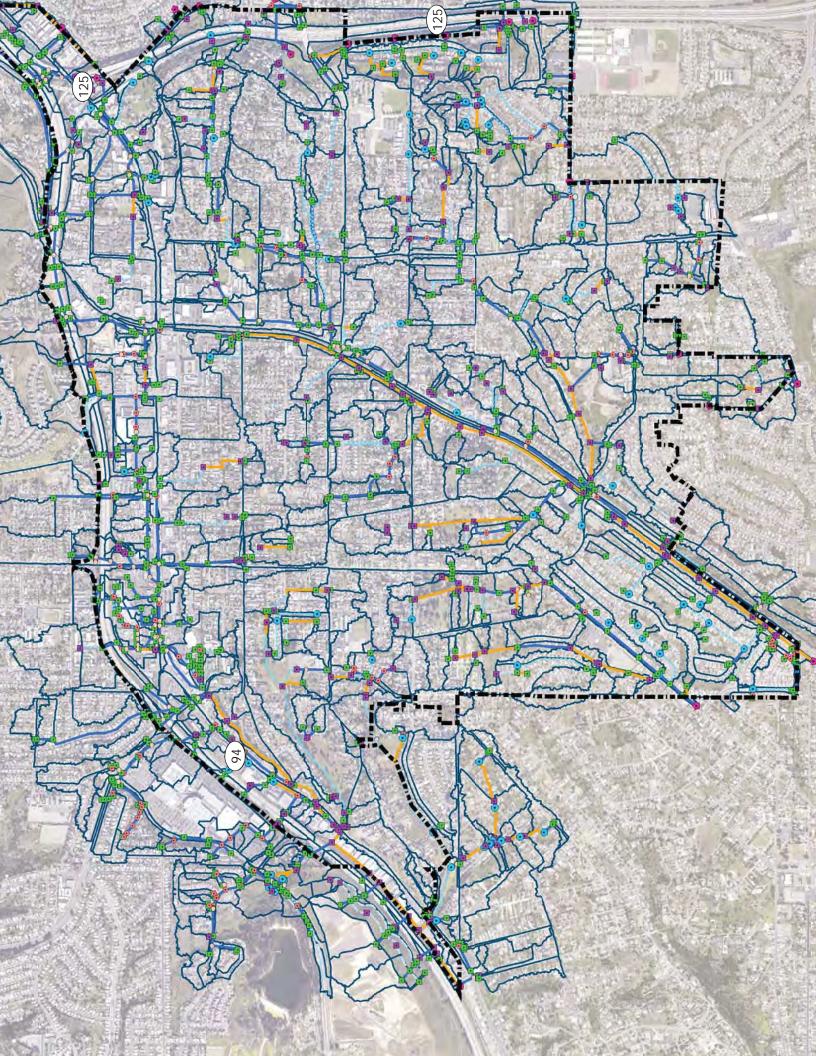
Removal and replacement is recommended if the pipe cannot be rehabilitated.

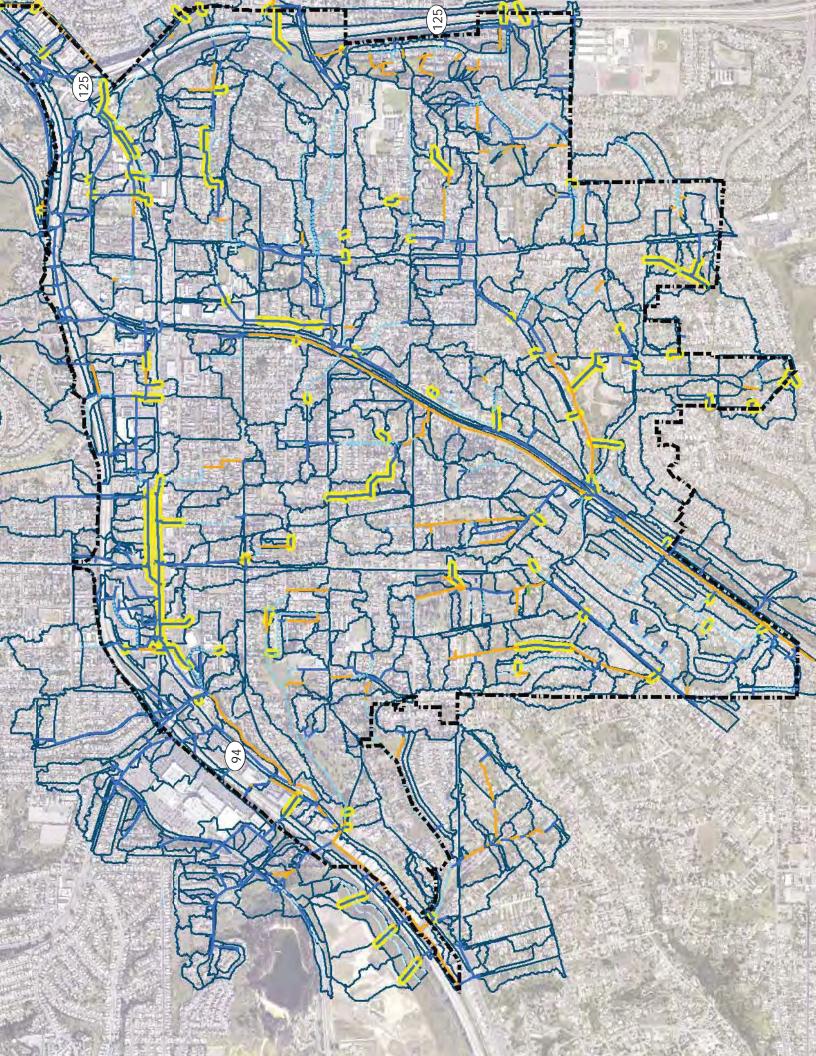
C. GIS Dataset Exhibits

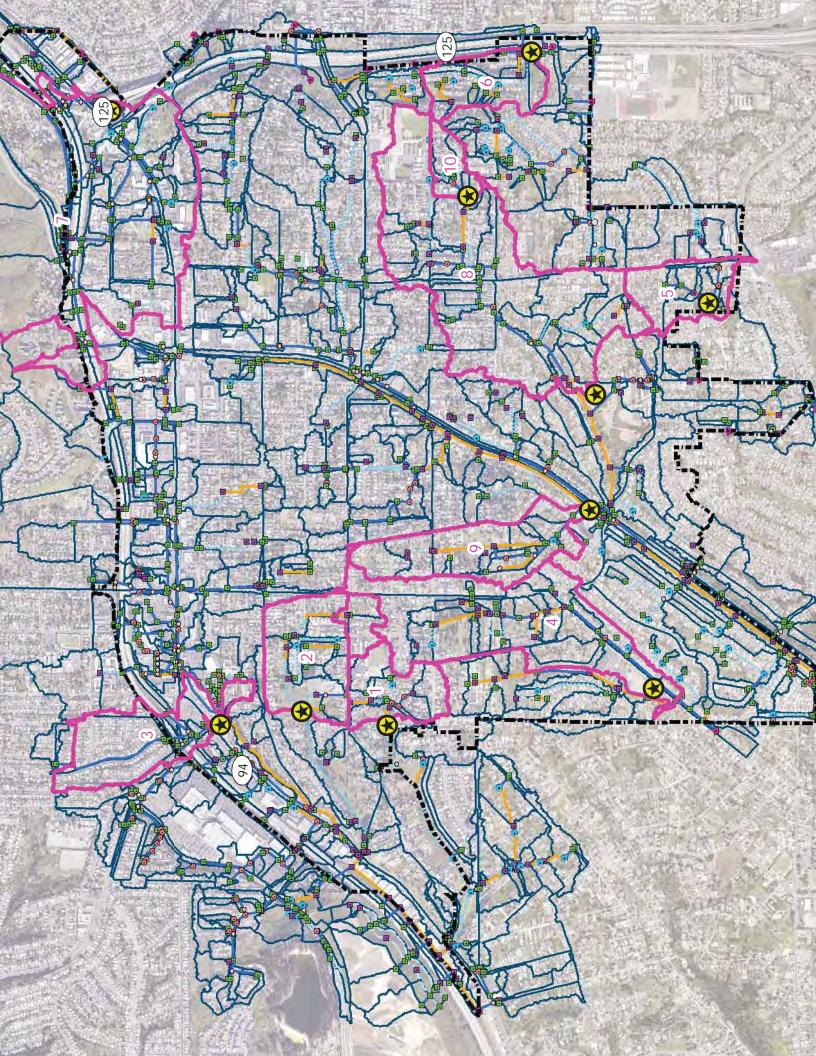




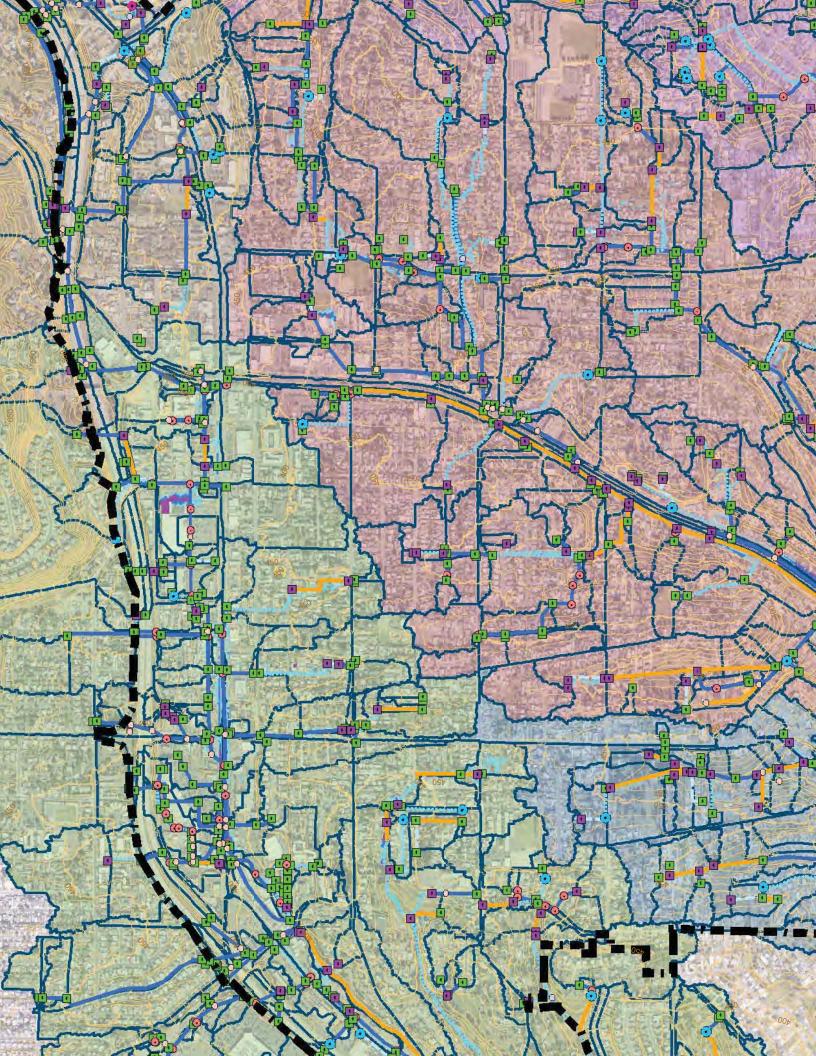


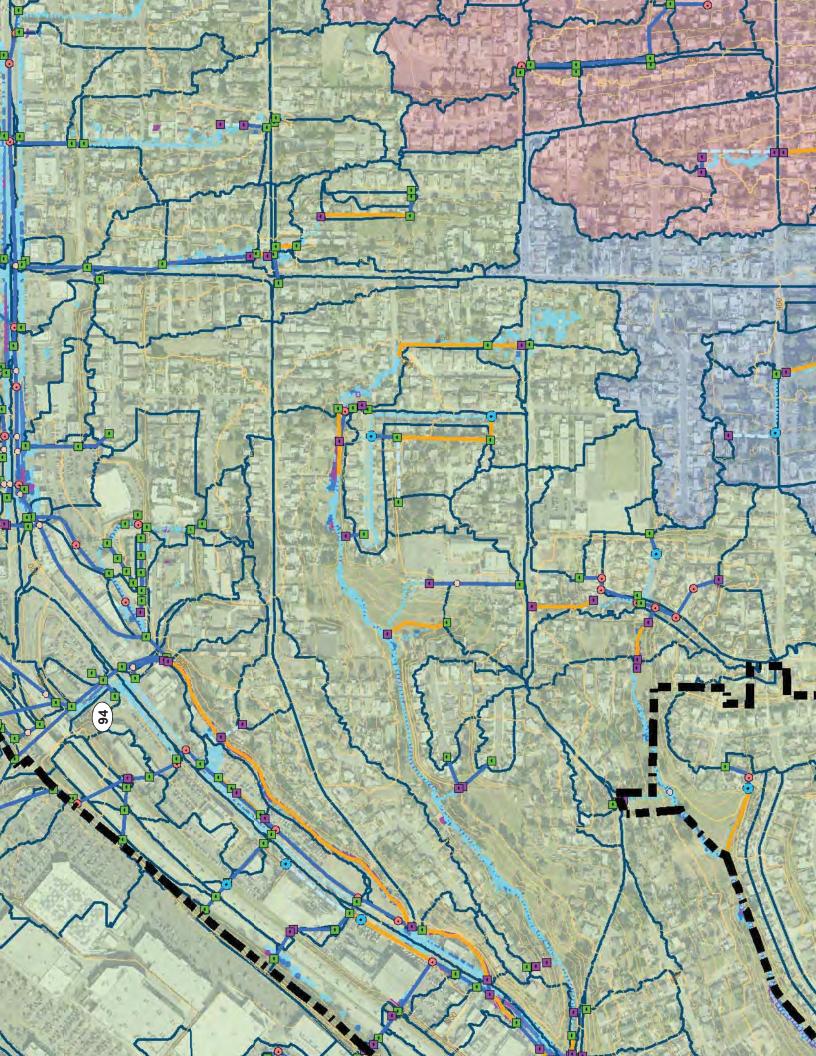


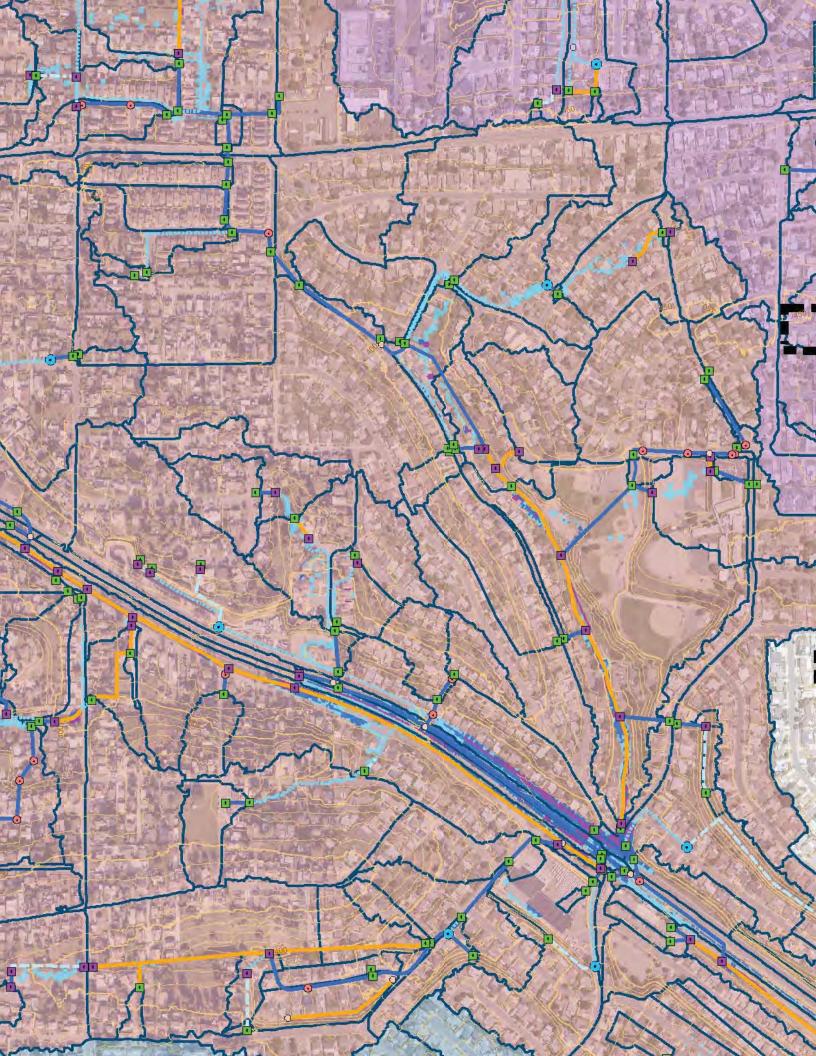


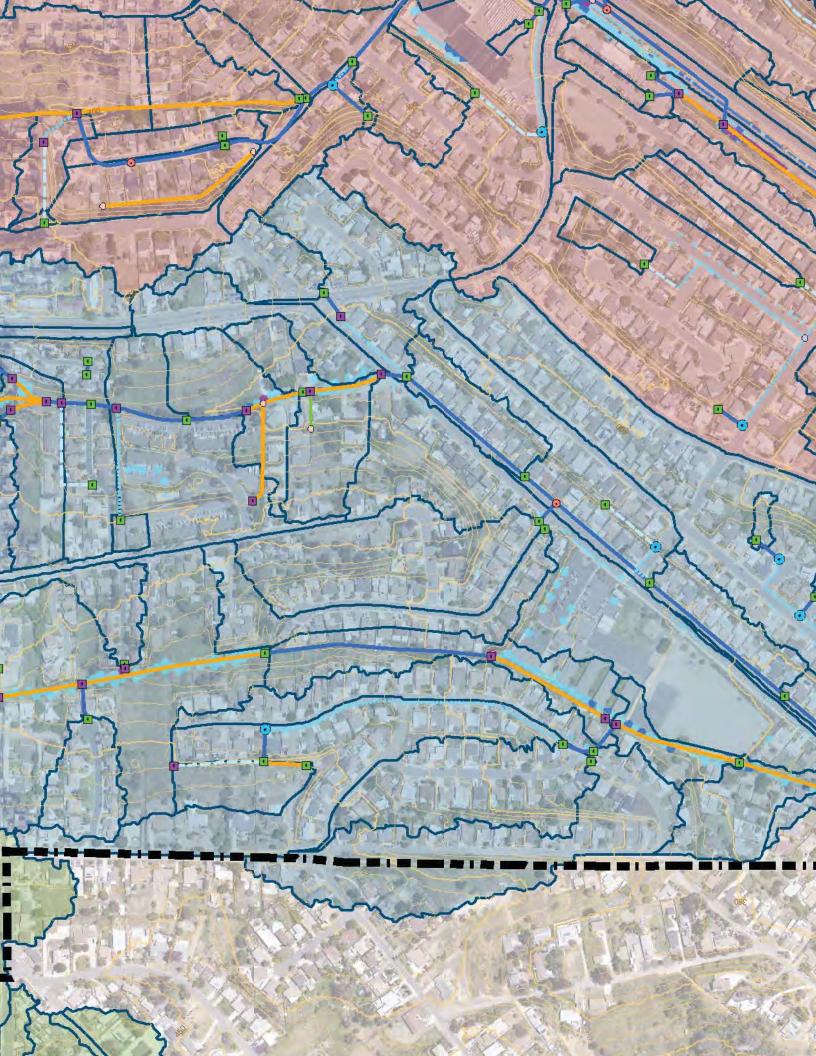


D. Inundation Maps

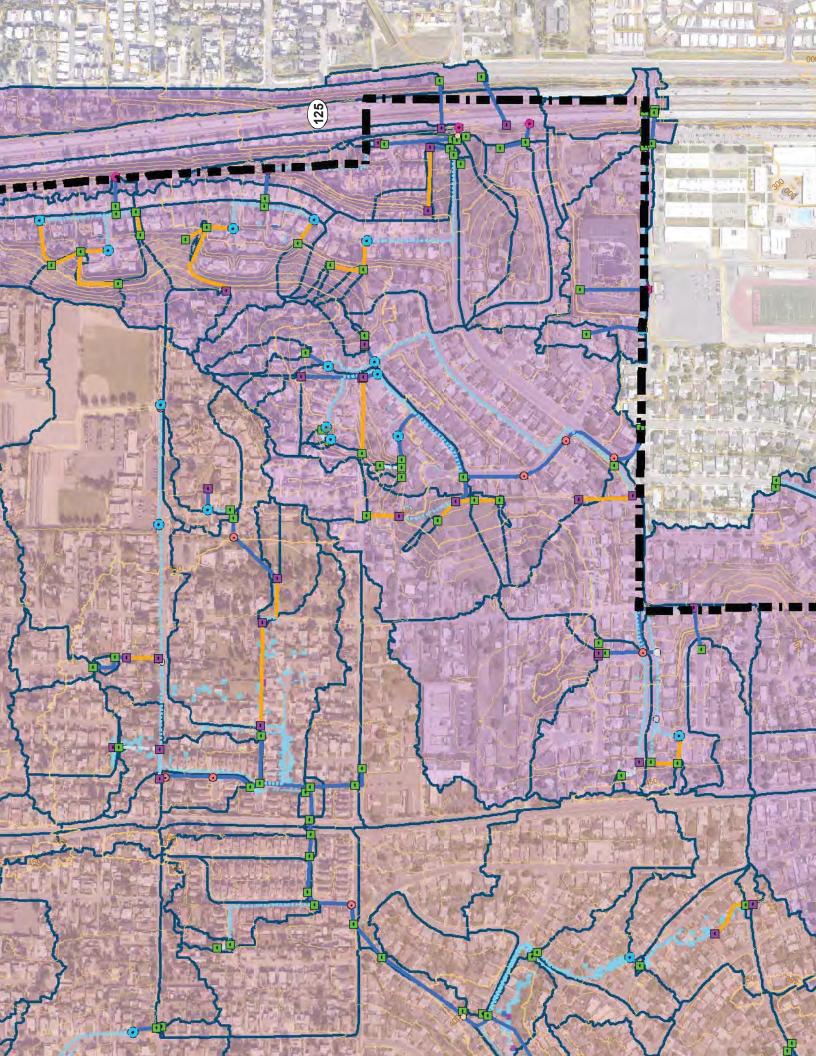


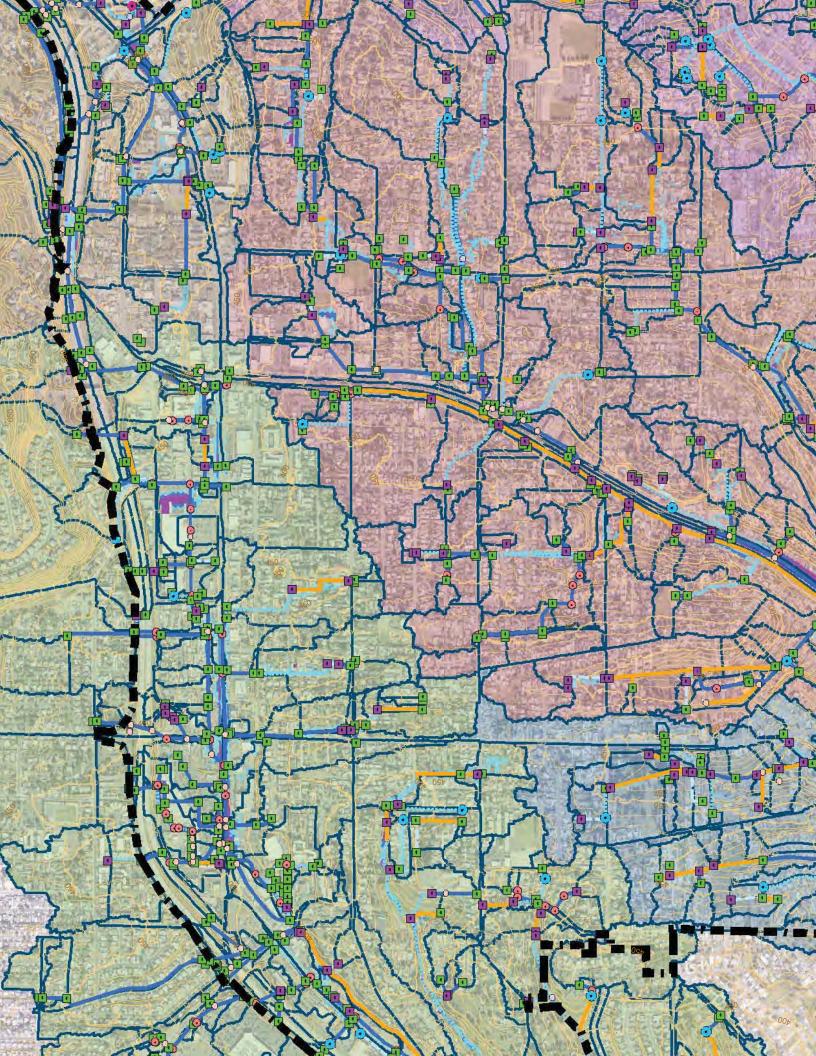


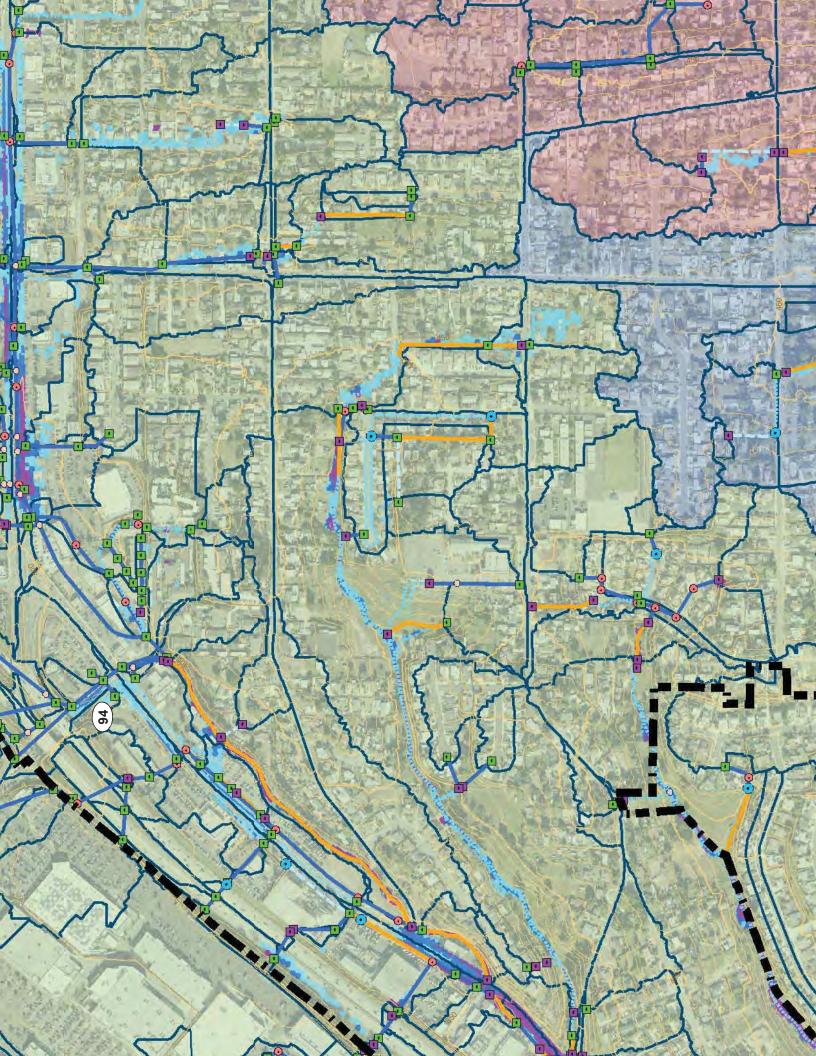


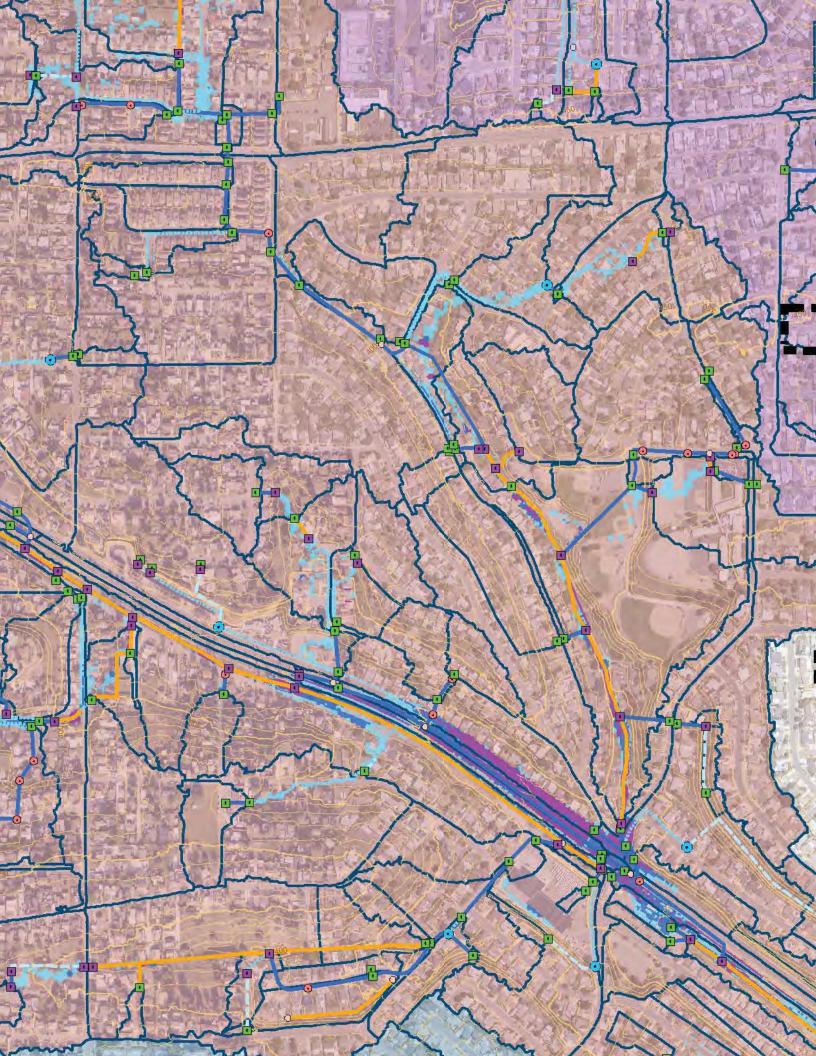


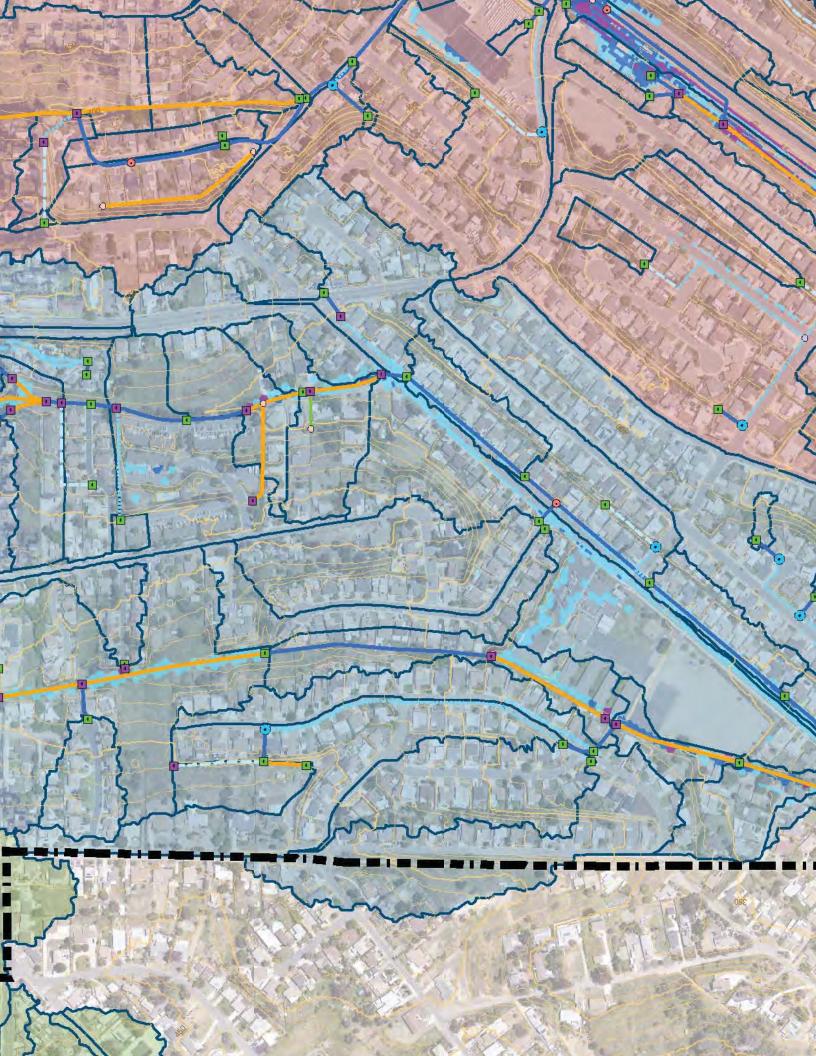




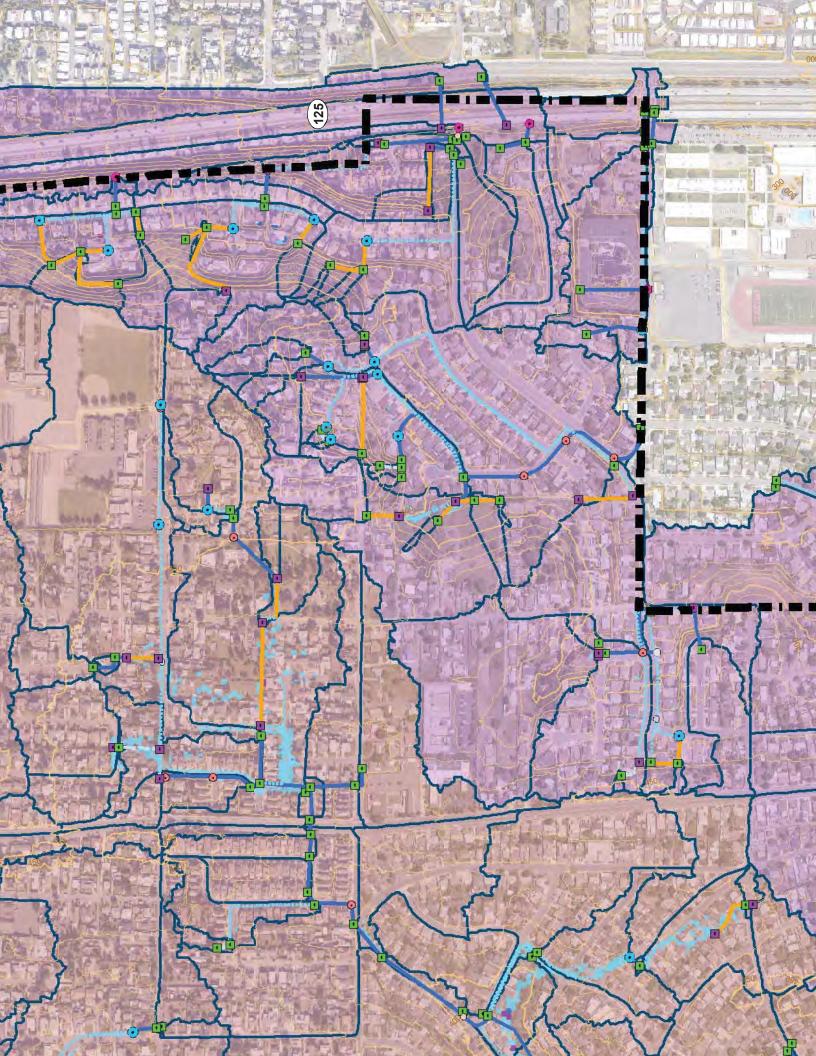


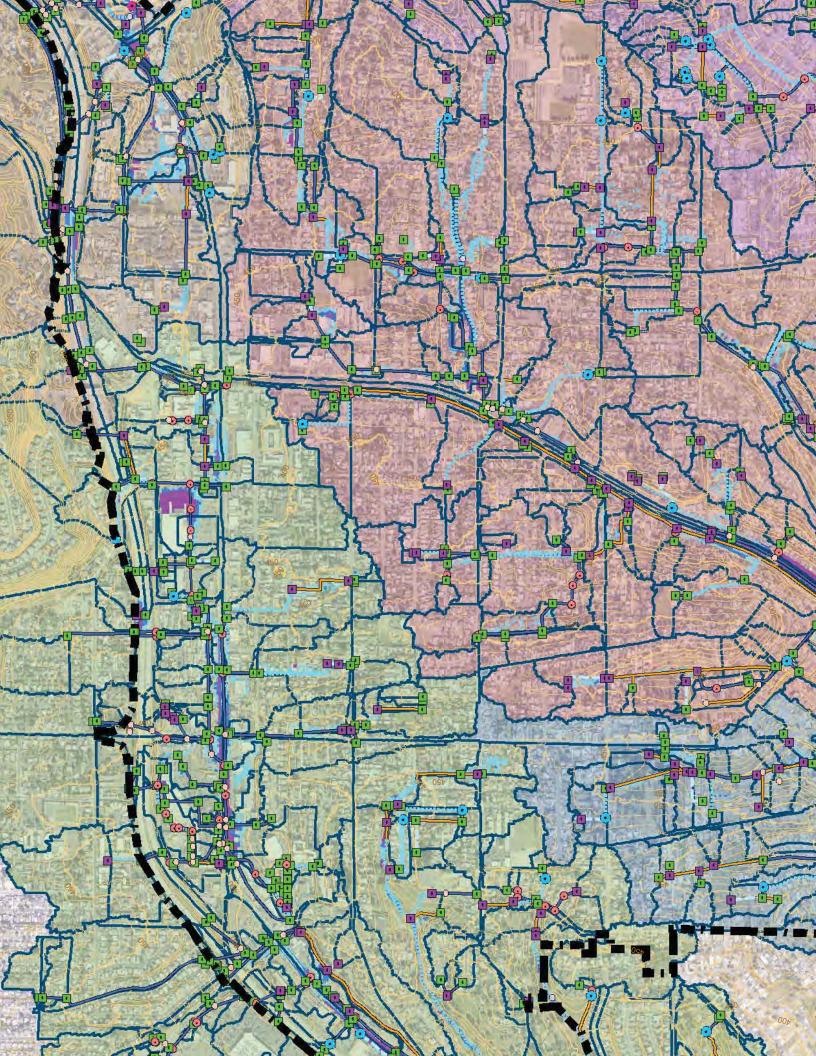


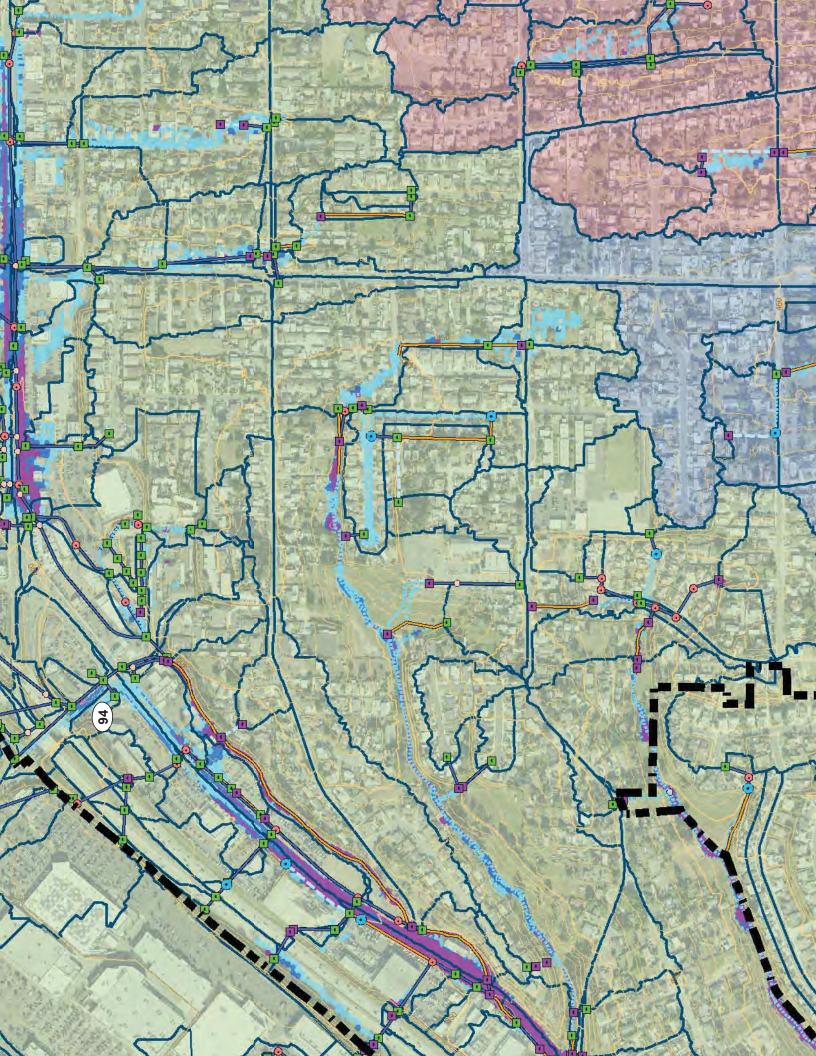


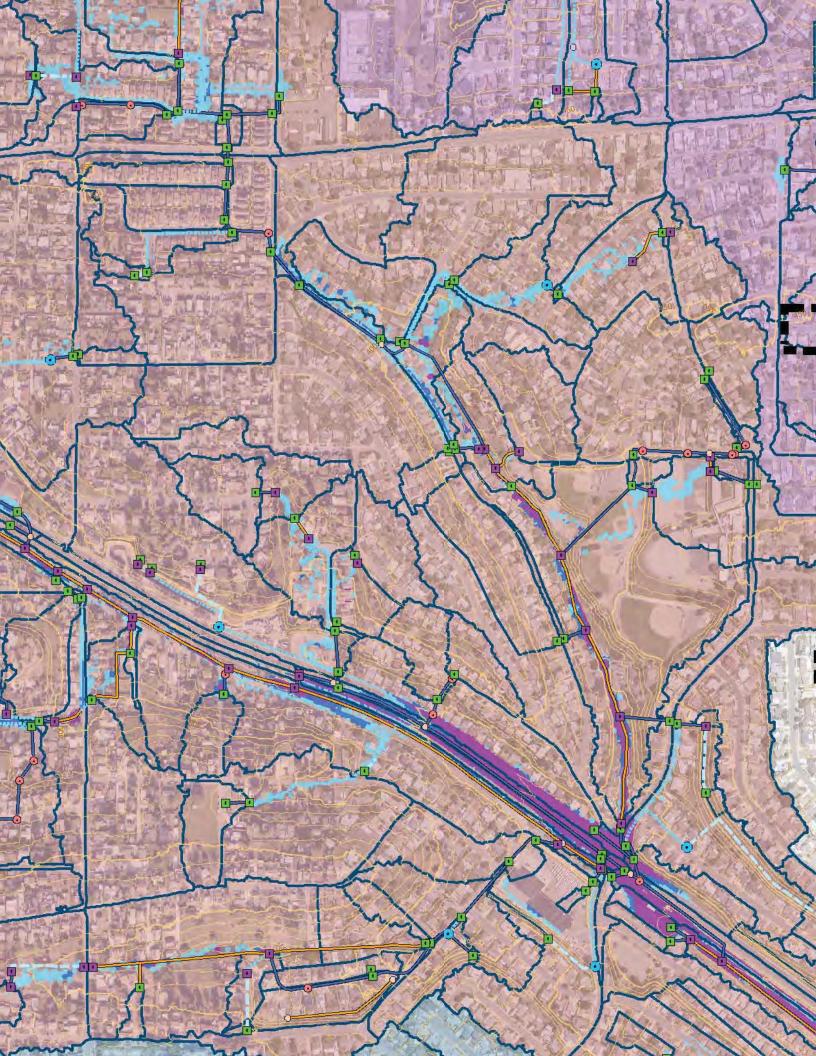


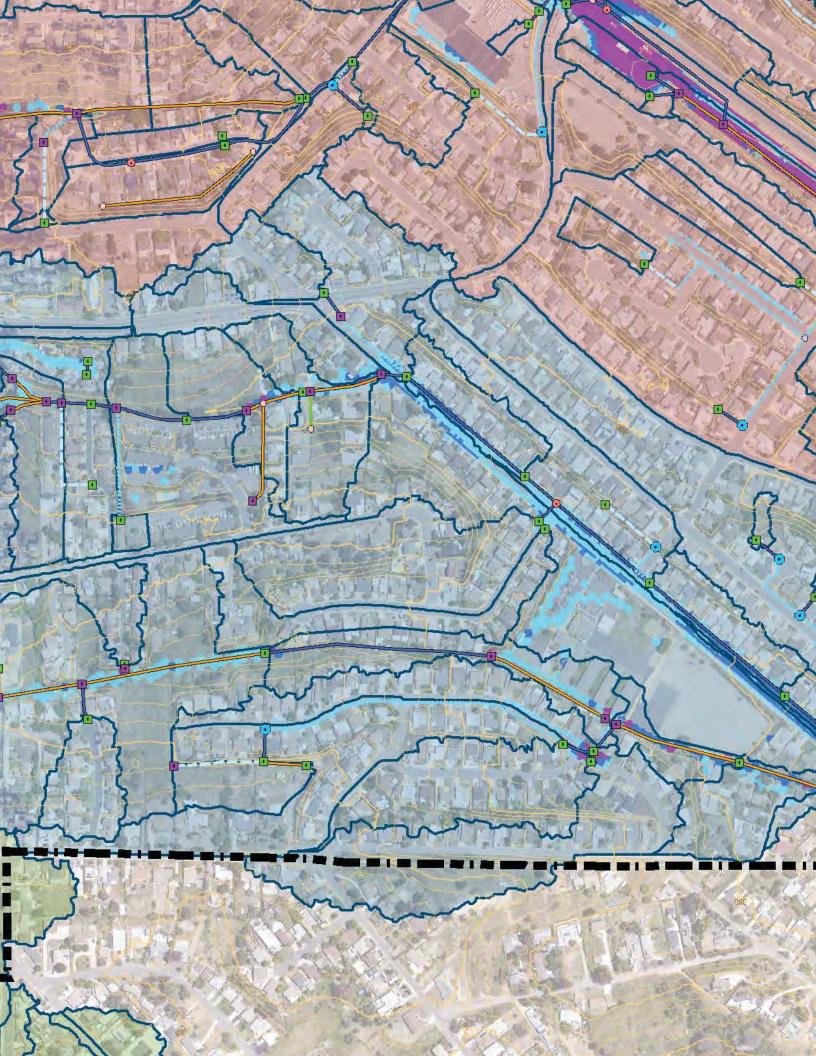




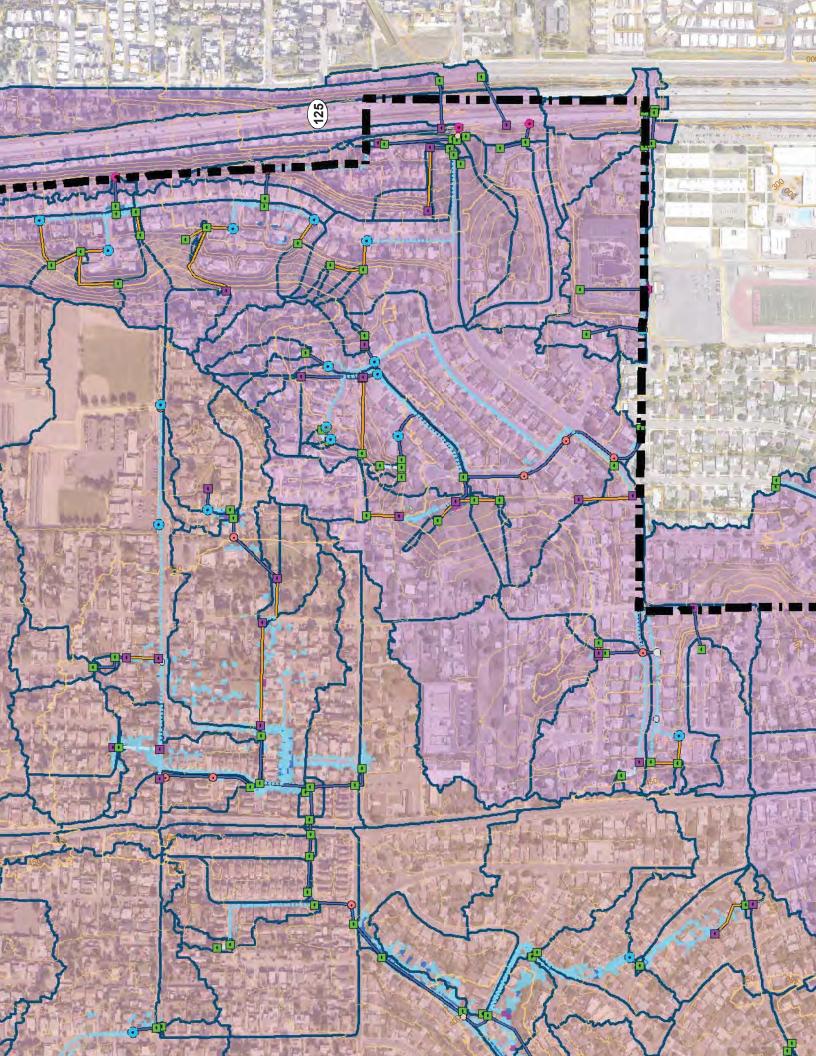


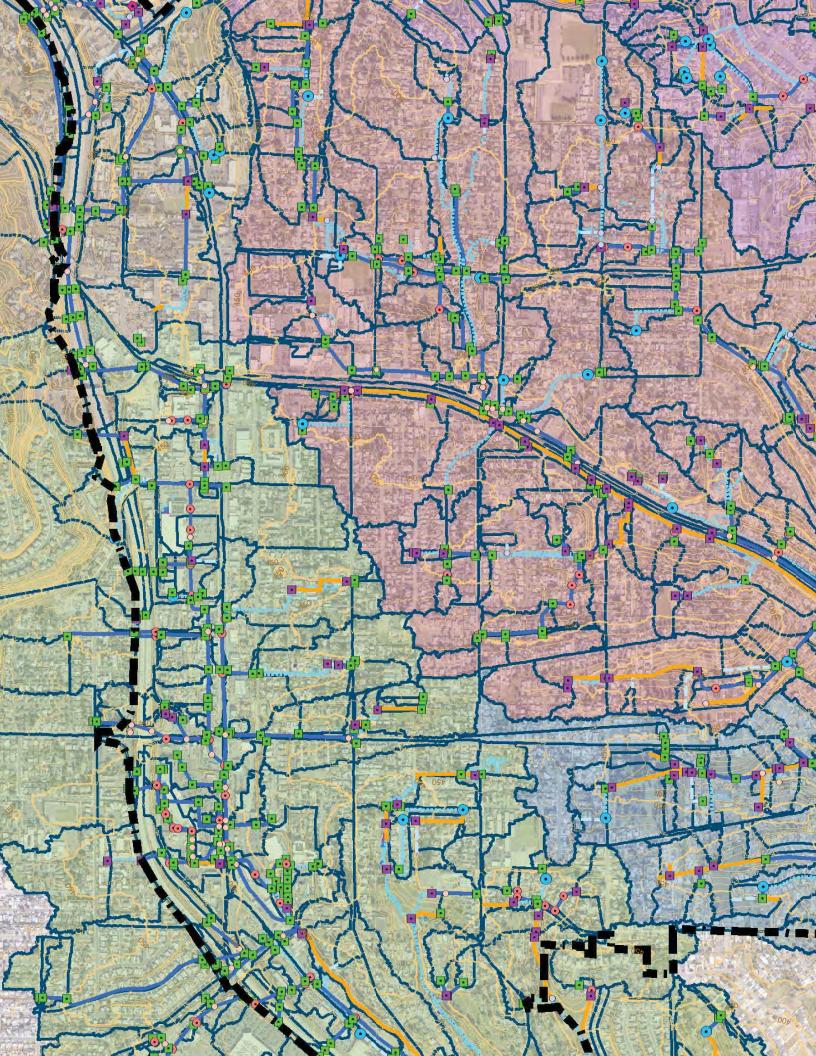


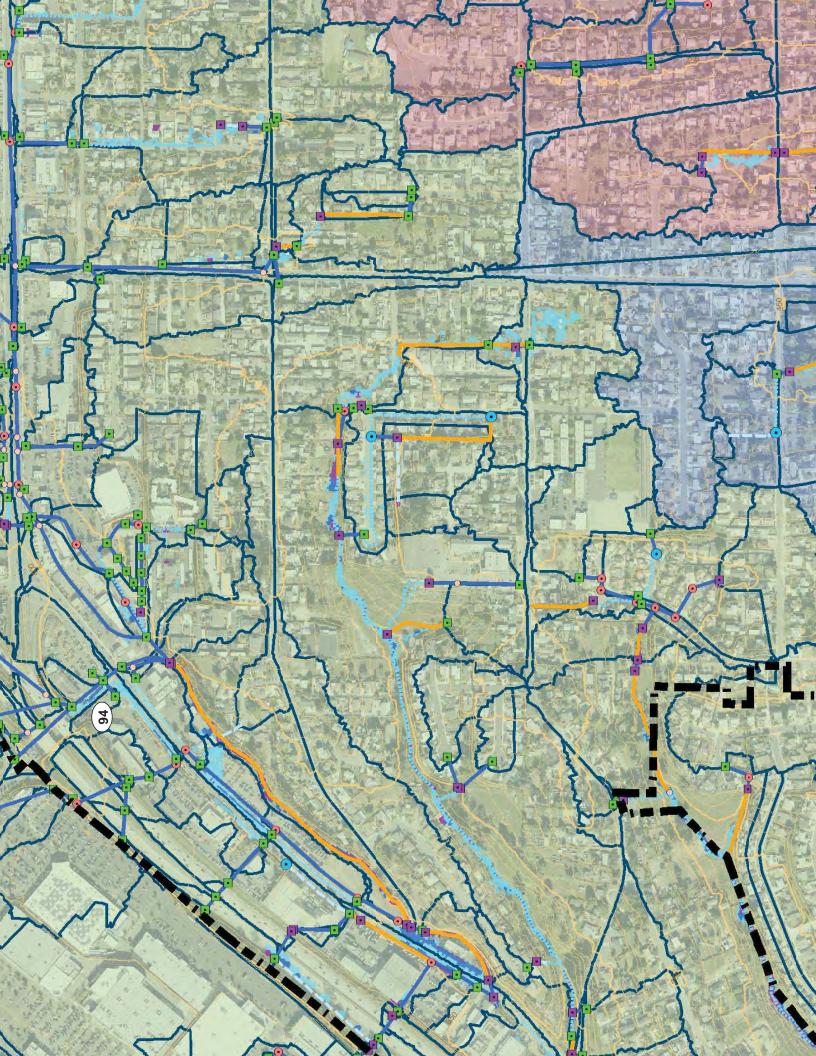


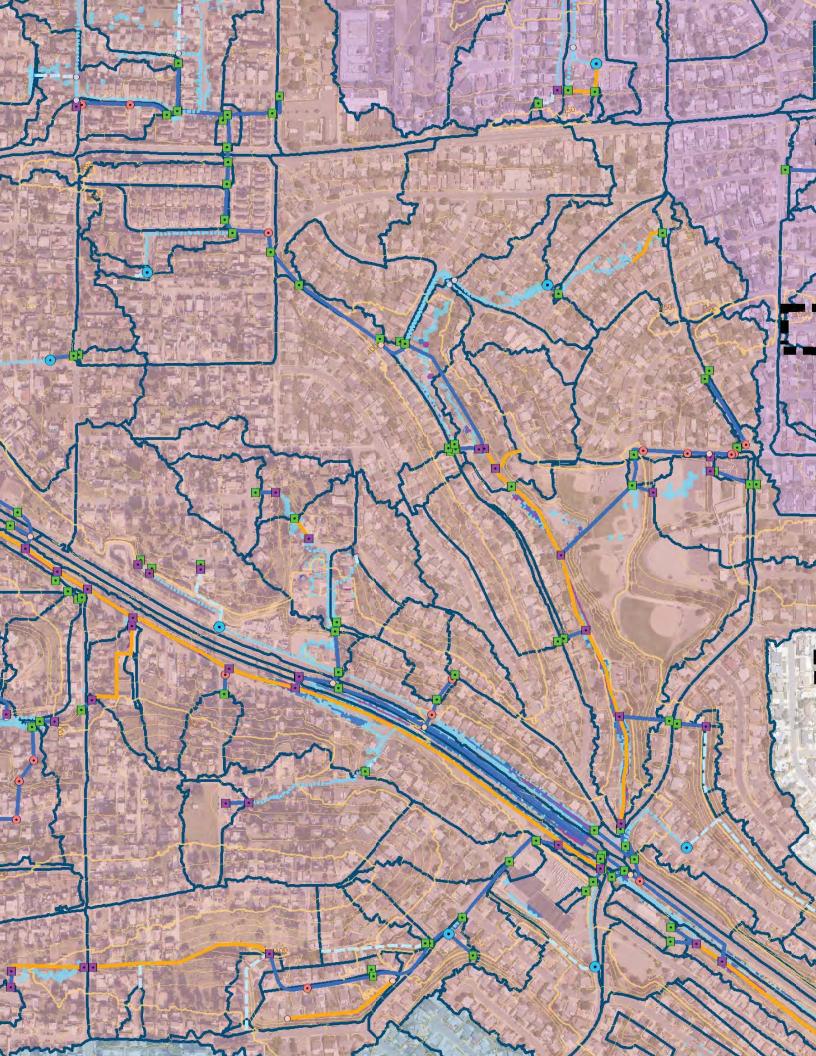


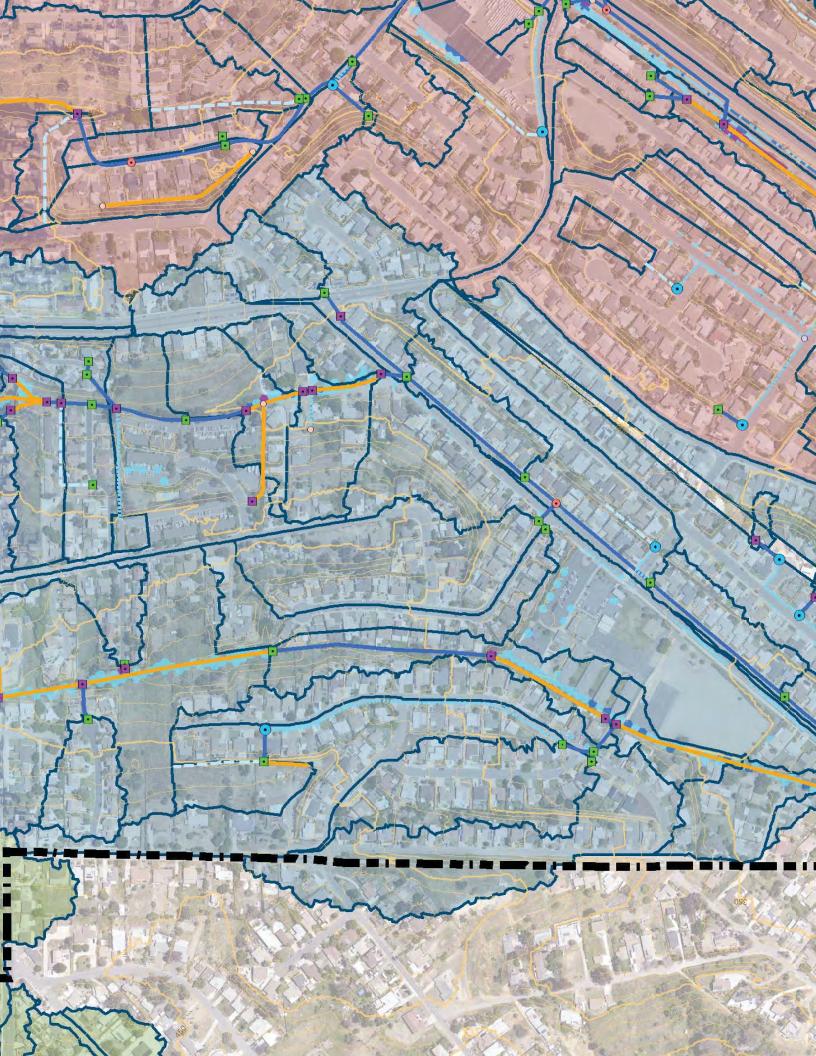




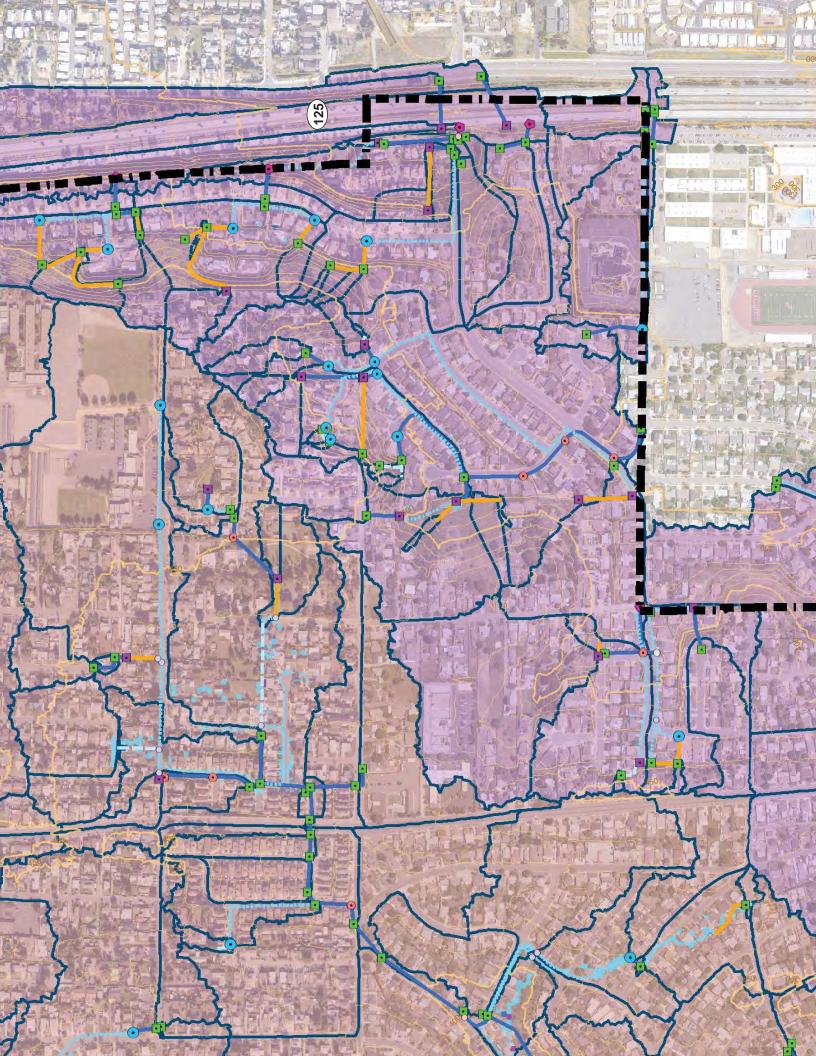


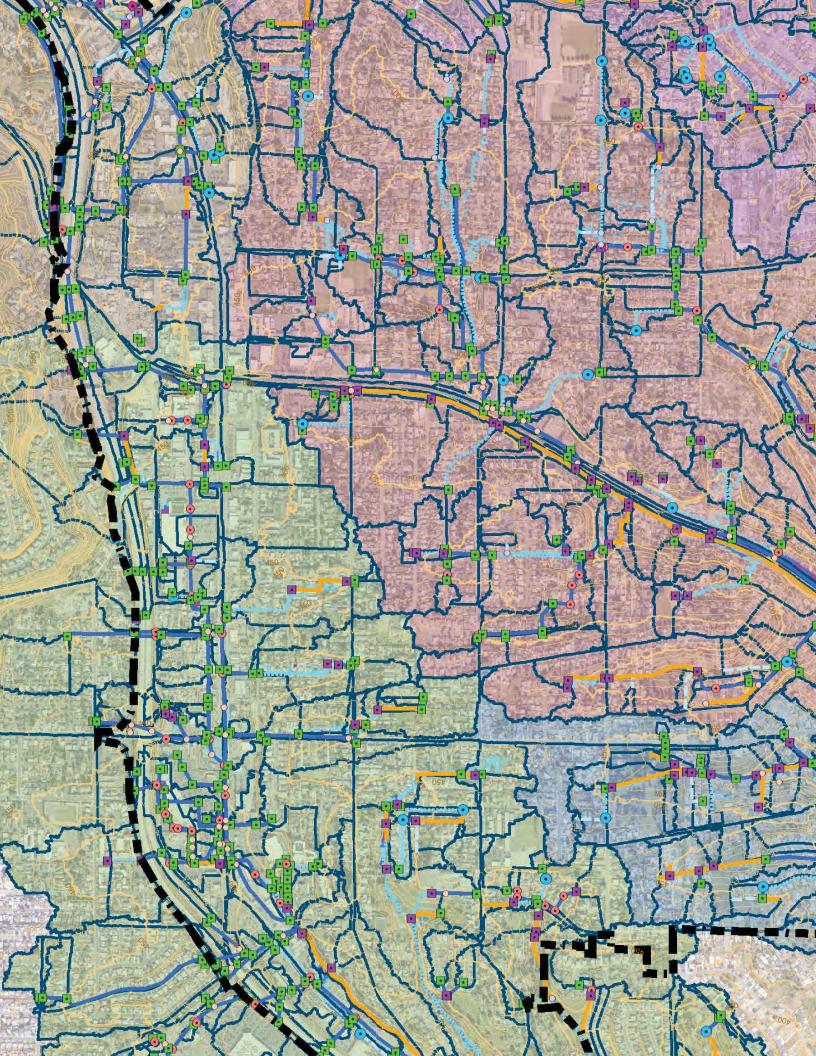


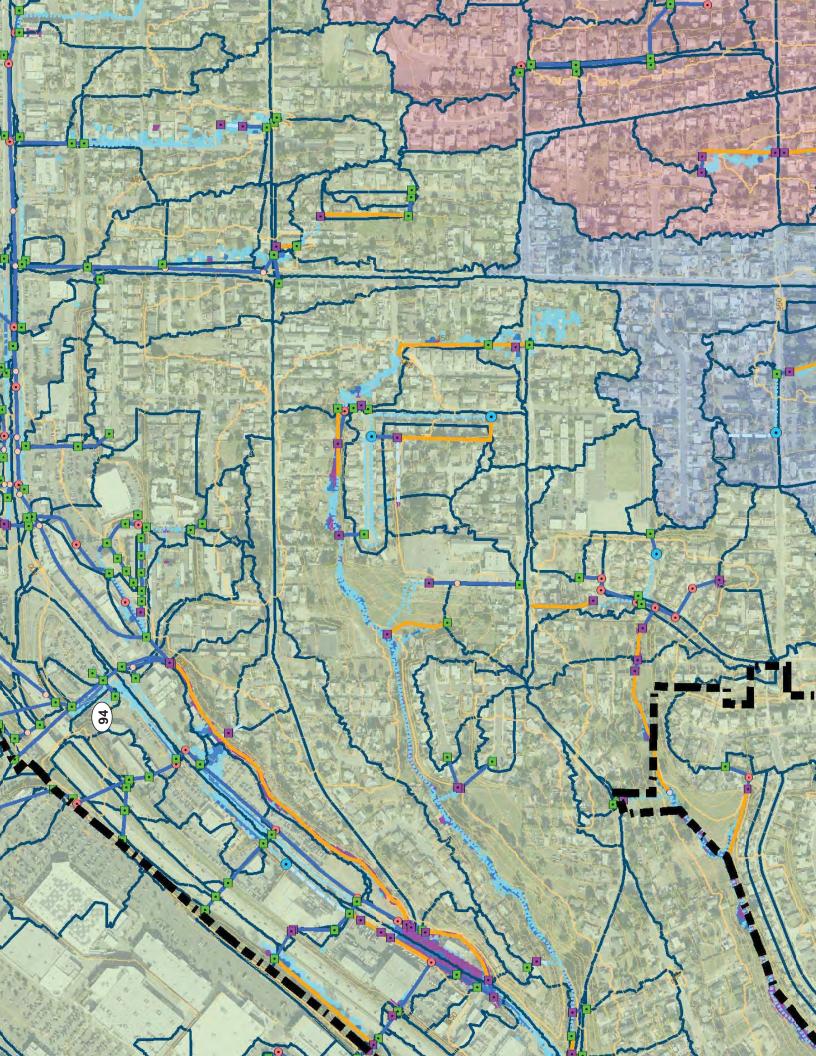


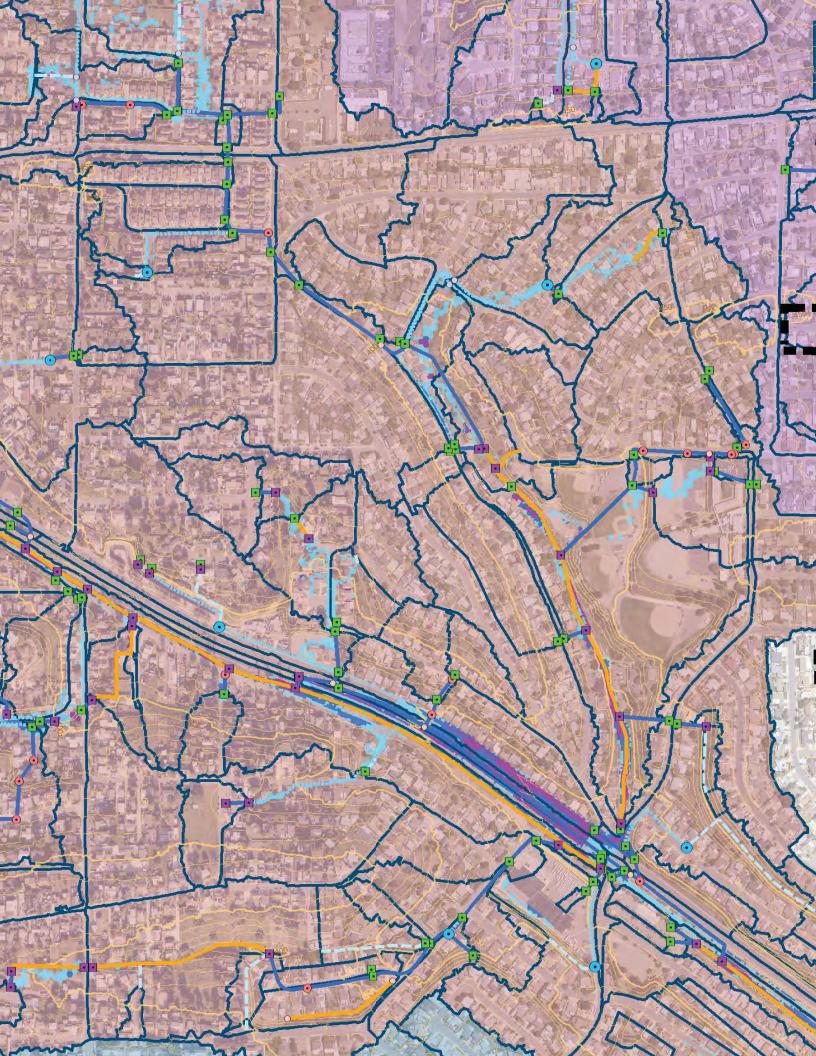


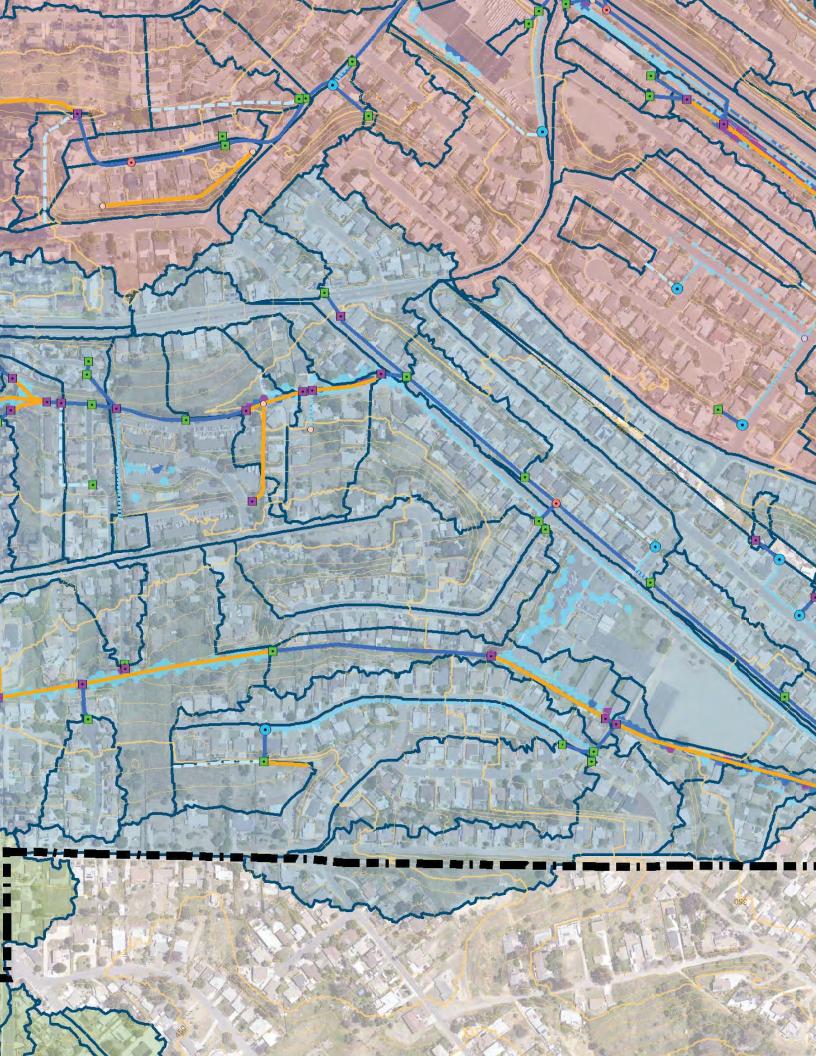




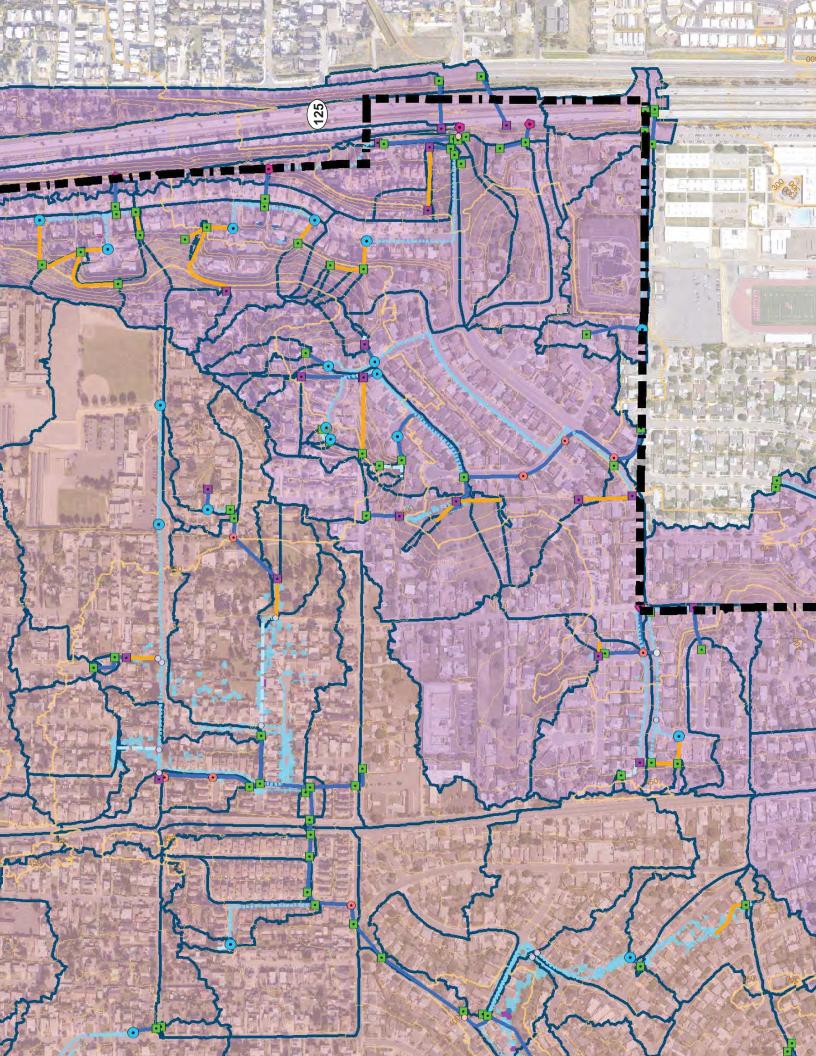


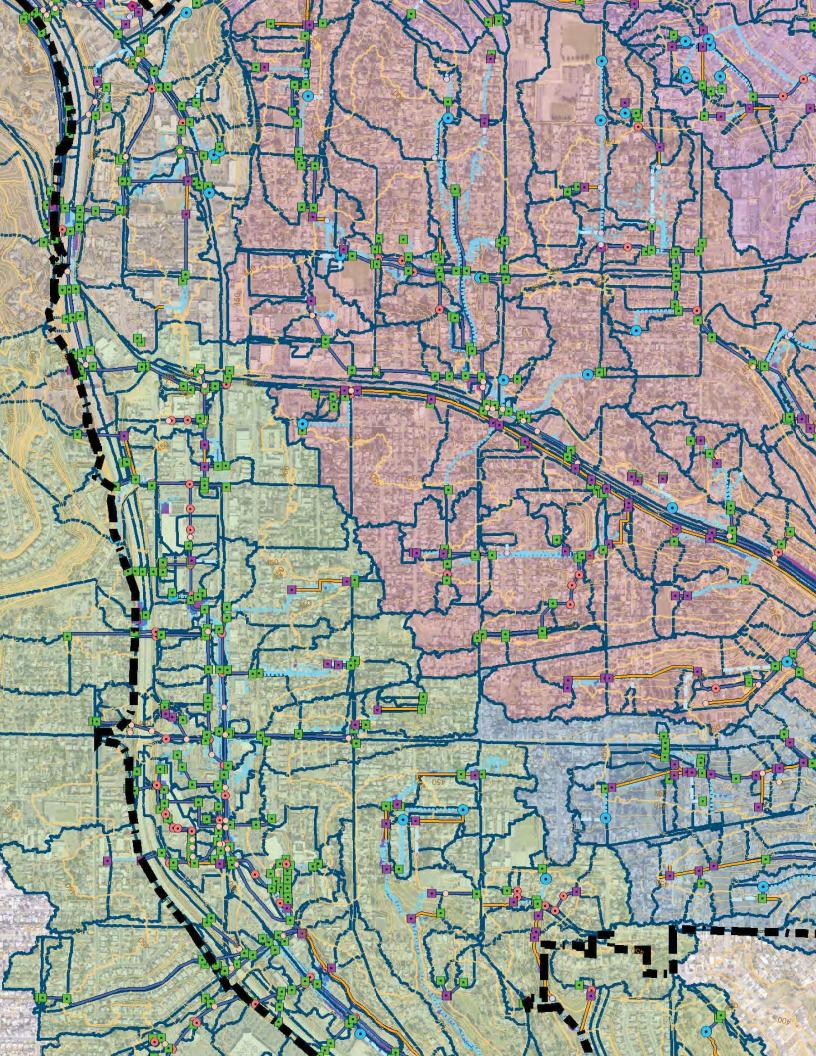


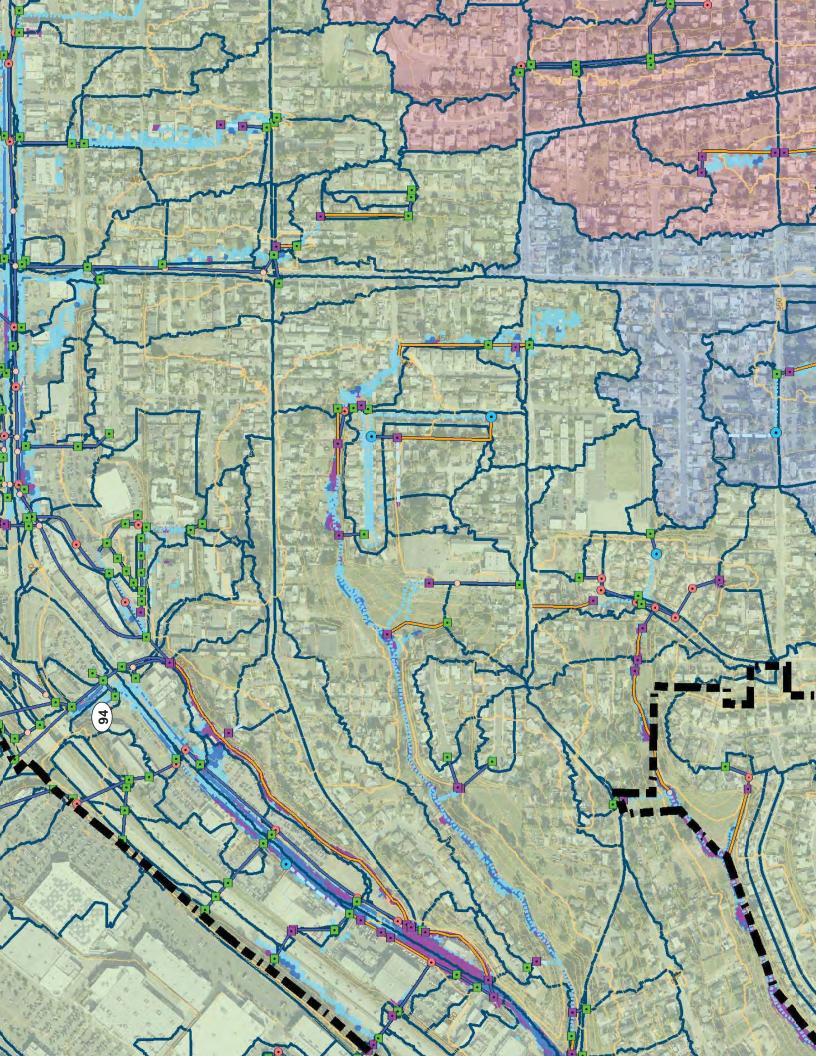


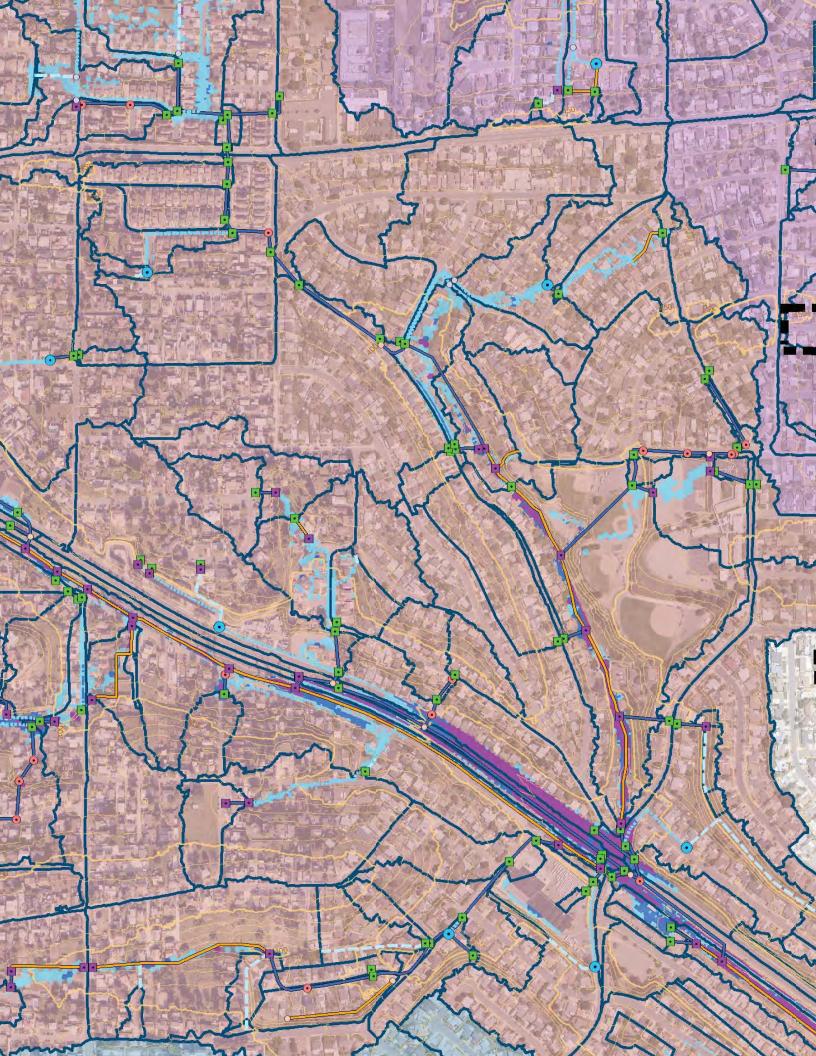


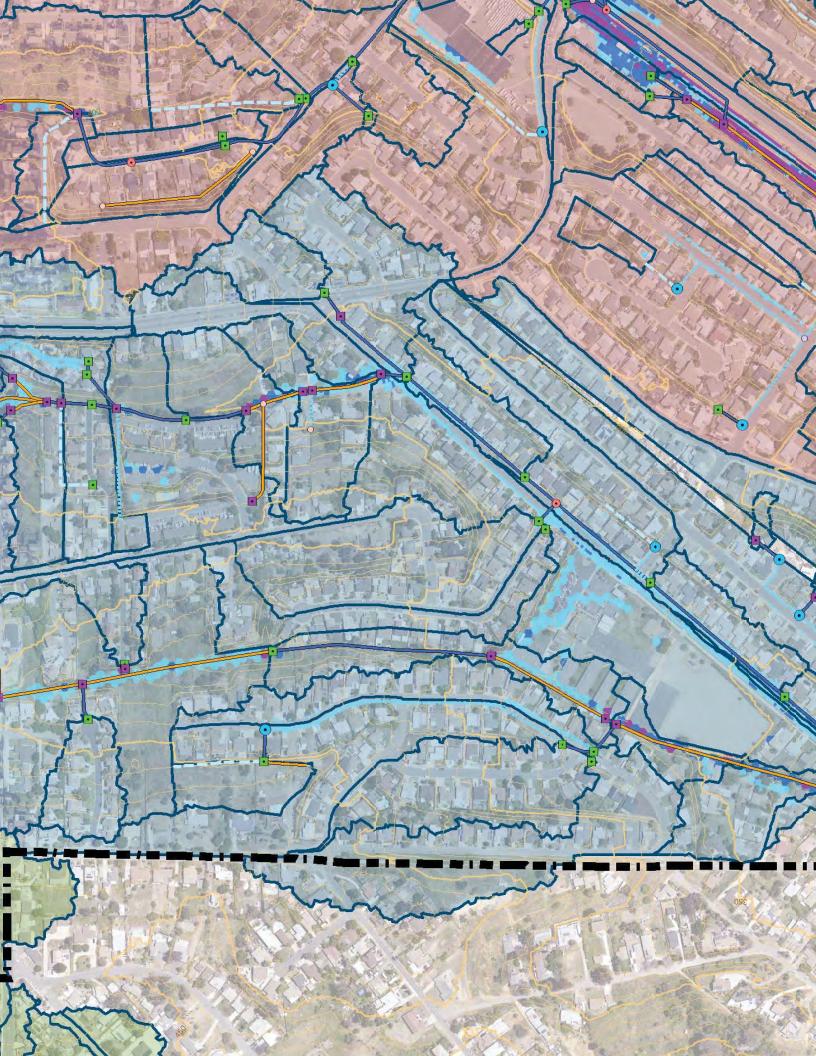




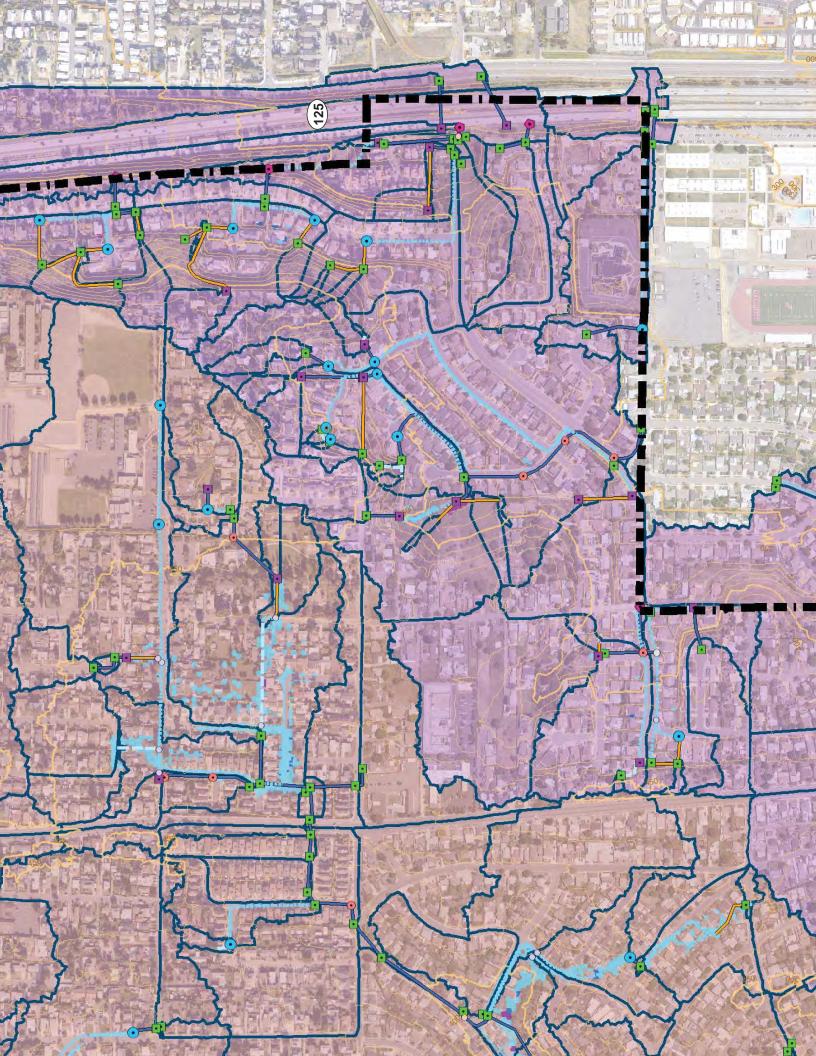




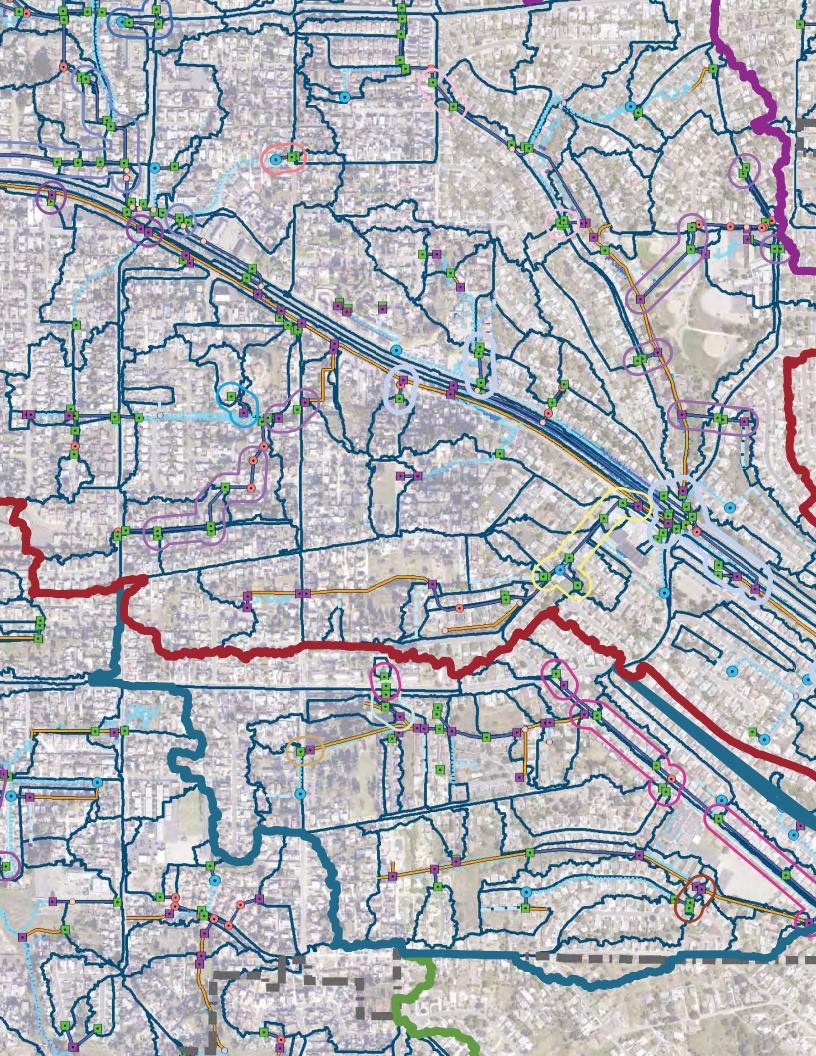


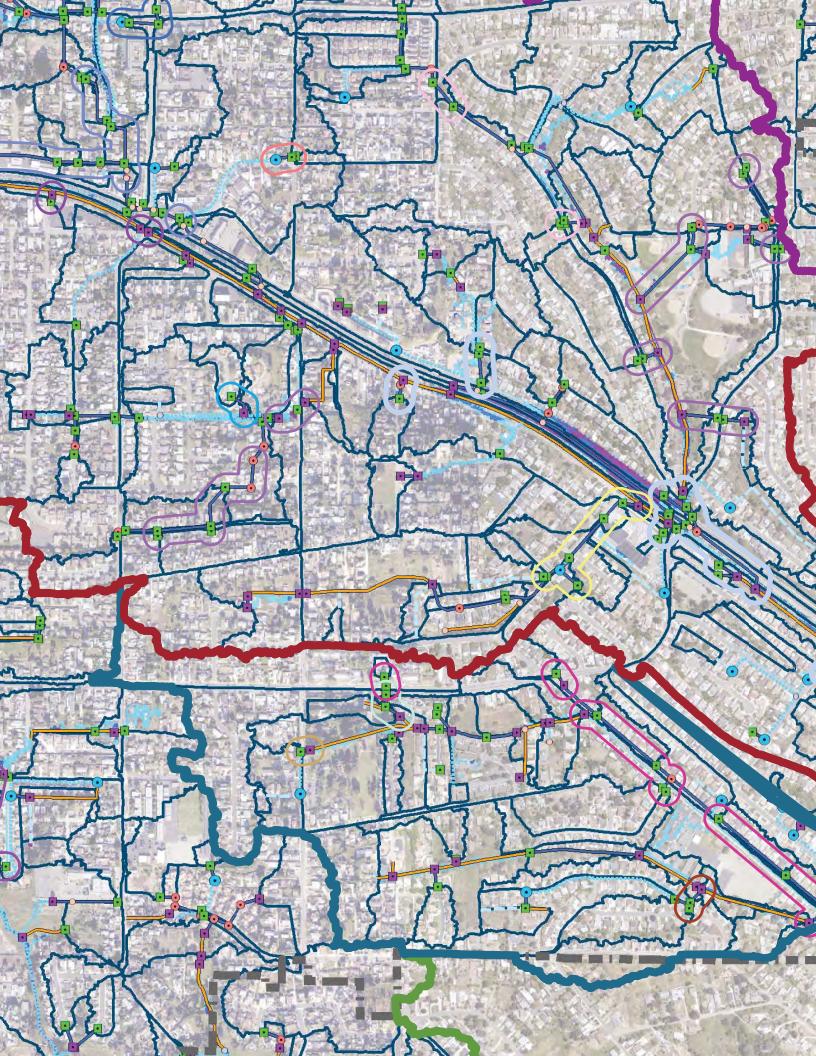


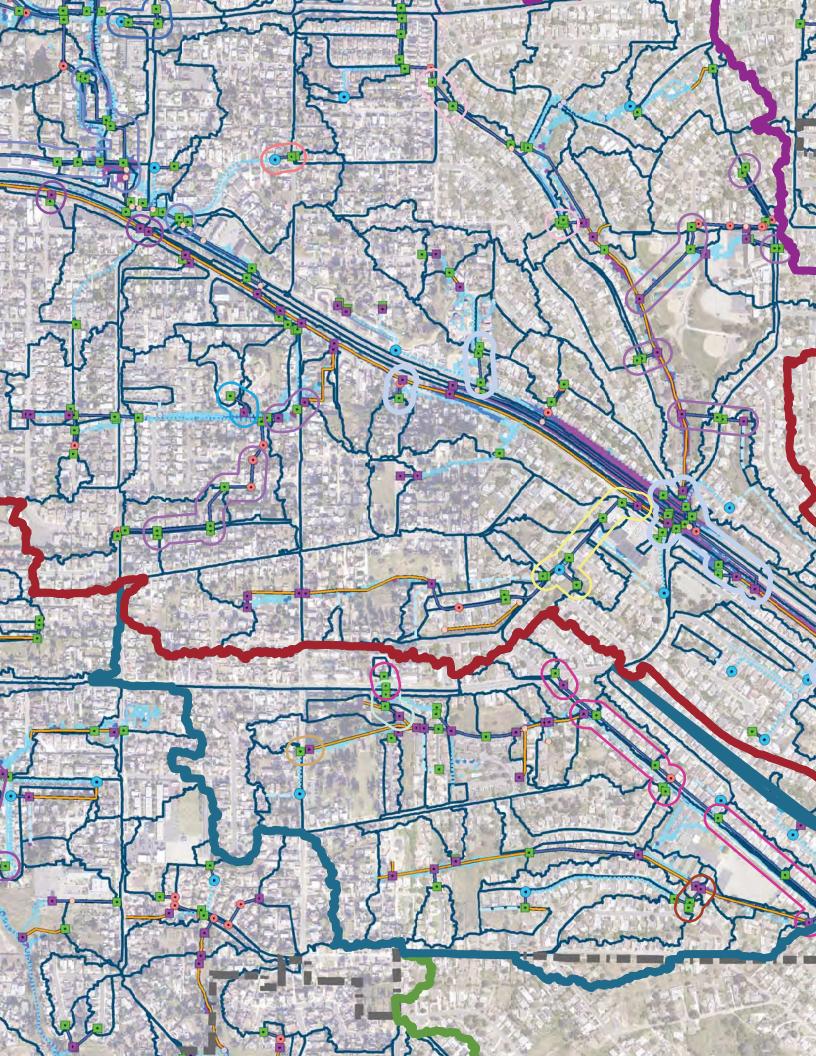


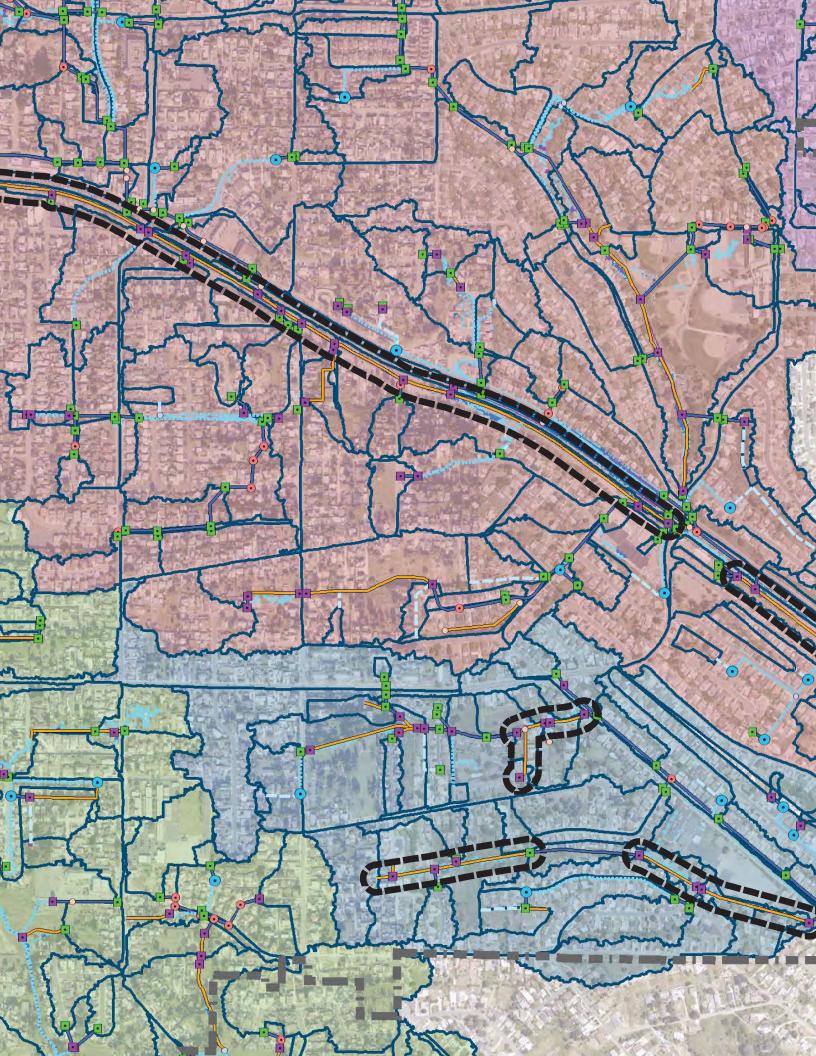


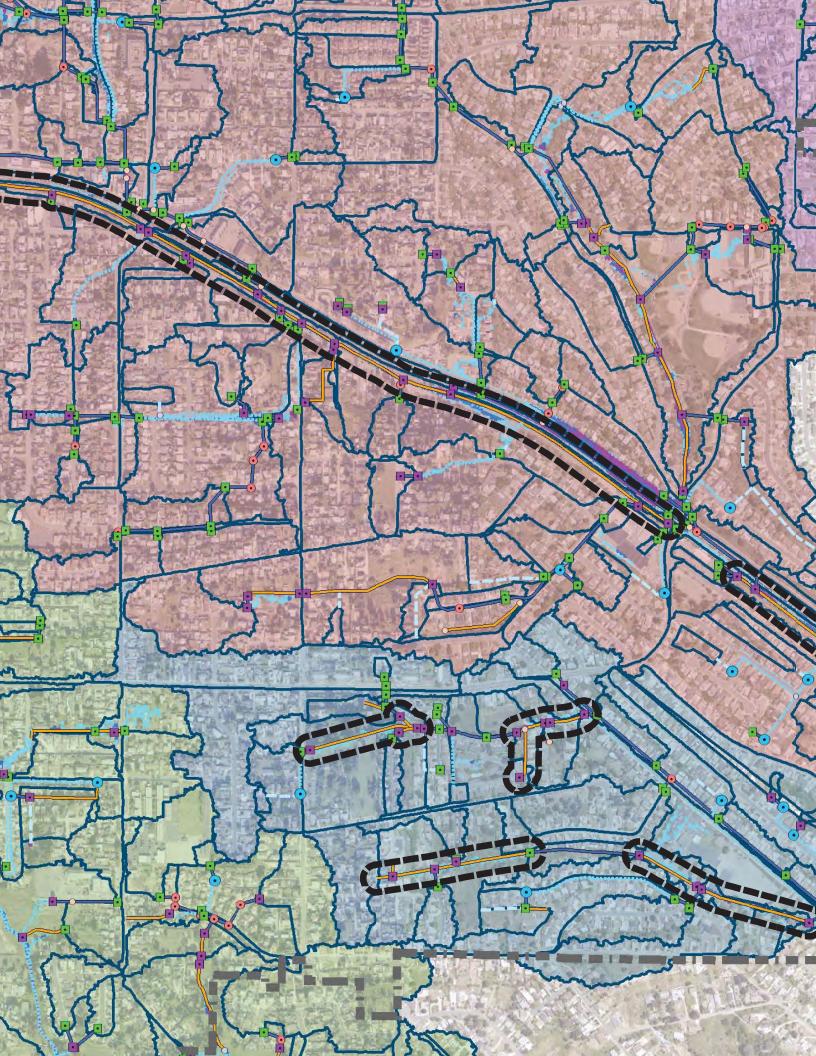
E. Proposed Conditions

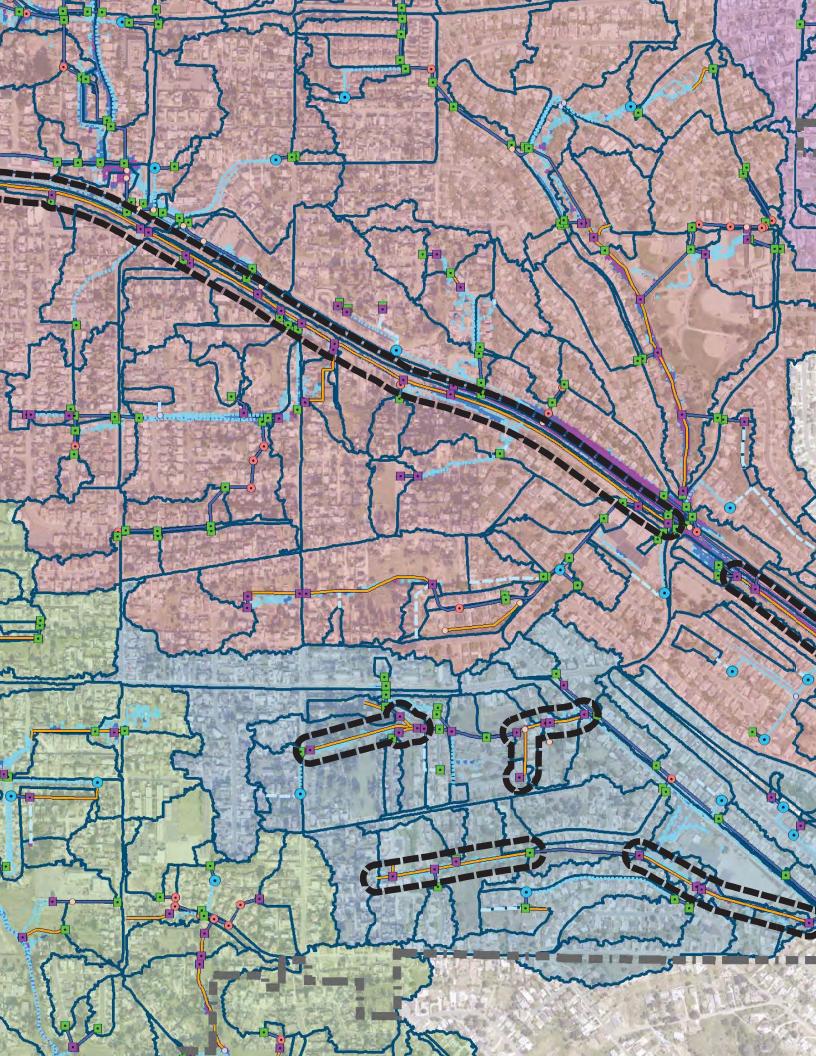












F. Summary Tables

			(cfs)		(cfs)	
20	1 RECT_OPEN	0.00662 Other	0	0	0	
0	1 CIRCULAR	0.13435 RCP	8.04	0.1	13.83	
0	1 IRREGULAR	0.09333 Earthen	4.81	0	8.3	
0	1 CIRCULAR	0.08121 RCP	0	0	6.02	
3	1 PARABOLIC	0.27746 Other	1.78	0.02	2.96	
8	1 RECT_OPEN	0.28107 Other	6.67	0.01	11.25	
0	3 CIRCULAR	0.03785 Other	175.6	0.3	223.11	
30	1 RECT_OPEN	0.00484 Other	10.27	0	30.98	
∞	1 RECT_CLOSED	0.01601 RCB	175.71	0.31	223.18	
8	1 RECT_CLOSED	0.05066 RCB	175.73	0.18	223.19	
30	1 RECT_OPEN	0.3131 Other	43.12	0	54.1	
30	1 RECT_OPEN	0.76122 Other	2.01	0	3.34	
30	1 RECT_OPEN	0.00041 Other	144.81	0.05	153.64	
30	1 RECT_OPEN	0.0104 Other	63.78	0	127.38	
0	1 CIRCULAR	0.01571 RCP	1.48	0.11	3.27	
0	1 CIRCULAR	0.04786 HDPE	5.21	0.17	8.28	
30	1 RECT_OPEN	0.04555 Other	0	0	0	
20	1 TRAPEZOIDAL	0.01244 Other	25.02	0.13	41.06	
7	1 CIRCULAR	0.00681 RCB	58.4	1.06	69.04	
0	1 CIRCULAR	0.0273 CMP	14.44	0.71	21.46	
0	1 CIRCULAR	0.0271 RCP	17.18	0.46	31.07	
0	1 CIRCULAR	0.00832 RCP	54.73	6.0	64.54	
0	1 CIRCULAR	0.08918 RCP	9.73	0.31	18.76	
0	1 CIRCULAR	0.1136 Other	0	0	0	
0	1 CIRCULAR	0.10304 Other	5.04	0.34	7.96	
0	1 CIRCULAR	0.6801 Other	2.81	0.07	4.46	
0	1 CIRCULAR	0.07777 CMP	8.39	0.25	14.6	
0	1 CIRCULAR	0.06302 Concrete	0.71	0.02	1.26	
3	1 PARABOLIC	0.01685 Other	69:0	0.03	1.24	
0	1 CIRCULAR	0.01072 Concrete	11.25	0.7	19.88	
0	1 CIRCULAR	0.00597 Concrete	15.39	1.29	27.04	
3	1 PARABOLIC	0.13008 Other	15.92	0.23	27.85	
0	1 CIRCULAR	0.0109 Other	15.86	0.67	26.9	
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0	1 CIRCULAR	0.05453 CONC	0	0	0	
0	1 CIRCULAR	0.02442 CMP	12.46	0.65	19.77	
0	1 CIRCULAR	0.01107 CONC	7.28	0.31	12.58	
0	1 CIRCULAR	0.00682 CONC	2.66	0.14	4.4	
0	1 CIRCULAR	0.00684 CONC	2.95	0.16	4.82	

			(cfs)		(cfs)	
0	1 CIRCULAR	0.0778 CONC	13.08	0.21	24.47	
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0	1 CIRCULAR	0.03638 CONC	13.1	0.3	25.56	
0	1 CIRCULAR	0.01441 RCP	15.23	0.19	26.51	
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0	1 CIRCULAR	0.00778 CONC	49.66	0.39	78.67	
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0	1 CIRCULAR	0.49848 CONC	0	0	0	
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0	1 CIRCULAR	0.11358 RCP	13.72	0.18	24.11	
0	1 CIRCULAR	0.0126 RCP	22.51	0.89	22.81	
0	1 CIRCULAR	0.00215 RCP	22.5	2.15	22.79	
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0	1 CIRCULAR	0.03039 RCP	2.51	0.14	4.4	
0	1 CIRCULAR	0.01047 RCP	3.21	0.3	5.53	
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0	1 CIRCULAR	0.02806 RCP	20.08	1.14	25.42	
0	1 CIRCULAR	0.28995 RCP	20.99	0.17	27.07	
3	1 PARABOLIC	0.14718 Concrete	1.65	0.03	2.26	
0	1 CIRCULAR	0.0249 CONC	25.63	0.4	37.15	
0	1 CIRCULAR	0.00374 CONC	1.61	0.25	2.69	
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			(cfs)		(cfs)	
0	1 CIRCULAR	0.00813 CONC	0.32	0.02	0.5	
0	1 CIRCULAR	0.28118 CONC	0.31	0	0.5	
0	1 CIRCULAR	0.0076 CONC	1.77	0.00	5.7	
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0	1 IRREGULAR	0.26594 Other	0.04	0	90.0	
3	1 PARABOLIC	0.17654 Other	0.1	0	0.19	
3	1 PARABOLIC	0.03167 Other	1.05	0.04	1.67	
0	1 CIRCULAR	0.01884 CONC	0.4	0.01	0.63	
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0	1 CIRCULAR	0.01155 CONC	1.97	80.0	3.12	
0	1 CIRCULAR	0.00646 CONC	0.28	0.02	0.43	
0	1 CIRCULAR	0.05241 CONC	43.12	0.13	54.1	
0	1 CIRCULAR	0.01477 CMP	12.12	0.81	11.54	
0	1 CIRCULAR	0.06713 CONC	1.39	0.02	2.25	
0	1 CIRCULAR	0.04016 CONC	43.13	0.15	54.1	
0	1 CIRCULAR	0.27741 CONC	41.91	0.35	52.14	
0	1 CIRCULAR	0.07911 CONC	1.14	0.02	1.75	
0	1 CIRCULAR	0.02972 CONC	40.14	1.03	49.67	
0	1 CIRCULAR	0.15393 CONC	0.48	0.01	0.75	
0	1 CIRCULAR	0.08633 CONC	0.48	0.01	0.74	
0	1 CIRCULAR	0.02973 CONC	40.18	1.03	49.67	
0	1 CIRCULAR	0.01295 CONC	0.32	0.01	3.71	
0	1 CIRCULAR	0.15413 CONC	3.41	0.04	5.79	
0	1 CIRCULAR	0.03219 CONC	3.42	80:0	5.79	
0	1 CIRCULAR	0.02973 CONC	36.22	0.93	45.48	
0	1 CIRCULAR	0.02972 CONC	3.7	60.0	6.46	
0	1 CIRCULAR	0.045 CONC	30.8	0.35	50.52	
0	1 CIRCULAR	0.03859 CONC	1.66	0.02	2.8	
0	1 CIRCULAR	0.00554 CONC	5.88	0.35	10.8	

			(cfs)		(cfs)	
0	1 CIRCULAR	0.00118 CONC	8.25	0.59	10.27	
0	1 CIRCULAR	0.00118 CONC	43.91	3.12	44.35	
0	1 CIRCULAR	0.00117 CONC	44.51	5.75	45.29	
0	1 CIRCULAR	0.01145 CONC	0.56	0.05	0.91	
0	1 CIRCULAR	0.01325 CONC	99:0	0.03	1.08	
0	1 CIRCULAR	0.16198 CONC	0.81	0.01	1.31	
0	1 CIRCULAR	0.0143 CONC	0.48	0.05	0.77	
0	1 CIRCULAR	0.00604 CONC	0.52	0.03	0.84	
0	1 CIRCULAR	0.27246 RCP	0.05	0	0.1	
0	1 CIRCULAR	0.08137 RCP	2.48	0.05	4.64	
0	1 CIRCULAR	0.14974 CONC	16.74	0.11	30.41	
0	1 CIRCULAR	0.0177 RCP	13.52	0.45	23.67	
0	1 IRREGULAR	0.11937 Concrete	3.18	0	5.22	
0	1 CIRCULAR	0.03075 CONC	0	0	2.66	
0	1 CIRCULAR	0.04315 RCP	11.01	0.23	19.41	
0	1 CIRCULAR	0.11215 ABS	19.46	0.0	21.19	
0	1 CIRCULAR	0.00902 RCP	53.35	0.56	85.72	
9	1 TRIANGULAR	0.00689 CONC	0.29	0.02	0.72	
0	1 CIRCULAR	0.01009 RCP	60.46	0.45	101.98	
3	1 PARABOLIC	0.07516 Concrete	0.5	0.02	0.61	
0	1 CIRCULAR	0.01528 RCP	12.94	0.46	22.72	
0	1 CIRCULAR	0.36589 RCP	12.95	60.0	22.74	
0	1 CIRCULAR	0.31957 RCP	12.95	0.1	22.73	
0	1 CIRCULAR	0.00616 RCP	12.89	0.73	25.27	
0	1 CIRCULAR	0.00941 CONC	3.18	0.14	5.23	
0	1 CIRCULAR	0.26871 RCP	12.89	0.11	24.49	
0	1 CIRCULAR	0.00918 RCP	13.37	0.62	25.8	
0	1 CIRCULAR	0.01035 CONC	24.74	0.36	41.75	
0	1 CIRCULAR	0.03263 RCP	50.65	0.45	85.47	
0	1 CIRCULAR	0.14147 RCP	50.7	0.33	85.5	
0	1 CIRCULAR	0.04496 RCP	48.3	0.56	81.54	
0	1 CIRCULAR	0.06107 RCP	0.62	0.05	0.98	
0	1 CIRCULAR	0.02665 RCP	3.35	0.2	5.76	
0	1 CIRCULAR	0.00693 RCP	1.58	0.08	2.66	
0	1 CIRCULAR	0.00944 RCP	9.81	96.0	17.64	
0	1 CIRCULAR	0.033 RCP	2.21	0.12	3.9	
0	1 CIRCULAR	0.04284 RCP	3.1	0.14	5.45	
0	1 CIRCULAR	0.06509 RCP	9.82	0.37	17.65	
0	1 CIRCULAR	0.0756 RCP	0.62	0.00	0.98	
0	1 CIRCULAR	0.01109 RCP	0.75	0.07	1.22	
0	1 CIRCULAR	0.01744 RCP	5.06	0.36	8.73	
0	1 CIRCULAR	0.0543 RCP	4.91	0.2	8.85	

			(cfs)		(cfs)	
0	1 CIRCULAR	0.0869 RCP	4.98	0.16	8.82	
0	1 CIRCULAR	0.01913 RCP	4.93	0.34	8.82	
0	1 CIRCULAR	0.0049 RCP	2.75	0.37	4.94	
0	1 CIRCULAR	0.04397 RCP	12.98	0.27	22.1	
0	1 CIRCULAR	0.07376 RCP	4.18	0.15	7.14	
0	1 CIRCULAR	0.02315 RCP	2.22	0.14	3.91	
0	1 CIRCULAR	0.03348 RCP	2.21	0.11	3.9	
0	1 CIRCULAR	0.05196 RCP	24.63	0.48	41.83	
0	1 CIRCULAR	0.05642 RCP	11.45	0.21	19.59	
0	1 CIRCULAR	0.47787 RCP	1.18	0.02	1.88	
0	1 IRREGULAR	0.06202 Earthen	24.54	0	33.7	
0	1 IRREGULAR	0.02075 Earthen	28.59	0	41.53	
0	1 IRREGULAR	0.01689 Earthen	28.31	0	41.22	
0	1 IRREGULAR	0.15145 Earthen	0.27	0	0.43	
0	1 IRREGULAR	0.17542 Earthen	4.25	0	7.89	
0	1 IRREGULAR	0.28537 Earthen	3.39	0	6.31	
0	1 IRREGULAR	0.17845 Earthen	20.21	0	22	
0	1 CIRCULAR	0.127 RCP	1.28	0.02	2.04	
0	1 CIRCULAR	0.02463 RCP	30.52	0.47	47.28	
0	1 CIRCULAR	0.00989 RCP	30.57	0.75	50.24	
0	1 CIRCULAR	0.03491 RCP	30.24	0.39	46.68	
0	1 CIRCULAR	0.01894 RCP	1.97	0.14	3.55	
က	1 PARABOLIC	0.03062 Concrete	0	0	0	
0	1 CIRCULAR	0.01969 RCP	2.42	0.16	4.26	
0	1 CIRCULAR	0.24242 RCP	4.25	0.08	7.89	
0	1 CIRCULAR	0.02704 RCP	4.07	0.24	7.61	
0	1 CIRCULAR	0.0339 RCP	0.78	0.04	1.21	
0	1 CIRCULAR	0.15238 RCP	3.4	0.08	6.32	
0	1 CIRCULAR	0.01441 RCP	9.0	0.02	0.92	
0	1 CIRCULAR	0.01153 RCP	19.33	1.71	19.77	
0	1 CIRCULAR	0.06287 RCP	0.3	0.01	0.47	
3	1 PARABOLIC	0.01316 Concrete	0.57	0.03	0.89	
0	1 CIRCULAR	0.02156 RCP	19.7	1.28	20.02	
0	1 CIRCULAR	0.00485 RCP	2.39	0.33	4.22	
0	1 CIRCULAR	0.02279 RCP	2.28	0.14	4.03	
0	1 CIRCULAR	0.16671 RCP	4.11	0.1	79.7	
0	1 CIRCULAR	0.02839 RCP	2.15	0.12	3.83	
0	1 CIRCULAR	0.01689 RCP	20.21	1.48	22	
3	1 PARABOLIC	0.01841 Concrete	1.06	0.04	2.16	
0	1 IRREGULAR	-0.17256 Earthen	0	0	0	
0	1 CIRCULAR	0.0145 RCP	15.25	1.21	16.99	
0	1 CIRCULAR	0.00792 RCP	1.29	0.06	2.65	

				(cfs)		(cfs)	
0	1		0.00788 RCP	154.15	0.41	261.53	
0	1		0.12586 RCP	0.64	0.05	1.06	
0	1		0.01289 RCP	13.02	1.09	14.92	
0	1	CIRCULAR	0.01166 RCP	11.85	1.04	13.91	
0	1	CIRCULAR	0.04832 RCP	1.11	0.05	2.16	
0	1	CIRCULAR	0.02709 RCP	3.29	0.19	6.1	
0	1	CIRCULAR	0.08051 RCP	4.39	0.15	7.99	
0	1	CIRCULAR	0.22803 RCP	0.56	0.01	0.95	
0	1	CIRCULAR	0.00923 RCP	9.25	0.92	11.71	
0	1	CIRCULAR	0.12857 RCP	0.99	0.03	1.82	
0	1	CIRCULAR	0.07572 RCP	66:0	0.03	1.81	
0	1	CIRCULAR	0.15911 RCP	1.37	0.03	2.28	
0	1	CIRCULAR	0.11242 CONC	3.79	0.03	9.88	
0	1	CIRCULAR	0.0122 RCP	12.41	1.07	14.31	
0	1	CIRCULAR	0.16693 RCP	4.86	0.11	8	
3	1	1 PARABOLIC	0.02936 Concrete	0	0	0	
3	1	1 PARABOLIC	0.02817 Concrete	0	0	0	
3	1	1 PARABOLIC	0.01189 Concrete	0	0	0	
3	1	1 PARABOLIC	0.04384 Concrete	0	0	0	
3	1	1 PARABOLIC	0.02529 Concrete	0	0	0	
3	1	1 PARABOLIC	0.03361 Concrete	0	0	0	
3	1	PARABOLIC	0.02587 Concrete	0	0	0	
3	1	1 PARABOLIC	0.02739 Concrete	0	0	0	
0	1	CIRCULAR	0.0872 CONC	6.84	90.0	13.16	
3	1	1 PARABOLIC	0.31866 Concrete	0	0	0	
3	1	1 PARABOLIC	0.09845 Concrete	0.57	0.01	0.89	
3	1	PARABOLIC	0.10003 Concrete	1.05	0.02	2.15	
3	1	PARABOLIC	0.01024 Concrete	1.05	90.0	2.15	
3	1	PARABOLIC	0.00908 Concrete	0.05	0	0.08	
3	1	PARABOLIC	0.11334 Concrete	0.05	0	0.08	
2	1	TRIANGULAR	0.25461 Concrete	20.21	0.09	22	
0	1	CIRCULAR	0.37845 RCP	0	0	0	
0	1	CIRCULAR	0.16515 RCP	30.1	0.18	46.39	
0	1	CIRCULAR	0.50056 RCP	0.16	0	0.24	
0	1	CIRCULAR	0.05563 RCP	24.54	0.2	33.69	
0	1	CIRCULAR	0.09183 RCP	8.0	0.01	2.29	
0	1	IRREGULAR	0.07956 Earthen	1.32	0	4.03	
0	1	1 IRREGULAR	0.16629 Earthen	2.01	0	6.18	
0	1	IRREGULAR	0.15216 Earthen	2.81	0	29.6	
3.5	1	TRIANGULAR	0.04742 Concrete	0	0	0	
3.5	1	TRIANGULAR	0.03475 Concrete	0	0	0	
3.5	1	TRIANGULAR	0.02011 Concrete	0	0	0	

			(cfs)		(cfs)
3.5	1 TRIANGULAR	0.03242 Concrete	0.57	90.0	2.4
3.5	1 TRIANGULAR	0.02978 Concrete	0	0	0
0	1 CIRCULAR	0.29986 CMP	1.51	0.00	5.21
0	1 CIRCULAR	0.03612 RCP	33.76	0.79	61.48
0	1 CIRCULAR	0.02814 RCP	22.18	0.58	39.8
0	1 CIRCULAR	0.02642 RCP	32.64	0.89	59.34
0	1 CIRCULAR	0.00984 RCP	3.47	0.33	6.21
0	1 CIRCULAR	0.04388 RCP	4.63	0.21	8.21
0	1 CIRCULAR	0.0059 RCP	53.3	69.0	82.4
0	1 CIRCULAR	0.02862 RCP	7.6	0.7	13.61
0	1 CIRCULAR	0.00466 RCP	39.3	98.0	70.3
0	1 CIRCULAR	0.02792 RCP	0	0	0
0	1 CIRCULAR	0.02613 RCP	3.07	0.18	5.38
0	1 CIRCULAR	0.23975 CONC	21.41	0.19	37.16
0	1 CIRCULAR	0.01058 CONC	3.84	0.17	6.1
0	1 CIRCULAR	0.01739 CONC	25.24	0.85	39.99
0	1 CIRCULAR	0.15624 CONC	8.83	0.1	15.14
0	1 CIRCULAR	0.0284 CONC	1.24	0.03	2.15
0	1 CIRCULAR	0.09169 RCP	8.94	0.13	15.46
0	1 CIRCULAR	0.01802 RCP	8.08	0.27	22.09
0	1 CIRCULAR	0.03052 RCP	35.25	0.89	40.25
0	1 CIRCULAR	0.00253 RCP	14.67	1.29	14.65
0	1 IRREGULAR	0.0394 Earthen	12.11	0	19.8
0	1 IRREGULAR	0.01044 Earthen	25.01	0	30.98
0	1 IRREGULAR	0.04285 Earthen	3.34	0	5.7
0	1 IRREGULAR	0.06107 Earthen	2.71	0	4.92
0	1 IRREGULAR	0.05729 Earthen	1.21	0	1.97
0	1 IRREGULAR	0.0977 Earthen	6.38	0	10.76
0	1 IRREGULAR	0.00107 Earthen	7.79	0.01	11.32
0	1 IRREGULAR	0.13612 Earthen	7.92	0	11.52
0	1 IRREGULAR	0.02861 Earthen	16.61	0	19.11
0	1 IRREGULAR	0.01535 Earthen	23.43	0	29.14
0	1 IRREGULAR	0.08393 Earthen	16.05	0	19.63
0	1 CIRCULAR	0.01602 CONC	16.6	1.25	19.15
0	1 CIRCULAR	0.04258 CONC	25.01	1.15	30.98
0	1 CIRCULAR	0.00445 CONC	16.05	2.29	19.83
0	1 CIRCULAR	0.05136 RCP	6.38	0.27	10.77
0	1 CIRCULAR	0.08958 RCP	41.94	0.34	60.75
0	1 CIRCULAR	0.04171 RCP	16.34	0.2	27.43
0	1 CIRCULAR	0.7111 RCP	22.14	0.25	35.66
0	1 CIRCULAR	0.02932 RCP	1.3	0.07	2.11
0	1 CIRCULAR	0.0089 RCP	9.0	90.0	96.0

			(cfs)		(cfs)	
0	1 CIRCULAR	0.16319 RCP	0.25	0.01	0.41	
0	1 CIRCULAR	0.01622 RCP	2.42	80:0	3.83	
0	1 CIRCULAR	0.0333 RCP	5.07	0.26	8.76	
0	1 CIRCULAR	0.2531 HDPE	0	0	0	
0	1 CIRCULAR	0.02991 RCP	1.3	0.02	2.39	
0	1 CIRCULAR	0.03346 RCP	28.75	0.38	47.51	
0	1 CIRCULAR	0.15358 RCP	0	0	0	
0	1 CIRCULAR	0.07147 RCP	0	0	0	
5.5	1 CIRCULAR	0.00541 CMP	53.5	2.01	53.36	
5.5	1 CIRCULAR	0.00895 CMP	53.5	1.57	53.36	
0	1 CIRCULAR	0.02458 RCP	0	0	0	
0	1 CIRCULAR	0.05404 RCP	0.54	0.01	96.0	
0	1 CIRCULAR	0.05318 RCP	0.53	0.01	0.95	
0	1 CIRCULAR	0.00612 RCP	2.69	0.15	3.25	
0	1 CIRCULAR	0.0664 RCP	0	0	86.0	
0	1 CIRCULAR	0.02 RCP	0	0	0	
0	1 CIRCULAR	0.0095 RCP	0	0	0	
0	1 CIRCULAR	0.01855 RCP	0	0	0	
0	1 CIRCULAR	0.00971 RCP	4.34	0.19	7.61	
0	1 CIRCULAR	0.08472 SP	15.38	0.43	27.35	
0	1 CIRCULAR	0.00958 RCP	4.33	0.2	7.61	
0	1 CIRCULAR	0.02473 RCP	4.33	0.12	7.6	
0	1 CIRCULAR	0.00383 RCP	7.84	0.56	13.88	
0	1 CIRCULAR	0.03044 RCP	0	0	0	
0	1 CIRCULAR	0.06465 RCP	0	0	0	
0	1 CIRCULAR	0.04035 RCP	0	0	0	
0	1 CIRCULAR	0.04249 RCP	0	0	0	
0	1 CIRCULAR	0.00117 CMP	36.06	4.74	35.21	
0	1 CIRCULAR	0.08941 RCP	10.82	0.02	20.64	
0	1 CIRCULAR	0.0074 RCP	10.82	0.19	20.71	
0	1 CIRCULAR	0.02767 RCP	37.23	0.16	26.88	
0	1 CIRCULAR	0.02594 RCP	38.05	0.16	56.39	
0	1 CIRCULAR	0.03249 RCP	7.39	0.39	22.16	
0	1 CIRCULAR	0.2143 RCP	1.02	0	1.65	
0	1 CIRCULAR	0.00377 CONC	15.43	0.61	27.51	
0	1 CIRCULAR	0.00524 CONC	15.39	0.52	27.43	
0	1 CIRCULAR	0.01283 RCP	344.91	1.17	354.05	
0	1 CIRCULAR	0.00246 RCP	49.6	0.44	50.38	
0	1 CIRCULAR	0.03745 ABS	0.77	0.11	1.26	
0	1 CIRCULAR	0.06325 ABS	0.67	0.07	1.06	
0	1 CIRCULAR	0.07322 RCP	3.47	0.36	4.5	
0	1 CIRCULAR	0.04763 ABS	2.1	0.27	3.44	

			(cfs)		(cfs)
0	1 CIRCULAR	0.14235 RCP	1.79	0.02	3.15
0	1 CIRCULAR	0.02113 ABS	0.92	0.18	1.53
0	1 CIRCULAR	0.08454 CMP	1.83	0.33	3.3
0	1 CIRCULAR	0.02043 SP	0.26	0.03	0.46
0	1 CIRCULAR	0.07526 RCP	0	0	0
8	1 RECT_CLOSED	0.02261 RCB	214.3	0.32	241.33
0	1 CIRCULAR	0.19522 RCP	6:39	0.14	11.52
0	1 CIRCULAR	0.03309 ABS	7.57	1.17	7.57
0	1 CIRCULAR	0.03023 ABS	10.73	0.59	18.74
3	1 PARABOLIC	0.1641 RCP	3.52	90.0	6.18
0	1 CIRCULAR	0.01262 RCP	0.29	0.07	0.59
0	1 CIRCULAR	0.0057 RCP	0.06	0.02	0.14
0	1 CIRCULAR	0.13647 CMP	5.65	0.27	10.31
0	1 CIRCULAR	0.03992 RCP	33.42	0.17	36.03
0	1 CIRCULAR	0.0133 RCP	29.25	90.0	77.78
0	1 CIRCULAR	0.00365 RCP	58.65	0.68	76.04
0	1 CIRCULAR	0.00391 RCP	176.37	0.84	322.21
0	1 CIRCULAR	0.00341 RCP	174.16	0.89	299.5
0	1 CIRCULAR	0.01039 RCP	162.55	0.61	282.45
0	1 CIRCULAR	0.01571 RCP	108.45	0.33	195.21
0	1 CIRCULAR	0.02475 RCP	79.52	0.19	144.57
0	1 CIRCULAR	0.00709 RCP	79.32	98'0	147.69
0	1 CIRCULAR	0.0077 RCP	33.1	0.37	74.48
0	1 CIRCULAR	0.03572 RCP	57.73	0.3	119.93
0	1 CIRCULAR	0.01468 RCP	8.82	0.11	14.34
0	1 CIRCULAR	0.06052 RCP	11.52	0.07	20.89
0	1 CIRCULAR	0.0109 HDPE	0.65	0.1	1.06
0	1 CIRCULAR	0.00612 HDPE	2.86	0.57	4.77
0	1 CIRCULAR	0.0342 HDPE	2.85	0.24	4.77
0	1 CIRCULAR	0.04641 HDPE	1.06	0.08	1.8
0	1 CIRCULAR	0.01048 HDPE	1.85	0.28	3.08
0	1 CIRCULAR	0.03596 RCP	0.17	0	2.95
0	1 CIRCULAR	0.01075 RCP	429.37	86:0	558.01
0	1 CIRCULAR	0.1456 RCP	2.15	0.02	3.62
0	1 CIRCULAR	0.01633 RCP	2.51	0.19	4.26
0	1 CIRCULAR	0.0151 RCP	2.5	0.19	4.25
0	1 CIRCULAR	0.02257 HDPE	2.74	0.17	4.88
0	1 CIRCULAR	0.01518 RCP	33.15	1.19	35.22
0	1 IRREGULAR	0.19961 Earthen	0.13	0	0.21
0	1 CIRCULAR	0.00845 HDPE	3.14	0.53	5.52
0	1 CIRCULAR	0.01821 RCP	3.09	0.35	5.46
0	1 CIRCULAR	0.01598 RCP	14.74	1.11	24.15

			(cfs)		(cfs)
0	1 CIRCULAR	0.01737 RCP	11.16	0.81	20.06
0	1 CIRCULAR	0.02144 RCP	16.44	0.27	29.45
0	1 CIRCULAR	0.06449 RCP	23.15	0.14	39.66
0	1 CIRCULAR	0.01678 RCP	2.18	0.02	6.51
0	1 CIRCULAR	0.16213 PVC	0.91	0.18	1.53
0	1 CIRCULAR	0.02387 RCP	20.29	0.32	32.68
0	1 CIRCULAR	0.0155 RCP	2.56	0.00	2.09
0	1 CIRCULAR	0.01653 RCP	2.56	0.00	2.07
0	1 CIRCULAR	0.07858 RCP	2.55	0.04	2.06
0	1 CIRCULAR	0.08978 PVC	2.21	0.21	3.82
0	1 CIRCULAR	0.08805 RCP	2.23	0.07	4
0	1 CIRCULAR	0.10047 CMP	2.14	0.12	3.73
0	1 CIRCULAR	0.00716 CMP	11.18	1.08	15.89
0	1 CIRCULAR	0.00716 RCP	5.12	0.58	8.57
0	1 CIRCULAR	0.11572 RCP	1.39	0.01	3.35
0	1 CIRCULAR	0.02669 RCP	7.33	0.43	12.74
0	1 CIRCULAR	0.02534 CMP	35.96	1.84	35.95
0	1 CIRCULAR	0.0369 RCP	120.63	0.62	182
0	1 CIRCULAR	0.0315 RCP	59.32	0.5	69.43
0	1 CIRCULAR	0.02168 RCP	99.86	1	114.46
0	1 CIRCULAR	0.02175 RCP	124.68	0.84	163.01
0	1 CIRCULAR	0.03355 RCP	57.88	0.47	65.47
0	1 CIRCULAR	0.02837 RCP	2.37	0.13	4.28
0	1 CIRCULAR	0.05008 CMP	13.97	1.1	14
0	1 CIRCULAR	0.03224 CMP	17.84	1.75	18.54
0	1 CIRCULAR	0.00332 RCP	3.99	0.31	4.25
0	1 CIRCULAR	0.0059 RCP	2.14	0.00	3.91
0	1 CIRCULAR	0.08432 ABS	6.93	0.37	18.1
0	1 CIRCULAR	0.00453 RCP	96:0	90.0	1.77
0	1 CIRCULAR	0.02619 RCP	0.18	0	0.27
0	1 CIRCULAR	0.06693 RCP	1.01	0.04	1.73
3	1 PARABOLIC	0.11591 CONC	0	0	0
3	1 PARABOLIC	0.00757 CONC	1.6	0.12	3
0	1 CIRCULAR	0.00305 RCP	0.2	0.1	0.44
3	1 PARABOLIC	0.01636 CONC	0	0	0
0	1 CIRCULAR	0.17878 CMP	0.85	0.1	1.5
16	1 RECT_CLOSED	0.00788 RCB	277.5	0.22	527.52
0	1 CIRCULAR	0.06169 RCP	0.03	0	0.05
3	1 PARABOLIC	0.04794 CONC	0	0	0
3	1 PARABOLIC	0.09823 CONC	0	0	0
3	1 PARABOLIC	0.07036 CONC	2.03	0.02	3.6
0	1 CIRCULAR	0.01774 CMP	5.03	0.66	8.11

			(cfs)		(cfs)	
0	1 CIRCULAR	0.02147 CMP	28.99	0.55	50.95	
0	1 CIRCULAR	0.05043 RCP	0.9	0.04	1.43	
0	1 CIRCULAR	0.01278 RCP	1.43	0.12	17.83	
0	1 CIRCULAR	0.00966 RCP	2.16	0.21	3.64	
3	1 PARABOLIC	0.17585 Concrete	2.83	0.07	4.77	
0	1 CIRCULAR	0.02919 CMP	0.24	0.04	0.39	
0	1 CIRCULAR	0.01504 HDPE	0.26	0.03	0.43	
0	1 CIRCULAR	0.04105 CMP	0.26	0.04	0.43	
0	1 CIRCULAR	0.06328 CMP	1.86	0.13	3.34	
0	1 CIRCULAR	0.01859 RCP	9.04	0.63	15.26	
0	1 CIRCULAR	0.06189 CMP	6.87	0.49	12.13	
0	1 CIRCULAR	0.47947 CMP	3.18	0.04	5.8	
0	1 CIRCULAR	0.01083 RCP	11.78	0.71	20.7	
0	1 CIRCULAR	0.01081 CMP	20.82	6.0	36.56	
0	1 CIRCULAR	0.02205 HDPE	3.46	0.65	4.75	
0	1 CIRCULAR	0.15237 CMP	5.46	0.25	8.53	
0	1 CIRCULAR	0.00506 CMP	6.31	1.56	9.76	
0	1 CIRCULAR	0.01534 CMP	3.84	0.54	6.79	
0	1 CIRCULAR	0.00263 RCP	89.08	0.37	219.18	
0	1 CIRCULAR	0.01929 RCP	4.35	0.3	7.63	
0	1 CIRCULAR	0.00704 CMP	3.83	8.0	6.58	
0	1 CIRCULAR	0.0524 HDPE	4.01	80:0	98.9	
0	1 CIRCULAR	0.27655 CMP	0	0	0	
0	1 IRREGULAR	0.01478 EAR	9.0	0.2	96.0	
0	1 CIRCULAR	0.19015 CMP	3.45	0.14	2.69	
0	1 CIRCULAR	0.09578 CMP	18.93	0.28	29	
0	1 CIRCULAR	0.03988 RCP	1.33	90:0	2.31	
4	1 RECT_OPEN	0.02479 Concrete	0	0	0	
0	1 CIRCULAR	0.00564 RCP	79.5	1.59	78.92	
8	1 RECT_OPEN	0.00961 Concrete	5.17	0.1	8.53	
2	1 RECT_OPEN	0.02826 Concrete	0.17	0	0.26	
0	1 CIRCULAR	0.0106 CMP	5.23	0.89	7.91	
0	1 CIRCULAR	0.04587 RCP	6.31	0.21	9.73	
0	1 CIRCULAR	0.00784 RCP	7.9	0.64	12.69	
0	1 CIRCULAR	0.87276 PVC	1.17	0.22	1.83	
∞	1 RECT_OPEN	0.00915 EAR	1.79	0.02	3.16	
0	1 CIRCULAR	0.00576 HDPE	97.27	68:0	182.34	
0	1 CIRCULAR	0.04554 CMP	0.94	80.0	1.56	
0	1 CIRCULAR	0.01812 HDPE	97.83	0.51	182.97	
0	1 CIRCULAR	0.00379 RCP	21.16	1.52	22.45	
3	1 PARABOLIC	0.02196 Earthen	1.64	0.34	2.83	
0	1 CIRCULAR	0.00517 CMP	1.3	0.15	2.12	

			(cfs)		(cfs)	
3	1 PARABOLIC	0.04 Concrete	0.48	0.02	0.61	
0	1 CIRCULAR	0.1509 CONC	5.11	90.0	8.05	
0	1 CIRCULAR	0.01522 RCP	87.5	0.27	154.09	
0	1 CIRCULAR	0.14643 CMP	2.81	0.13	4.47	
0	1 CIRCULAR	0.00976 CMP	1.42	0.25	2.46	
0	1 CIRCULAR	0.17017 CMP	0.51	0.02	0.88	
0	1 CIRCULAR	0.04798 HDPE	1.87	0.04	3.43	
0	1 CIRCULAR	0.46873 HDPE	2.39	0.02	4.33	
0	1 CIRCULAR	0.03969 HDPE	7.52	98:0	11.99	
0	1 CIRCULAR	0.00333 CMP	16.5	0.37	26.99	
0	1 CIRCULAR	0.10334 Earthen	24.01	0.02	38.95	
20	1 RECT_OPEN	0.10318 Earthen	24	0	38.95	
0	1 CIRCULAR	0.04903 HDPE	0.86	0.04	1.38	
0	1 CIRCULAR	0.03154 HDPE	0.89	0.02	1.43	
0	1 CIRCULAR	0.03585 HDPE	6.74	0.34	10.76	
0	1 CIRCULAR	0.02862 HDPE	7.55	0.42	12.04	
0	1 CIRCULAR	0.02449 HDPE	0.51	0.03	0.79	
0	1 CIRCULAR	0.01638 HDPE	0.41	0.03	0.63	
0	1 CIRCULAR	0.02458 ABS	14.1	0.4	25.27	
0	1 CIRCULAR	0.01862 HDPE	4.94	0.56	9.1	
0	1 CIRCULAR	0.01962 HDPE	1.08	0.07	1.71	
0	1 CIRCULAR	0.01614 HDPE	0.19	0.01	0.29	
0	1 CIRCULAR	0.03746 HDPE	0.54	0.03	0.82	
0	1 CIRCULAR	0.13082 HDPE	4.52	90:0	69.7	
3	1 PARABOLIC	0.0177 CONC	0.83	0.02	1.91	
0	1 CIRCULAR	0.01652 HDPE	1.57	0.12	2.56	
0	1 CIRCULAR	0.03322 HDPE	2.05	0.11	3.3	
0	1 CIRCULAR	0.01452 HDPE	1.03	0.08	1.59	
0	1 CIRCULAR	0.02852 HDPE	1.28	0.07	2	
0	1 CIRCULAR	0.04167 HDPE	4.25	0.5	6.74	
0	1 CIRCULAR	0.08783 CMP	99.0	0.12	1.05	
0	1 CIRCULAR	0.00621 HDPE	2.45	0.3	3.89	
0	1 CIRCULAR	0.02495 HDPE	3.52	0.21	29.65	
0	1 CIRCULAR	0.06935 HDPE	1.18	0.04	1.84	
0	1 CIRCULAR	0.10685 HDPE	4.79	90:0	7.61	
0	1 CIRCULAR	0.0196 RCP	7.02	0.48	12.36	
0	1 CIRCULAR	0.00366 RCP	8.89	1.4	15.35	
e	1 PARABOLIC	0.10962 Concrete	0	0	0	
3	1 PARABOLIC	0.05945 Concrete	0	0	0	
3	1 PARABOLIC	0.02626 Concrete	1.35	0.08	2.7	
3	1 PARABOLIC	0.14246 Concrete	1.97	0.02	3.52	
3	1 PARABOLIC	0.08587 Concrete	1.37	0.02	2.6	

			(cfs)		(cfs)	
0	1 CIRCULAR	0.06224 RCP	1.15	0.04	2.11	
0	1 CIRCULAR	0.01105 RCP	28.35	0.19	52.51	
0	1 CIRCULAR	0.07414 RCP	0.64	0.05	1.14	
0	1 CIRCULAR	0.03938 RCP	27.58	0.1	51.13	
0	1 CIRCULAR	0.02111 CMP	16.86	0.52	28.34	
0	1 CIRCULAR	0.05984 CMP	24.19	0.45	41.18	
0	1 CIRCULAR	0.01887 CMP	5.24	0.67	9.5	
0	1 CIRCULAR	0.04587 RCB	20.31	0.42	36.88	
0	1 CIRCULAR	0.02502 CMP	12.5	1.39	18.7	
0	1 CIRCULAR	0.02587 CMP	11.15	1.22	16.21	
0	1 CIRCULAR	0.05871 CMP	37.3	0.43	66.52	
0	1 CIRCULAR	0.02778 CMP	2.8	0.3	8.16	
0	1 CIRCULAR	0.00906 HDPE	4.39	2.13	4.47	
0	1 CIRCULAR	0.12358 ABS	4.19	0.11	8.48	
0	1 CIRCULAR	0.0162 RCP	65.94	0.78	117.55	
0	1 CIRCULAR	0.07062 CMP	0.76	0.02	1.32	
0	1 CIRCULAR	0.01712 RCP	72.36	0.38	128.25	
0	1 CIRCULAR	0.03356 RCP	56.16	0.21	104.15	
0	1 CIRCULAR	0.00678 RCP	56.23	0.48	104.3	
0	1 CIRCULAR	0.0181 RCP	54.24	0.28	99.92	
0	1 CIRCULAR	0.05178 RCP	3.73	0.46	69.9	
0	1 CIRCULAR	0.03747 RCP	25.2	0.2	44.52	
0	1 CIRCULAR	0.0509 CMP	5.4	0.42	10.37	
0	1 CIRCULAR	0.09784 CMP	10.57	0.00	19.17	
0	1 CIRCULAR	0.03933 RCP	25.18	0.03	44.73	
0	1 CIRCULAR	0.01682 ABS	2.78	0.2	4.75	
0	1 CIRCULAR	0.2452 ABS	2.77	0.02	4.74	
0	1 CIRCULAR	0.02226 ABS	5.64	0.36	9.75	
0	1 CIRCULAR	0.06198 ABS	5.63	0.22	9.73	
0	1 CIRCULAR	0.00607 ABS	4.86	0.59	9.31	
0	1 CIRCULAR	0.01527 RCP	25.28	0.02	78.06	
0	1 CIRCULAR	0.06046 RCP	19.37	0.12	34.35	
0	1 CIRCULAR	0.0082 RCP	19.39	0.32	34.32	
0	1 CIRCULAR	0.10425 RCP	11.44	0.02	20.74	
0	1 CIRCULAR	0.00806 CMP	6.55	1.28	9.47	
33	1 PARABOLIC	0.02293 Concrete	0.11	0.01	0.17	
3	1 PARABOLIC	0.07433 Concrete	0.19	0.01	0.31	
0	1 CIRCULAR	0.01033 CMP	10.59	0.85	15.9	
3	1 PARABOLIC	0.07132 Concrete	0.16	0.01	0.24	
0	1 CIRCULAR	0.02264 RCP	1.34	0.00	2.45	
0	1 CIRCULAR	0.00901 RCP	9.61	0.45	17.25	
0	1 CIRCULAR	0.03829 RCP	17.2	0.39	31.14	

			(cfs)		(cfs)	
0	1 CIRCULAR	0.0967 RCP	1.36	0.04	2.55	
0	1 CIRCULAR	0.04935 ABS	2.18	0.00	3.98	
0	1 CIRCULAR	0.01085 CMP	19.28	0.51	22.16	
3	1 PARABOLIC	0.10272 Concrete	0.7	0.00	1.21	
0	1 CIRCULAR	0.0152 RCP	0.84	90.0	1.53	
3	1 PARABOLIC	0.31425 Concrete	0.08	0	0.12	
3	1 PARABOLIC	0.16378 Concrete	0.53	0.01	1.06	
3	1 PARABOLIC	0.04039 Concrete	0.23	0.01	0.45	
0	1 CIRCULAR	0.0219 CMP	4.46	0.53	7.87	
0	1 CIRCULAR	0.01514 CMP	5.57	0.8	8.06	
0	1 CIRCULAR	0.01978 CMP	4.31	0.88	5.24	
0	1 CIRCULAR	0.00456 HDPE	4.05	0.57	6.91	
0	1 CIRCULAR	0.03154 CONC	26.6	0.22	44.87	
0	1 CIRCULAR	0.10703 RCP	2.92	0.08	6.28	
0	1 CIRCULAR	0.00646 RCP	37.67	0.33	22.69	
0	1 CIRCULAR	0.00902 RCP	50.3	0.37	95.66	
0	1 CIRCULAR	0.0122 RCP	51.22	0.32	94.15	
0	1 CIRCULAR	0.00327 RCP	18.78	0.23	32.39	
0	1 CIRCULAR	0.0409 ABS	3.16	0.02	6.13	
0	1 CIRCULAR	0.02557 ABS	1.34	0.04	2.32	
0	1 CIRCULAR	0.01378 ABS	1.3	0.02	2.26	
0	1 CIRCULAR	0.15746 CMP	1.36	90.0	2.37	
0	1 CIRCULAR	0.06161 CMP	24.1	0.18	32.96	
3	1 PARABOLIC	0.01145 CONC	2.34	0.15	3.35	
0	1 CIRCULAR	0.00884 CMP	2.31	0.43	4.13	
29	1 RECT_CLOSED	0.00802 RCB	2.54	0.21	4.58	
0	1 CIRCULAR	0.00666 CMP	10.89	2.34	12.25	
1.5	1 PARABOLIC	0.03101 CONC	10.99	1.04	12.15	
0	1 CIRCULAR	0.07756 RCP	7.03	0.24	7.39	
0	1 CIRCULAR	0.05399 SP	16.85	0.5	30.06	
3	1 PARABOLIC	0.02734 CONC	0.55	0.00	0.99	
0	1 CIRCULAR	0.13726 HDPE	0.7	1.02	0.67	
0	1 CIRCULAR	0.00492 RCP	15.99	1.01	17.46	
0	1 CIRCULAR	0.01641 RCP	28.47	0.33	43.75	
0	1 CIRCULAR	0.00819 RCP	68.69	1.16	79.64	
0	1 CIRCULAR	0.03748 RCP	67.87	0.53	79.49	
0	1 CIRCULAR	0.00833 RCP	75.13	0.82	79.51	
0	1 CIRCULAR	0.00403 RCP	19	1.32	20.81	
0	1 CIRCULAR	0.02132 RCP	4.78	0.02	8.57	
0	1 CIRCULAR	0.05786 RCP	18.07	0.11	32.36	
0	1 CIRCULAR	0.09632 RCP	8.01	0.25	13.75	
0	1 CIRCULAR	0.03919 RCP	17.99	0.14	32.23	

			(cfs)		(cfs)
0	1 CIRCULAR	0.04267 RCP	7	0.32	6.37
0	1 CIRCULAR	0.36144 RCP	2.4	0.04	3.72
0	1 IRREGULAR	0.01301 CONC	305.17	0.11	535.07
0	1 CIRCULAR	0.02067 RCP	7.37	0.49	10.71
0	1 CIRCULAR	0.01369 RCP	10.78	0.88	15.98
0	1 CIRCULAR	0.00701 CMP	10.63	1.04	15.22
0	1 CIRCULAR	0.0427 HDPE	2.14	0.1	2.9
0	1 CIRCULAR	0.02612 CMP	8.83	96.0	8.95
0	1 IRREGULAR	0.01988 EAR	7.24	0	11.9
3	1 PARABOLIC	0.02879 EAR	0	0	0
3	1 PARABOLIC	0.15859 Concrete	0.12	0	0.22
0	1 CIRCULAR	0.00199 RCP	36.41	0.81	53.07
2	1 HORIZ_ELLIPSE	0.00131 CMP	144.75	2.78	153.3
2	1 HORIZ_ELLIPSE	0.00422 CMP	143.58	3.31	151.95
2	1 HORIZ_ELLIPSE	0.13693 CMP	143.73	0.27	152.12
2	1 CIRCULAR	0.05677 CMP	92.93	1.08	92.05
0	1 CIRCULAR	0.00352 CMP	45.28	2.11	44.36
0	1 CIRCULAR	0.01661 CMP	41.04	0.88	40.85
0	1 CIRCULAR	0.02256 CMP	14.34	0.78	16.04
0	1 CIRCULAR	0.04862 PVC	6.38	0.13	11.31
0	1 CIRCULAR	0.00483 CMP	0.63	0.16	1.06
0	1 CIRCULAR	0.07683 RCP	3.12	0.11	5.2
0	1 CIRCULAR	0.00776 CMP	88.43	1.29	86.38
0	1 CIRCULAR	0.3513 RCP	3.41	0.02	29.67
0	1 CIRCULAR	0.01352 RCP	40.73	1.55	43.77
2	1 RECT_CLOSED	0.01171 CMP	79.27	0.82	79.24
9	1 RECT_CLOSED	0.02261 RCB	79.26	0.47	79.24
0	1 CIRCULAR	0.01132 PVC	1.54	2.59	1.51
0	1 CIRCULAR	0.02844 RCP	56.59	0.5	83.12
0	1 CIRCULAR	0.01439 CMP	0.04	0.01	3.31
0	1 CIRCULAR	0.04342 CMP	11.1	0.94	11.59
0	1 CIRCULAR	0.01865 RCP	45.27	0.63	55.51
0	1 CIRCULAR	0.10633 CMP	0	0	0
0	1 CIRCULAR	0.00575 RCP	60.82	0.56	80.17
0	1 CIRCULAR	0.01936 CMP	4.69	0.59	7.89
0	1 CIRCULAR	0.06851 CMP	6.4	0.43	10.68
0	1 CIRCULAR	0.03324 ABS	0	0	0
0	1 CIRCULAR	0.00743 RCP	14.67	0.75	26.9
0	1 CIRCULAR	-0.02002 RCP	0.17	0.01	2.66
0	1 CIRCULAR	0 SP	9.02	27.24	9.14
0	1 CIRCULAR	0.02058 RCP	7.9	0.13	14.48
0	1 CIRCULAR	0.00752 SP	10.51	1.41	10.97

			(cfs)		(cfs)
0	1 CIRCULAR	0.0127 RCP	11.49	0.45	20.21
0	1 CIRCULAR	0.03828 RCP	96.6	0.23	17.98
0	1 CIRCULAR	0.0025 RCP	0.47	0.02	96.0
0	1 CIRCULAR	0.00103 CMP	8.92	0.51	10.12
0	1 CIRCULAR	0.03355 SP	8.91	1.39	10.09
0	1 CIRCULAR	0.01792 RCP	0	0	0.3
0	1 CIRCULAR	0.03195 RCP	17.43	0.93	17.65
0	1 CIRCULAR	0.03125 RCP	0	0	0
0	1 CIRCULAR	0.00867 RCP	17.52	0.46	16.99
0	1 CIRCULAR	0.11215 RCP	3.86	0.03	6.23
0	1 CIRCULAR	0.03885 CMP	7.75	69:0	77.7
0	1 CIRCULAR	0.00731 CMP	11.67	1.11	11.45
0	1 CIRCULAR	0.00581 RCP	28.55	1.66	29.83
0	1 CIRCULAR	0.01189 RCP	4.12	0.36	7.42
0	1 CIRCULAR	0.01529 RCP	5.71	1.3	29.67
0	1 CIRCULAR	0.02304 RCP	0.74	0.02	1.39
0	1 CIRCULAR	0.03061 PVC	0.2	0.03	0.45
0	1 CIRCULAR	0.01932 RCP	4.02	0.28	8.78
0	1 CIRCULAR	0.01945 PVC	8.89	1.79	10.14
0	1 CIRCULAR	0.00379 HDPE	0.87	0.13	1.56
0	1 CIRCULAR	0.00328 RCP	9.65	1.6	11.56
0	1 CIRCULAR	0.0285 RCB	16.97	0.44	29.82
0	1 CIRCULAR	0.02354 RCP	15.31	0.44	26
0	1 CIRCULAR	0.03063 RCP	17.21	0.43	29.43
0	1 CIRCULAR	0.01699 CMP	17	0.59	29.86
0	1 CIRCULAR	0.01088 ABS	21.8	1.99	22.04
0	1 CIRCULAR	0.01269 RCP	96.76	9.0	124.05
0	1 CIRCULAR	0.00444 CMP	2.04	0.54	3.55
0	1 CIRCULAR	0.05891 ABS	4.21	0.27	7.33
0	1 CIRCULAR	0.0115 ABS	5.05	0.73	96.8
0	1 CIRCULAR	0.00803 RCP	130.3	0.34	221.71
0	1 CIRCULAR	0.05139 RCP	1.51	90.0	2.9
0	1 CIRCULAR	0.05264 RCP	3.14	0.03	7.68
0	1 CIRCULAR	0.04159 RCP	2.81	0	4
0	1 CIRCULAR	0.05905 CONC	13.99	0.14	25.39
0	1 CIRCULAR	0.00317 CONC	14.54	0.63	27.79
0	1 CIRCULAR	0.00316 RCP	133.07	0.56	241.23
0	1 CIRCULAR	0.13892 RCP	8	0.2	14.2
0	1 CIRCULAR	0.00623 RCP	134.21	0.4	228.89
0	1 CIRCULAR	0.01699 RCP	138.99	0.54	235.29
0	1 CIRCULAR	0.00709 RCB	138.89	0.39	235.3
0	1 CIRCULAR	0.06048 CMP	15.34	0.28	31.92

			(cfs)		(cfs)	
3	1 PARABOLIC	0.02251 ASPHALT	5.6	0.3	9.3	
0	1 CIRCULAR	0.02474 CMP	10.6	0.55	16.93	
0	1 CIRCULAR	0.06675 ABS	4.08	0.44	7.26	
0	1 CIRCULAR	0.01744 HDPE	14.38	0.48	24.16	
0	1 CIRCULAR	0.01806 HDPE	1.41	0.1	2.52	
0	1 CIRCULAR	0.03489 HDPE	1.4	0.07	2.5	
0	1 CIRCULAR	0.00705 HDPE	9.18	0.48	15.57	
0	1 CIRCULAR	0.1717 HDPE	1.22	0.08	2.12	
0	1 CIRCULAR	0.02095 HDPE	6.02	1.17	6.07	
0	1 CIRCULAR	0.09901 CMP	10.54	0.39	18.44	
0	1 CIRCULAR	0.01308 RCP	5.75	0.48	11.13	
0	1 CIRCULAR	0.05481 ABS	2.41	0.29	4.78	
0	1 CIRCULAR	0.01369 RCP	3.22	0.26	2.66	
0	1 CIRCULAR	0.01785 CMP	3.2	0.42	5.2	
0	1 CIRCULAR	0.02373 CMP	9.56	0.51	15.07	
0	1 CIRCULAR	0.02559 CMP	2.52	0.28	4.4	
0	1 CIRCULAR	0.02648 CMP	20.41	0.56	32.34	
0	1 CIRCULAR	0.03535 CMP	20.35	0.49	32.27	
0	1 CIRCULAR	0.00714 RCP	20.3	0.59	32.17	
0	1 CIRCULAR	0.00711 RCP	58.41	1.69	85.62	
0	1 CIRCULAR	0.08274 RCP	63.3	0.33	104.1	
0	1 CIRCULAR	0.00819 CMP	1.48	0.29	2.61	
0	1 CIRCULAR	0.00287 CMP	2.13	0.7	3.78	
3	1 RECT_CLOSED	-0.004 RCB	2.7	0.24	4.51	
0	1 CIRCULAR	0.03087 HDPE	3.72	0.2	6.14	
0	1 CIRCULAR	0.0312 CMP	90.0	0	0.00	
0	1 CIRCULAR	0.03948 CMP	11.4	0.11	20.36	
0	1 CIRCULAR	0.00689 CMP	29.56	0.99	29.63	
0	1 CIRCULAR	0.03258 RCP	3.39	0.18	92.9	
3	1 PARABOLIC	0.07889 Concrete	0.27	0.01	0.44	
3	1 PARABOLIC	0.05771 Concrete	0.05	0	0.1	
0	1 CIRCULAR	0.00581 ABS	0.58	0.21	98.0	
0	1 CIRCULAR	0.00402 ABS	3.28	1.45	4.92	
0	1 CIRCULAR	0.04015 ABS	5.02	0.7	4.75	
0	1 CIRCULAR	0.00851 RCP	7.64	0.79	9.25	
0	1 CIRCULAR	0.0111 HDPE	6.62	1.76	6.73	
0	1 CIRCULAR	0.01417 RCP	2.35	0.19	3.83	
0	1 CIRCULAR	0.05023 CMP	7.37	0.58	12.87	
0	1 CIRCULAR	0.01876 CMP	10.28	1.32	15.68	
0	1 CIRCULAR	0.01477 VCP	1.39	1.01	1.5	
4	1 RECT_OPEN	0.00572 Earthen	1.89	0.13	4.18	
0	1 CIRCULAR	0.01031 RCP	3.5	0.97	4.45	

			(cfs)		(cfs)
0	1 CIRCULAR	0.01982 RCP	33.82	0.17	51.53
0	1 CIRCULAR	0.10128 CONC	4.13	90:0	6.81
0	1 CIRCULAR	0.00692 RCP	15.28	0.28	27.54
0	1 CIRCULAR	0.0085 RCP	15.27	0.25	27.45
0	1 CIRCULAR	0.05279 RCP	1.59	0.07	2.84
0	1 CIRCULAR	0.05562 RCP	17.35	0.11	31.42
0	1 CIRCULAR	0.00673 RCP	21.26	0.63	39.23
0	1 CIRCULAR	0.03092 RCP	23.44	0.32	43.24
0	1 CIRCULAR	0.02696 RCP	23.36	0.14	41.44
0	1 CIRCULAR	0.08306 RCP	28.68	0.24	52.95
0	1 CIRCULAR	0.02342 RCP	33.05	0.53	60.31
0	1 CIRCULAR	0.16796 CMP	0.12	0.01	0.18
0	1 CIRCULAR	0.01787 RCP	9.33	99.0	16.34
0	1 CIRCULAR	0.3433 RCP	0.28	0.01	0.45
0	1 CIRCULAR	0.00529 RCP	116.94	0.38	138.67
0	2 CIRCULAR	0.02311 RCP	130.17	1.04	130.21
0	1 CIRCULAR	0.01451 CMP	14.32	2.09	14.31
0	1 CIRCULAR	0.00414 CMP	16.94	4.62	17.02
0	1 CIRCULAR	0.01415 RCP	53.23	1.09	81.36
0	1 CIRCULAR	0.0385 RCP	29.87	0.18	54.51
0	1 CIRCULAR	0.00408 RCP	115.61	0.43	311.67
3	1 PARABOLIC	0.09321 EAR	0	0	0
0	1 CIRCULAR	0.01089 RCP	54.18	1.27	55.97
0	1 CIRCULAR	0.01124 CMP	2.99	0.5	4.33
0	1 CIRCULAR	0.0107 CMP	8.72	69.0	10.35
0	1 CIRCULAR	0.07895 CMP	2.53	0.16	4.5
0	1 CIRCULAR	0.01978 RCP	37.4	0.19	59.39
0	1 CIRCULAR	0.01978 RCP	37.49	0.19	58.9
0	1 CIRCULAR	0.04044 HDPE	3.44	0.48	4.25
0	1 IRREGULAR	0.01187 Earthen	537.3	0.08	884
0	1 CIRCULAR	0.01978 RCP	41.89	0.21	67.42
0	1 CIRCULAR	0.01947 RCP	154.07	0.56	261.3
0	1 CIRCULAR	0.02089 RCP	153.96	0.54	261.18
0	1 CIRCULAR	0.03843 RCP	1.18	0.03	2.03
0	1 CIRCULAR	0.00764 RCP	157.42	0.43	267.78
0	1 CIRCULAR	0.04813 HDPE	7.19	0.31	15.25
0	1 CIRCULAR	0.01396 HDPE	10.63	0.4	25.84
0	1 IRREGULAR	0.01417 Earthen	551.4	0.37	911.75
0	1 IRREGULAR	0.01338 Earthen	537.86	0.37	896.82
0	1 IRREGULAR	-0.11433 Earthen	459.15	0.11	690.05
0	1 CIRCULAR	0.02166 CONC	3.29	0.63	5.16
0	1 CIRCULAR	0.19098 HDPE	13.71	0.14	13.96

			(cfs)		(cfs)
0	1 CIRCULAR	0.01976 RCP	0.99	0.07	1.86
0	1 IRREGULAR	0.037 Earthen	542.83	0.05	99.606
0	1 IRREGULAR	0.01391 Earthen	543.45	0.04	917.34
0	1 CIRCULAR	0.08056 CONC	3.92	0.03	12.38
0	1 CIRCULAR	0.00486 RCP	30.89	1.08	47.21
0	1 CIRCULAR	0.04831 RCP	45.39	0.14	68.32
0	1 CIRCULAR	0.00818 RCP	29.64	0.23	44.16
0	1 CIRCULAR	0.00854 CMP	209.63	1.84	235.02
0	1 CIRCULAR	0.11696 CMP	24.36	1.25	24.47
0	1 CIRCULAR	0.29333 CMP	4.17	90.0	15.71
0	1 CIRCULAR	0.00849 RCP	175.39	0.36	320.5
0	1 CIRCULAR	0.01041 CMP	61.41	0.26	124.82
0	1 CIRCULAR	0.01564 CMP	61.18	0.21	124.47
0	1 CIRCULAR	0.00271 RCP	66.77	0.24	132.98
6	1 RECT_CLOSED	0.01748 RCB	133.53	0.3	244.76
0	1 CIRCULAR	0.00716 RCP	65.37	0.15	133.67
0	1 CIRCULAR	0.05349 CMP	0.42	0.01	0.56
0	1 CIRCULAR	0.16129 CMP	1.05	0.02	1.59
0	1 CIRCULAR	0.0284 RCP	175.48	0.5	320.25
0	1 CIRCULAR	0.03687 CMP	190.43	0.7	218.69
0	1 CIRCULAR	0.00343 RCP	31.98	0.82	33.2
0	1 CIRCULAR	0.00206 RCP	22.4	0.49	29.44
0	1 CIRCULAR	0.00338 RCP	18.67	0.48	20.78
0	1 CIRCULAR	0.013 HDPE	4.53	0.18	7.7
0	1 CIRCULAR	0.01304 HDPE	4.53	0.18	7.7
0	1 CIRCULAR	0.04507 HDPE	4.51	0.00	7.68
0	1 CIRCULAR	0.01265 RCP	240.96	0.41	454.16
0	1 CIRCULAR	-0.00651 RCP	35.47	1.94	29
0	1 CIRCULAR	0.0481 RCP	7.92	0.05	10.01
0	1 CIRCULAR	0.00868 CMP	1.31	0.25	1.27
0	1 CIRCULAR	-0.0007 RCP	22.18	0.84	28.87
0	1 CIRCULAR	0.01482 RCP	63.35	0.36	106.49
0	1 CIRCULAR	0.31215 RCP	63.34	0.08	106.49
0	1 CIRCULAR	0.03407 HDPE	3.46	0.08	2.66
0	1 CIRCULAR	0.05257 RCP	29.11	0.31	49.03
0	1 IRREGULAR	0.02049 Concrete	338.29	0.13	411.97
0	1 IRREGULAR	0.01427 Concrete	331.66	0.15	401.61
0	1 IRREGULAR	0.00495 Concrete	337.28	0.26	402.82
0	1 IRREGULAR	0.02722 Concrete	332.05	0.11	400.84
0	1 IRREGULAR	0.05109 Concrete	121.4	0.03	177.81
0	1 IRREGULAR	0.01883 Concrete	331.19	0.03	422.15
0	1 CIRCULAR	0.07351 RCP	38.66	0.21	65.03

			(cfs)		(cfs)	
0	1 CIRCULAR	0.01495 ABS	0.78	0.18	1.27	
0	1 CIRCULAR	0.00877 CMP	157.31	1.37	156.07	
0	1 CIRCULAR	0.01026 CMP	153.27	1.23	154.6	
0	1 CIRCULAR	0.03387 CMP	112.34	0.43	111.85	
0	1 CIRCULAR	0.0095 CMP	11.2	0.94	14.06	
0	1 CIRCULAR	0.01692 RCP	6.37	0.47	11.15	
0	1 CIRCULAR	0.05965 ABS	1.41	0.16	1.52	
0	1 CIRCULAR	0.00988 RCP	20.9	0.93	20.8	
0	1 CIRCULAR	0.04842 CMP	4.81	0.38	2.06	
8	1 RECT_OPEN	0.02254 RCB	229.01	0.39	437.81	
0	1 CIRCULAR	0.07663 CMP	12.7	0.81	12.53	
1.6	1 CIRCULAR	0.00429 CMP	34.05	1.44	33.66	
0	1 CIRCULAR	0.03133 CMP	18.79	0.87	18.68	
0	1 CIRCULAR	0.02019 CMP	7.95	0.98	8.54	
0	1 CIRCULAR	0.03182 CMP	11.98	0.3	21.77	
0	1 CIRCULAR	0.02222 CMP	15.32	0.46	27.41	
0	1 CIRCULAR	0.02762 CMP	11.97	1.27	11.68	
0	1 CIRCULAR	0.02196 CMP	9:98	1.18	12.76	
0	1 CIRCULAR	0.01657 CMP	4.51	0.62	7.59	
0	1 CIRCULAR	0.01262 HDPE	10.46	2.61	9.84	
0	1 CIRCULAR	0.08025 CMP	3.38	0.21	6.17	
0	1 CIRCULAR	0.02419 RCP	67.86	0.65	90.92	
0	1 CIRCULAR	0.05238 RCP	68.89	0.45	73.73	
0	1 CIRCULAR	0.00207 CMP	61.47	1.74	62.72	
0	1 CIRCULAR	0.10592 RCP	0.55	0.03	96.0	
0	1 CIRCULAR	0.01039 CMP	61.37	0.77	62.63	
0	1 CIRCULAR	0.00174 RCP	59.97	3.51	78.06	
0	1 CIRCULAR	0.02646 RCP	59.95	6.0	78.09	
0	1 CIRCULAR	0.03132 RCP	67.51	0.57	90.52	
0	1 CIRCULAR	0.04937 RCP	8.13	0.05	13.49	
0	1 CIRCULAR	0.07018 HDPE	0.96	0.1	1.52	
0	1 CIRCULAR	0.00966 CMP	152.19	1.26	153.67	
0	1 CIRCULAR	0.03732 HDPE	0.63	0.00	1.01	
0	1 CIRCULAR	0.00527 RCP	9.46	0.2	15.92	
0	1 CIRCULAR	0.01672 RCP	56.51	0.17	90.13	
0	1 CIRCULAR	0.55138 RCP	0.79	0	1.31	
0	1 CIRCULAR	0.02255 RCP	54.37	0.14	83.98	
0	1 CIRCULAR	0.05594 RCP	3.9	0.04	6.48	
0	1 CIRCULAR	0.07201 HDPE	3.66	90.0	6.11	
0	1 CIRCULAR	0.00685 RCP	6.4	0.34	20.98	
3	1 PARABOLIC	0.02976 Concrete	0	0	0	
0	1 CIRCULAR	0.02432 CMP	15.27	0.34	29.44	

			cfs)		(cfs)	
0	1 CIRCULAR	0.04998 PVC	0.24	0.58	0.42	
3	1 PARABOLIC	0.10043 Concrete	0	0	0	
3	1 PARABOLIC	0.0915 Concrete	0	0	0	
0	1 CIRCULAR	0.20008 RCP	2.66	0.01	4.41	
0	1 CIRCULAR	0.07002 CONC	23.11	0.21	31.21	
3	1 PARABOLIC	0.02878 Concrete	15.86	2.6	19.96	
0	1 CIRCULAR	0.04492 CONC	21.64	0.25	28.73	
0	1 CIRCULAR	0.02864 RCP	16.38	0.24	29.35	
0	1 CIRCULAR	0.01469 HDPE	4.01	0.32	6.87	
0	1 CIRCULAR	0.02426 Not modeled	24.29	0.7	38.22	
3	1 PARABOLIC	0.04219 Other	0.29	0.04	0.52	
0	1 CIRCULAR	0.10623 RCP	4.3	0.13	7.73	
0	1 CIRCULAR	0.04233 CMP	24.09	0.53	37.77	
0	1 CIRCULAR	0.08841 RCP	8.42	0.27	14.86	
0	1 CIRCULAR	0.08949 RCP	10.95	0.35	19.23	
0	1 CIRCULAR	0.07287 RCP	7.19	0.25	12.66	
0	1 CIRCULAR	0.01118 RCP	16.56	1.49	23.84	
0	1 CIRCULAR	0.00616 RCP	16.13	1.96	20.12	
0	1 CIRCULAR	0.01387 RCP	12.7	1.03	12.16	
0	1 CIRCULAR	0.01682 RCP	15.91	1.17	16.73	
0	1 CIRCULAR	0.10761 RCP	18.99	0.55	31.13	
0	1 CIRCULAR	0.01317 RCP	3.24	0.27	8.2	
0	1 CIRCULAR	0.07204 CMP	15.78	0.26	23.62	
0	1 CIRCULAR	0.04634 CMP	2.46	0.2	4.39	
3	1 PARABOLIC	0.19867 CONC	0.21	0	0.34	
0	1 CIRCULAR	0.03611 CMP	53.78	1.27	63.88	
3	1 PARABOLIC	0.01341 CONC	12.51	0.72	2.31	
0	1 IRREGULAR	0.04951 Other	1.05	0.01	2	
3	1 PARABOLIC	0.17945 Other	1.48	0.00	2.77	
0	1 CIRCULAR	0.00744 RCP	22.92	1.17	36.97	
3	1 PARABOLIC	0.0674 Other	10.68	0.21	20.45	
0	1 IRREGULAR	0.03539 Other	0	0	0	
0	1 CIRCULAR	0.00777 RCP	52.46	0.41	96.51	
0	1 CIRCULAR	0.00648 RCP	1.85	0.22	2.84	
0	1 IRREGULAR	0.02576 CONC	0	0	0	
0	1 CIRCULAR	0.33922 CMP	19.27	60:0	33.52	
0	1 CIRCULAR	0.02456 RCP	71.68	0.32	127.18	
0	1 CIRCULAR	0.10048 RCP	31.59	0.44	33.07	
0	1 CIRCULAR	0.10367 CMP	5.25	0.29	8.95	
0	1 IRREGULAR	0.08468 Other	3.44	0.01	90.9	
0	1 CIRCULAR	0.07684 RCP	6.52	0.22	11.27	
0	1 CIRCULAR	0.02637 RCP	6.77	0.4	11.67	

					•							
			LX	Isting	Existing Condition June	unctions		S Sum	Results Summary Lable	a		
ensions				2-year			T	10-year				100-year
		Z S	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total				
Rim	Depth	HGL		Inflow	Surcharging	HGL	Inflow	Inflow	Surcharging	Max. HGL	Max. Lateral	Max.
(feet)	(feet)	(2-year)	(2-	(2-	(2-year)	(10- year)	(10-	(10-	(10-year)	(100-year) (feet)	(100-year) (cfs)	100-ye
		(leet)	year) (cfs)	year) (cfs)		(feet)	year) (cfs)	year) (cfs)				
341.403	0	344.21	0	220.37	YES	344.41		248.78	YES	344.7	0	
	0	346.77	0	0	YES	346.77	0	0.0		347.93	0	
3347.275	0	347.27	0 0	00 338	YES	347.28		0 411 07	YES	349.03		
	0	330.6	0	337.28	ON	330.79				331.5	0	
	0	328.25	0	331.66	ON					329.36	0	
322.374	0	323.28	0	332.05	ON	323.45				324.14		
303.901	0	306.01	0	336.28	ON	306.42	0	498.94	NO	307.76		
	O (K)	395.5	0 0	24.01	YES	395.58		(T)		(1)		
7	0	406.66	0	0	YES	406.66					0	
	0	379.89	0	4.81	YES			80	YES		0	
	11.529	388.88	0	175.6	YES						0	
	5.975	384.59	0	175.71	YES			22			0	
	0.0	340.14		C.7	YES			4.7	YES			
314.412	10 567	304 68	0 0	787	NO NO	305 17		52.25		305 75		
	TO::01	374.17		103 49	ON NEW YORK			-				
	0 /	388.64	0	72.29	YES					(1)	0	
	0	360.32	0.04	0.04	YES		0.0				0.0	
1 355.651	0	360.69	1.44	13.7	YES			13.84				
	0	360.08	0	135.93	YES			П	YES		0	
	6	349.68	0	25.23	YES				YES		0	
348.925	o 0	340.92	0 1, 1,	30.74	ON	341.54	0 00	81.83	ON	342.58	0	
	0 0	374.44	C+: TT	3.52	YFS	('					0.12	
	0	377.49	7.43	10.11	YES		14.0				24.42	
7	0	409.14	0	1.49	YES		0			409.25	0	
	0	407.9	0	2.22	YES						0	
	0	443.22	0.69	4.85	YES					443.26	2.35	
	0	462.81	7.06	7.06	YES	462.88	12			462.92	22.63	
	0	458.37	0.26	7.29	YES	458.42				458.51	0.6	
	0	499.92	5.17	17.36	YES	500.27	9.42			500.65	16.51	
	0	480.9	2.96	13.04	YES	480.95	5.46	18.91	YES			
	Ø LUK	484.47	0.18	10.94	YES	480.57						
7 375,557	0.557	374.05	2.02	2.00	YFS	374.27	0.7.0	4.44	YES	374.56	0.32	
	12.835	431.54	0	77.28	YES	431.65						
	7.952	416.48	0	53.8	YES					421.11	0	
	0	420.91	0.98	32.81	YES		1.5	7		424.42	2.52	
9 449.159	9	445.44	0	9.43	YES	446.41	0	15.73	YES	447.58	0	

			Ŧ	isting	Existing Condition lung	unctions		Sum	Results Summary Table	0		
				0								
ensions				z-year				10-year				100-year
Rim Elevation	Depth	Max. HGL (2-vear)	Max. Lateral Inflow	Max. Total Inflow	Surcharging (7-vear)	Max. HGL (10-	Max. Lateral Inflow	Max. Total Inflow	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	Max. Infl
(feet)		(feet)	year) (cfs)	year) (cfs)	(100.6-2)	year) (feet)	year) (cfs)	year) (cfs)	(100)	(feet)	(100-year) (cfs)	(100-ye
	7	390.32	0	138.92	YES			236.12		395.74	0	
9 392.309	0	394.87	1.67	125.73	YES	396.86	2.69	152	YES	398.62	4.31	
	0	417.46	0	0.16	YES			97.01	YES	417.89	0	
	0	395.32	0	63.3	YES			104.69		395.89	0	
	0	443.93	7.4	7.59	YES					444.46	23.31	
416.806		410.91	11.02	33.8	YES	411.19	20.44	51.42	YES	411.48	36.44	
	0	334.65	18.07	155.71	ON			170.06	OZ	335.59	57.6	
.5 333.38	9.13	329.23	0	131.49	ON	334.39	0	344.94	ON	335.17	0	
3 382.41	4.08	380.09	5.29	48.02	YES	382.89	9.27	60.42	YES	383.08	14.85	
	7.5	386.44	0	153.96	YES			261.18	YES	391.62	0	
386.892	10.392	379.35	2 30	157.38	YES	380.29	0 22 7	277.46	YES	382.34	0 2	
	2.5	407.75	0	31.83	YES			49.05		408.32	0	
	7	401.49	8.02	37.31	YES		13.4	57.39		402.03	22.55	
396.922	7	392.69	0	45.44	YES	394.48	0	68.32	YES	396.05	0	
	7	392.7	0	38.16	YES			58.46			0	
	12.741	385.71	0	175.93	YES			321.08			0	
(1)	10.03	391.78	0	209.63	YES			235.04		394.65	0	
397.87	0	398.19	7.83	2.83	YES	398.25	4.6	4.63	YES	398.32	6.7	
	5.5	376.86	0	22.6	YES		0	29.55		378.84		
	∞	394.85	0	165.65	YES			167.18		397.5	0	
4 397.974	7.75	396.02	0	153.26	YES	397.42	0	154.59	YES	398.38	0	
	4	397.95	0	0.78	YES			1.27		400.29		
	7.75	401.33	0	157.39	YES		0	156.06		402.01	0	
7 415.359	6.759	416.64	0 0	61.49 8 15	YES	416.75	0 6 77	13 57	YES	416.86	0 0	
	0	337.27	0.11	46.77	ON			72.42		338.25	0	
	16.661	383.65	0	50.7	YES	(1)		85.5		389.63		
3 441.73	6	433.36	0	5.12	YES	433.59	0	8.84	YES	521.31	0	
1 459.585	8.675	451.29	0	2.23	YES	451.42	0	3.92	YES	529.36		
	8.272	447.73	0	2.22	YES		0	3.91		529.99	0	
442.716	6.476	436.6	0	3.1	YES		0	5.45		524.35	0	
		435.28	0	4.93	YES			8.82	YES	505.64	0	
	10.898	437.49	0	9.12	YES			15.89	YES	513.44	0	
	8.442	440.16	0	2.21	YES			3.9	YES		0	
	9.686	453.45	0	2.24	YES	7		3.93	YES			
449.186	6.146	443.39		2.21	YES		0	3.9				
421.927	11.927	410.16	0	0.62	YES	410.2	0	0.98	YES	461.18	0	

	100-year		0	0 0	0	0	0	0	0	0	0		0	0	0	0	0	0 0	0 0	0	0	0 0	0 61	0	0	0	0	0 0	0 0	0	0	0	0	0		0 0
		Max. Lateral Inflow (100-year) (cfs)																																		
		Max. HGL (100-year) (feet)	454.54	350.39	292.2	432.43	281.11	311.95	429.83	319	425.69	436.83	393.06	433.56	313.26	429.73	406.9	435.06	412.3	295.98	295.41	393.22	312 34	351.29	306.13	354.02	414.1	438.39	446.74	411.94	415.44	414.26	435.42	434.87	434.63	00.704
Junctions Results Summary Table	•	Surcharging (10-year)	YES	YES	ON	YES	ON Z					YES	YES						YES				YES	YES		YES			YES	YES		YES		YES	YES	
s Sum	10-year	Max. Total Inflow (10- year) (cfs)	4.1	10.59	4		915.67			74		79.41		7			۵,		3.11	7	(1)		20.83						1.20	()			27.4		0 0	
Result	\	Max. Lateral Inflow (10- year) (cfs)		0 0									0								0		0 0			0						0		0		
ctions		M (fe		350.39			280.48				7	435.2					40		411.85			*)	31216			354.01			440.00			414.15			451.00	
Existing Condition June		Surcharging (2-year)	YES	YES	ON	YES	ON Z	ON	YES	ON	YES	YES	YES	YES	ON	YES	YES	YES	YES	ON	ON	YES	YES	YES	ON	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES YES	יובט
isting	2-year	Max. Total Inflow (2- year) (cfs)	2.11	6.22	358.12	15.97	557.07	0.91	1.98	356.04	4.1	1 07	43.12	44.51	53.66	89.8	37.49	2.54	0.17	18.3	18.99	7 5	10 93	0.02	3.21	0.04	0.71	0.32	0.69	15.92	17.01	18.26	15.39	0	0 0	0.00
Ë		Max. Lateral Inflow (2- year) (cfs)	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0	0 0	0	0		0 26	0	0	0	0	0	0	0	0	0	0	0	0	
		Max. HGL (2-year) (feet)	454.44	350.39	290.63	432.09	280.01	311.89	429.51	317.95	425.64	434.27	393.01	433.56	311.5	429.56	405.92	434.92	410.03	292.45	293.19	392.84	311 98	351.28	303	354.01	414.07	438.37	440.02	401.55	415.03	414.08	429.09	431.08	431.00 437.0E	727.62
		Depth (feet)	0	0 0	0	0	0	0	0				0	4.535	0	0	5.18	O L	0 1	3.21	4.		1.0/3	0	3.5	0.566	0	0	0 0	0	1.259	0	11.5	9 1	0 0	
	ensions	Rim Elevation (feet)		2 350.392 7 445.997			5 276.635	3 319.993	.5 429.407			1 451.881							7 414.937				316 506			4 354.566			5 443.335			9 413.877			430.070	

	100-yea	Max	(100-ye	0	0		0	0				0	0	2 6			0	0	0			0	0	0					0	0	0		0	0	0			0
		Max. Lateral Inflow	(100-year) (cfs)											1.4																								
O		Max. HGL (100-year)	(feet)	486.76	283.67	310.61	459.25	439.51	47.01	449.62	415.65	394.08	350.17	442.95	440.03	442.25	478.34	415.21	405.92	447.01	338.74	354.74	327.7	320.33	313.83	490.03	322.93	375.99	496.71	441.78	502.57	435.79	443.99	462.87	425.77	450.07	423.2	421.22
mary Table		Surcharging	(10-year)	YES	ON	ON	YES	YES	YES	YES	YES	YES		YES	YES			YES	YES		VES	YES		ON	ON	YES	YES		YES	YES	YES		YES	YES	YES	YES	YES	YES
Results Summary	10-year	Max. Total Inflow	(10- year) (cfs)	L	24.11	u,			0 6.67				,	51.9	7			u ,		10.8		(7	22.74	25.27			22.73		C	79.14	41.83		4.46				31 37	
	ν-1	Max. Lateral Inflow	(10- year) (cfs)		0	0	0	0			0	0	0	0.92	ی ر	0	0		0			0													0			0
Junctions		Max. HGL (10-	year) (feet)	486.51	282.88			43	479					443.11			478.34	415.13			338.04					4	321.8 406.19			404.49	423.55						421.05	
Existing Condition June		Surcharging	(z-year)	YES	ON CX	ON	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	VFS	YES	ON	ON	ON	YES	VFS	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES
isting	2-year	Max. Total Inflow	(2- year) (cfs)	13.1	22.51	333.62	1.93	2.27	4.12	2.28	0.32	6:39	28.29	40.32	40.18	0.48	0	43.18	43.13	5.88	CC./I	12.94	12.95	12.89	12.89	0.55	1.37	2.81	9.81	46.61	24.63	12.93	2.55	2.56	12.79	19.03	26.21	1.86
EX		Max. Lateral Inflow	(2- year) (cfs)		0				0 0					0.59			0	0			0 0		0				0 0				0						0	
		Max. HGL	(feet)	486.34	282.57	308.97	459.22	439.36	479	449.47	415.61	393.76	349.55	437.97	434.56	442.19	478.34	415	405.7	443.51	492.74	354.42	327.37	319.99	311.65	490	321.22	375.69	430.28	403.65	422.76	430.38	443.71	462.67	421.69	449.97	416.91	408.6
			(reet)	9.674	5.537	0	0.751	55.462	7.084	34.287	9	1	0	13.141	11.001	2	0.547	7		4 0	0 0	866.6	2	5	S.	0 L	n C	0	7.153	14.322	15.433		4.5	7.5	4.5	20	16.5	
	ensions	Rim Elevation	(feet)	.2 495.586	283.037		7		480.009					7049.407			4 479.047	7			7 492.567		.5 331.945	.6 324.546			6 406.116			2 416.522	8 437.233		1 447.831		423.764		422.621	

									•			
			LX	Isting	EXISTING Condition June	Junctions		s sum	Results Summary Lable	a)		
ensions				2-year			1	10-year				100-year
r Rim	Depth	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral	Max.
Elevation (feet)	(feet)	(2-year) (feet)	(2- year)	(2- year)	(2-year)	(10- year) (feet)	(10- year) (cfs)	(10- year) (cfs)	(10-year)	(100-year) (feet)	Intlow (100-year) (cfs)	Int (100-ye
3 357.793	4.5	353.68	3.44	3.44	YES	353.82			YES	354.01	10.63	
7 329.427	3	326.71	0.71	0.71	ON	326.8	1.22	1.22	ON	326.9	1.95	
1 441.85	0	441.91	0.72	0.72	YES	441.92		1.23	YES	441.93	1.97	
9 451.819	2 222	451.83	0.5	0.5	YES	451.84	0.87	0.87	YES	451.84	1.4	
3 418.869	0	419.03	0.18	0.18	YES	419.05	0.27	0.27	YES	419.09	0.42	
1 372.761	5.5	370.07	2.83	56.13	YES	372.81	4.64	97.95	YES	373.14	7.33	
.1 426.441	7	419.44	0	0	YES		0	5.27	YES	426.71	0	
	8.009	418	0	0	YES			90.9	YES	418.77	0	
	3.5	311.06	3.39	3.39	ON	311.18		5.47	ON	311.33	8.64	
3/5.63/	5.5	370.92	1.8	1 60	YES	3/1.05	2.98	31.21	YES	3/1.1/	4.87	
	0 0	374 57	1.09	21.69	CET X	375 16		80	VEC	375.71	4.30	
m	4.5	301.11	0.0	19.04	NO	304.77			ON	306.98	2.39	
	0	499.92	0	25.35	YES	500.27		4.87	YES	500.65	0	
8 313.858	4.5	309.89	8.43	8.43	ON		14.87	14.87	ON	313.55	25.49	
314.382	4.5	310.24	4.3	4.3	ON		7.74	7.74	ON	310.85	13.32	
	4.5	306.93	2.55	10.97	ON	307.32		19.47	ON	311.66	8.09	
310.718	4.5	306.73	2.92	7.21	ON :			12.8	ON :	310.18	8.99	
7 291.386	4.686	290.55	0.46	16.76	ON ON	290.95	0.75	7.25	OZ Z	292.45	1.24	
291.021	3.5	290.36	1.99	26.76	ON N	290.65			02	292.47	5.79	
	3	330.55	13.49	13.49	ON		7		ON	332.22	42.32	
306.682	3	304.16	7.68	8.5	ON	304.33	13.43	15.09	ON	304.58	23.19	
7 454.91	0	454.65	0	7.24	YES	454.67	0	11.93	YES	454.72	0	
	2	301.38	0.45	6.78	ON			11.67	ON	305.51	1.17	
304.522	2	299.93	3.52	3.52	ON :			5.72	ON :	300.18	9.1	
3 301.453	V II	1.762	4.08	/5./	ON C	7 201	6.48	12.16	OZ Z	297.55	10.26	
6 435.306	2	434.62	8.92	11.29	YES	440.96	15.57	19.87	YES	450.82	1.00	
	5	434.01	4.25	15.44	YES	440.09		27.04	YES	446.56	11.84	
8 450.438	5.5	445.57	0.7	15.24	YES	445.8		28.91	YES	446.13	1.79	
5 475.205	5	470.72	2.66	2.66	YES	470.89	4.41	4.41	YES	473.96	7.16	
9 441.503	12.503	429.57	0	4.54	YES	429.75	0	7.69	YES	429.95	0	
7 475.588	5.861	470.28	0.3	2.95	YES	470.73		4.86	YES	473.9	0.72	
	5	471.51	7.27	7.27	YES	471.79	1	12.56	YES	474.86	20.75	
5 474.845	5	470.32	2.58	2.58	YES	470.73		4.29	YES	473.89	6.98	
	6.428	469.46	0.4	14.38	YES	470.56		24.07	YES	473.38	1	
	6.889	470.23	0.44	7.71	YES	470.72	0	13.23	YES	474.04	1.01	
	m !	469.52	0.97	0.97	YES	470.6		1.5	YES	472.58	2.32	
475.988	4.5	471.68	1.09	1.09	YES	471.73	1.7	1.7	YES	471.79	2.61	

on lunctions Results Summary Table		Max. Lateral Total HGL Inflow Inflow (10-year) year) year) year) (feet) (cfs) HGC (10-year) (10-year) (feet) (100-year) (feet) (100-year) (feet) (100-year) (feet)	460.42 0 0.22 YES 460.43	YES 469.01 2.12 2.38 YES 469.83 3.29	474.65 50.65 70.65 YES 474.75 8	467.55 3.44 80.73 YES 468.16	489.84 0.51 25.54 YES 494.12	YES 467.26 3.08 78.52 YES 467.89 4.76 NO 286.46 15.31 21.86 NO 286.76 25.27	293.21 8.82 8.82 NO 293.24	283.16 0.1 23.88 NO	391.62 0 153.3 YES 392.07	NO 318.65 2.8 2.8 NO 318.71 4.72	363.04 1.84 1.84 YES 363.09	465.6 2.33 2.33 YES 465.73	YES 464.95 2.15 4.47 YES 465.07 3.56	434.00 1.32 3.00 1E3 440.00 434.00 1.32 434.00 434.00 1.32 434.00	435.66 5.91 5.91 YES 439.27 9.8	2.14 2.14 YES 460.81	432.17 8.95 8.95 YES 437.93 14.3	36.72 YES 424.42	421.36 2.13 17.29 TES 419.25 0.78 4.16 YES	416.02 1.81 2.45 YES 421.2	418.64 5.58 9.03 YES 421.07	YES	421.10 17.43 37.44 TES 421.43 421.45 471.08 2.52 2.52 YES 471.27	470.56 0.63 3.32 YES 470.63	498.77 25.09 25.09 YES 499.2 47	YES 469.87 1.22 1.22 YES 469.92 1.9	422.33 0 10.00 TES 424.42 1.7 M66.13 0.03 3.33 VES M66.10 1.7	476.75 0.26 1.11 YES 476.79	480.24 0.86 VES 480.29	483.37 0.43 0.43 YES 483.38	427.49	757.23 2 62 2 02 70 VEC A67.07
		Max. Lateral Inflow (10- year) (cfs)	0	2.69	50.65	3.44	0.51	3.08	8.82	0.1	0	2.8	1.84	2.33	2.15	, U.32	5.91	2.14	8.95	0 0	0.78	1.81	5.58	2.57	2.52	0.63	25.09	1.22	0 03	0.26	0.86	0.43	3.26	2 62
		Max. Surcharging (10- (2-year) year) (feet)																																
Existing Condition	2-year	Max. Max. Lateral Total Inflow Inflow (2- (2- year) year) (cfs) (cfs)		1.73 1.73 1.35 1.35	.,	ð		8.97 12.51		0.07 13.61	14		1.08 1.08		1.25 2.56			1.27 1.27		13 12 04	0.51 0.64			1.6 20.99			7	0.78 0.78	0 0 0.4					2 2 7 3 0
		Max. Lat HGL Infl (2-year) (3 (feet) ye (c	460.42	464.89	471.11	463.75	489.48	286.3	293.19	282.6	391.49	318.6	363	465.5	464.86	430.73	435.45	460.69	431.49	421.4	416.16	408.59	415.2	397.66	420.31	470.51	498.5	469.84	422.9	476.71	480.2	483.35	427.37	763.67
	ensions	Rim Elevation (feet)	479.884	5 473.745 5 5 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	474.533 4.	467.932 8.35	493.671	466.564 9	293.637	4 285.844 5	391.386 1.50		367.871	469.69	470.056 5.5	442.000	439.379	465.003	435.032 4	421.073 0	423.222	412.14	408.959	411.119 14.11			502.883	474.674 5	422.797		485.055	488.29	431.976	7 7 7 884

			•				-	(
			EX	Isting	Existing Condition Junctions Results Summary Table	tions	Result	s Sum	mary Table	O)		
ensions				2-year			1	10-year			. ,	100-year
Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year) (cfs)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	Max. Infl (100-ye
4 406.784	12	395.09	0.28	2.04	YES	397.02		12.13	YES		0.66	
	15	394.26	0.58	2.6	YES	397.15		11.93	YES	7		
402.713	7	396.62	4.38	6.54	YES	396.92		10.75	YES			
9 401.209	ა 1	396.71	2.93	48.17	YES	396.98	3.62	3.62	YES	397.45	5.88	
	2	389.17	8.3	8.3	YES	389.55	1	14.06	YES		2	
2 395.214	9.014	386.58	0.58	10.53	YES	386.69	96.0	17.57	YES	386.84	1.57	
3 392.925	5.625	388.27	1.73	66.6	YES	388.61	2.82	16.81	YES	389.17	4.55	
9 448.019	4.5	443.62	0.33	0.33	YES	443.65	0.52	0.52	YES	443.68	0.82	
	3.199	435.23	0.98	0.98	YES	435.36	1.6	1.64	YES		2.6	
.3 454.465	0	452.71	0	0 [YES	452.71		0	YES			
434.939	2.959	435.22	46.90	1 00	YES	455.34	84.20	85.5 61.0	YES	436.83	13/.2	
	0	420.29	0.28	2.67	YES	420.39		5.13	YES			
	3	413.06	0.29	0.29	YES	413.1	0.45	0.45	YES			
8 433.438	5	428.6	0.4	0.4	YES	428.64	0.64	0.64	YES	428.68	1	
.6 413.316	0	413.53	0.41	1.07	YES	413.58	0.64	1.69	YES	414.33	0.99	
3 434.83	7	428.09	1.1	1.5	YES	428.15		2.37	YES			
	0	502.25	10.24	10.24	YES	502.46		18.66	YES	50	,	
	2	440.23	0.35	0.35	YES	441.61	0.54	4.23	YES			
3 439.433	יט ר	434.65	1.42	1.42	YES	434.7	2.29	2.29	YES	434.77	3.65	
	2.855	433.19	0.67	1.15	YES	433.23		1.76	YES			
	5.484	440.51	0.3	36.32	YES	445.19		59.06	YES			
7 451.577	5	446.98	3.41	3.41	YES	447.1	5.78	5.78	YES	447.25	9.6	
2 445.952	5	441.37	3.71	3.71	YES	445.22	6.3	6.3	YES	446.14	10.47	
	5.5	448.18	1.69	1.69	YES	448.25	2.84	2.84	YES			
	7.346	444.02	2.14	30.8	YES	446.16		50.52	YES			
7	5 10	446.09	0.48	0.48	YES	446.12		0.75	YES			
	20.525	441.82	0.33	44.57	YES	442.11	0.53	45.38	YES			
.9 441.456	7.837	442.53	105.11	111.28	YES	442.82	183.78	183.78	YES		315.8	
	0	439.4	0	8.92	YES	439.4	0	10.12	YES			
	8.441	442.55	5.24	20.89	YES	442.75	3.6	40.43	YES		5.72	
448.695	14.48	443.33	0.43	18./9	YES	444.79	0.67	30.91	YES	448.05	1.04	
9 433.433	19.130	443.47	0.17 9.28	10.33 9 28	YES	443.14		30.22	YFS			
	7.579	443.95	0.41	9.69	YES	446.33	0.62	16.29	YES		0.94	
1 445.129	10.708	443.7	1.08	18.17	YES	445.75		29.94	YES	450.42	2.82	
446.578	12.084	443.82	1.29	17.08	YES	446.06	2.01	28.17	YES	451.28	3.12	
3 438.892	4.119	443.93	0.44	3.13	YES	446.26	0.67	6.47	YES	451.65	1.02	
1 437.841	2.931	443.9	0.48	3.59	YES	446.16	0.73	7.17	YES	451.38	1.12	

			EX	isting	Existing Condition Junc	unctions	Result	s Sum	Results Summary Table			
ensions				2-year			1	10-year				100-year
Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year) (cfs)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	Max. Infl
6 478.286	5.5	473.55	6.02	6.02	YES	473.83	10.71	10.71	YES	474.19	17.94	
4	IV I	452.28	0.11	0.67	YES	452.34	0.17	1.08	YES	452.41	0.27	
9 456.19	2	451.32	0.16	0.81	YES	451.36	0.26	1.32	YES	451.4	0.4	
456.152	5.552	453.82	0.48	0.48	YES	453.87	0.00	0.92	YES	453.13	1.23	
	2	453.42	0.05	0.52	YES	453.48	0.07	0.84	YES	453.56	0.11	
	5.5	431.62	16.74	16.74	YES	435.26	30.38	30.38	YES			
	0	495.65	0.53	0.82	YES	495.66	0.86	0.86	YES	495.68	1.33	
	8.062	426.42	0	53.36	YES	433.7	0	97.2	YES	434.68		
	0	450.74	0	3.15	YES	450.79	0 !	5.35	YES	450.86		
376.654	9 17 77	371.91	24.8	24.8	YES	372.36	41.87	41.87	YES	373.17	69.51	
r	12.137 12.436	392.98	1.80	48.28	YES	383.59	3.11	85.52	YES	393 07	5.11	
	6.341	374.41	0.12	60.57	YES	375.08	0.19	102.09	YES	376.39		
	6.12	436.15	4.92	4.92	YES	436.39	8.83	8.83	YES	506.41	C	
7 449.524	8.254	441.68	4.98	4.98	YES	441.82	8.83	8.83	YES	514.46	15.15	
.2 437.457	7.037	431.6	5.01	6.6	YES	434.15	8.89	17.64	YES	503.92	15.34	
	8.317	433.81	0.76	92.0	YES	433.89	1.23	1.23	YES	521.91		
	7.616	447.63	2.75	2.75	YES	447.86	4.77	4.77	YES			
	7.289	445.33	0.85	4.19	YES	445.45	1.4	7.15	YES		2.31	
7 431.233	4.233	428.6	7,	9.65	YES	428.87	00 7	11.56	YES	429.21	0	
	14.665	453.01	0.78	11.47	YES	426.91	1.22	19.62	YES			
	11.694	426.17	8.23	13.01	YES	426.42	13.85	22.14	YES			
	15.909	455.07	2.24	2.24	YES	455.16	3.93	3.93	YES	535.01	6.58	
9 421.039	8.139	413.05	0.62	0.62	YES	413.09	86.0	0.98	YES	461.23	1.53	
1 447.819	8.609	439.6	0.97	3.1	YES	439.73	1.67	5.45	YES	527.08	2.7	
8 442.532	12.552	430.24	0.27	1.64	YES	430.31	0.42	2.61	YES	504.96	0.67	
	8.13	406.89	1.59	1.59	YES	407.02	2.66	2.66	YES	442.5	4.23	
8 454.93	8.13	447.26	0.61	3.36	YES	447.41	1	5.93	YES	515.39		
	15.093	423.13	0.24	24.64	YES	423.78	0.37	42.03	YES	503.27	0.56	
	П	415.08	0	17	YES	415.32	0	29.86				
1 448.741	8.131	440.8	1.41	1.41	YES	440.85	2.38	2.38	YES	521.94		
	8.128	426.35	2.54	12.3	YES	426.51	4.19	21.76		491.86		
	11.255	432.85	0.2	1.38	YES	432.91	0.32	2.2	YES	505.47	0.5	
	8.138	406.53	8.15	9.71	YES	406.69	13.78	16.4	YES	442.47	22.67	
	18.797	373.18	1.29	1.29	YES	373.22	2.05	2.05		373.27		
.6 390.013	23.553	367.67	0.54	30.52	YES	368.05	0.84	47.29		372.11	1.29	
387.892	19.892	369.1	0.24	30.23	YES	369.43	0.38	46.68	YES	372.5	9.0	
7 405.627	0	405.79	0	20.21	YES	405.79	0	22	YES	405.83	0	
.8 386.848	0	386.85	0	0	YES	386.85	0	0	YES	386.85		

	100-year	Max. Inf (100-ye																																		
		Max. Lateral Inflow (100-year) (cfs)	3.96	0 0.43	0.34	0.49		0.12	11.66	9.0		0 0	0	1.39	2.19	T:4	0	0	0.38	0 7	7.24		8.82	4.97	0.63	0		10.5	0	1.45	3.2	3.1	1.38	6.07		2.96
		Max. HGL (100-year) (feet)	427.74	420.56	426.15	428.2	430.7	416.36	439.7	416.12	404.58	381.89	423.15	424.25	437.05	455.60	420	448.4	417.08	378.82	401.30	477.25	470.33	470.06	465.26	403.2	451.73	464.79	463.65	463.76	464.67	468.11	460.87	456.45	456.47	456.18
Junctions Results Summary Table		Surcharging (10-year)		YES			YES	YES	YES			YES			YES	YES	YES	YES		YES	YES		YES	YES	YES	VEC		YES	YES	YES	YES	YES			YES	YES
s Sum	10-year	Max. Total Inflow (10- year) (cfs)		4.26				1.22	16.01		6.32	80.0 80.0				19.0	0	0	0.24	0	1.71		5.32			16.98		5.92	15.33			1.89		4.74	1	1.5
Result	1	Max. Lateral Inflow (10- year) (cfs)	2.18	0.28	0.22	0.31	3.55	0.08	6.75	5.14	0	0 0	0	0.9	1.41	0.91	0	0	0.24	0 ,	1./1	3.32	5.32	3.01	0.39	0.90	0	5.92	0	0.92	1.92	1.89	0.87	3.77	1.05	1.5
ctions		Max. HGL (10- year) (feet)	427.59	420.19	425.97	428.03	430.51	416.22	439.66	415.97	404.53	381.81	423.13	424.18	436.6			448.4	417.06	378.82	459.77	480.93	468.42	467.89	463.31	403.24	451.01	461.91	461.69	461.84	461.89	457.13	457.05	451.15	451.11	451.07
Existing Condition June		Surcharging (2-year)	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	VEC	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES
isting	2-year	Max. Total Inflow (2- year) (cfs)	1.07	2.42	2.28	2.17	1.97	0.78	9.53	3.4	3.4	4.25	0.05	0.58	21.93	20.00	0.3	0	0.16	0 0	2.6	4.51	3.07	4.81	0.88	11.04	0.0	3.29	12.59	0.57	1.11	1.11	0.53	2.85	0.62	0.7
Ex		Max. Lateral Inflow (2- year) (cfs)	1.07	0.18	0.14	0.2	1.97	0.03	3.96	2.64	0	0 0	0	0.58	0.89	0.0	0	0	0.16	0	0.39	1.92	3.07	1.74	0.22	3.32	0	3.29	0	0.57	1.11	1.11	0.53	2.24	0.62	0.7
		Max. HGL (2-year) (feet)	427.45	419.97	425.83	427.91	430.38	410.1	439.12	415.85	404.49	381./3	423.12	424.12	435.9	434.38	419.99	448.4	417.05	378.82	454.38	459.58	462.63	461.72	457.83	437.77	456.22	455.74	454.57	454.87	457	456.52	451.75	446.92	447.72	445.3
		Depth (feet) (2.068	9.957	9.24	8.994	8.444	8.125	0	8.307	0	2 13	2.132	2.093	8.128	0.472	0	0	8.264	0 70,7			7.15	8.116	7.507	10 805	10.003	7.504	12.577	10.116	6.117	7.133	8.131	8.134		9.129
	ensions	Rim Elevation (feet)		432.756				6 425.215		3 423.837	4	2 425.75 2 475.75	7	425.933		435.532	2 419.982			378.818	.2 465.839		2 469.35			0/6.104	7 451.007		0 462.577	4 462.656		7 463.403	3 459.761			.5 454.279

							•					
			EX	isting	Existing Condition June	tions	Result	s Sum	Junctions Results Summary Table	a)		
ensions				2-year			1	10-year			, ,	100-year
Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year)	Max. Total Inflow (2- year)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year)	Max. Total Inflow (10- year)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	Max. Infl (100-ye
2 404 423	2 303	402.26	(CTS)	(CTS)	YES	402 37	(CTS)	(CTS)	YFS	402 49	2 94	
	2.132	379.81	0.3	1.29	YES	379.95			YES	380.09	2.06	
5 340.225	0	340.38	0.35	1.32	ON	340.46			ON	340.54	1.28	
369.935	2.125	368.08	0.93	2.53	YES	368.27	3.02	8.44	YES	368.5	6.73	
	0	390.53	0	0	YES	390.53		0	YES	390.53	0	
		351.84	0	0	YES	351.84		0	YES	351.84	0	
8 411.318	0 0	395.14	0 0	0 0	YES	411.32	0 0	0	YES	395.14	0	
	0	427.02	0	15.3	YES	427.17		27.49	YES	427.33	0	
420.914	0	421.02	0.07	0.07	YES	421.07	0.19	0.19	YES	421.11	0.33	
.5 426.15	0	426.33	0.34	0.34	YES	426.44	1.08	1.08	YES	426.53	2.34	
7	7.678		3.57	8.16	YES	440.82		14.44	YES	441.27	10.54	
402.84	10.32		1.34	33.74	YES	402.75		61.45	YES	406.99	3.3	
9 459./10	071.0	452.19	3.40	3.40	\ \ \ \ \	452.42	10 66	57.0	YES	452.65	10.53	
	10.686	393.81	3.23	39.17	YES	401.27		70.3	YES	413.13	9.09	
	8.126		1.2	4.67	YES	451.89		8.28	YES	452.12	3.46	
402.376	7.236	396.28	15.38	22.52	YES	426.51	26.91	39.8	YES	420.02	47.22	
	5.63	396.12	0	0	YES	396.12		0	YES	396.12	0	
2 465.982	0	466.94	0	0.97	YES	466.95			YES	466.96	0	
7	9.5	412.01	6.71	18.55	YES	417.58	11.1		YES	421.66	18.33	
3/8.15	0 0	3/8.33	0 0	20.99	YES	3/8.36	0	70.77	YES	3/8.42	0	
		378.84	0	0	YES	378.84		0	YES	378.84	0	
3 447.833		449.4	0	3.28	YES			4.92	YES	449.45	0	
	0	342.94	0	0	YES			0	YES	342.94	0	
7 298.545	5.778	293.88	3.81	3.81	ON			6.57	ON	299.05	10.75	
m	5.788	298.34	21.41	21.41	ON :		(1)	(1)	ON :	301.18	62.26	
7 305.53	5.783	299.99	1.25	1.25	ON C	300.007	2.16	2.16	0 0 2	300.15	3.48	
	5.78		7.6	8.84	OZ OZ			15.15	OZ OZ	299.36	22.31	
	2.782	293.24	1.64	7.72	ON		2	24.31	ON	296.2	4.43	
7 297.656	6.719	292.55	0	35.78	ON	296.4	0	55.22	ON	297.06		
5 281.806	4	282.67	3.63	38.66	ON	282.83	5.82	47.34	ON	282.96	9.2	
7 298.19	5.783	293.85	0.07	25.21	ON	299.01	0.11	40.28	ON	299.43	0.18	
	0		0	7.82	YES	444.29		14.15	YES	444.37	0	
439.226	7.406		0.94	3.57	YES	432.33	1.5	6.01	YES	432.47	2.43	
	21.618		0 67	41.94	ON	337.5			ON	337.86	0 0	
	7.335		2.53	22.14	YES	349.28		1)	YES	349.48	7.53	
	8.184		0.0	0.0	YES	412.55	D.		YES	412.65	L.53	
8707.978	0	407.98	0 0	3.55	YES	408	0	5.98	YES	408.02	0 0	

	100-vear	TOO-YEA	Max. Inf (100-ye																																		
			Max. Lateral Inflow (100-year) (cfs)	7.27	22.98				0	49.25		22.4		43.28		3.43		19.6			7.2	44.4			43.81	0.6					10.6		11.03		4.9		
0			Max. HGL (100-year) (feet)	433.39	388.71	383.83	373.71	356.56	338.73	356.78	346.69	369.06	361.29	359.23	358.02	358.02	356.56	356.56	388.39	351.99	379.38	379.58	441.52	417.32	422.78	336.18	309.4	331.01	313.28	338.17	338.64	406.22	288.93	284.72	290.07	284.57	390.64
lunctions Results Summary Table			Surcharging (10-year)	YES	YES				YES				YES							YES					YES					NO NO			ON			ON	
S SIIM	10-vear	-d-ycai	Max. Total Inflow (10- year) (cfs)		14.8		19.8		2.11				11.35					χ.		29.82		25	1.5		24.85	0.42			<u> </u>	16.81			6.55		2.9		
Recult			Max. Lateral Inflow (10- year) (cfs)	4.51	12.99	0	0	0	0	31.33	0	14.4	0	26.72	0	2.25	0	12.58	0		4.14	25.13	0	0 70 70	24.86	0.42	0	0	0		6.8	0	6.55	0	2.99		0
tions			Max. HGL (10- year) (feet)	433.27	388.36		373.69	355.82	338.4	353.45	346.66	367.64	361.16	357.15	355.87	355.87	354.39			350.46	373.28	(1)	441.5	413.4	416.04		309.4	330.03	311.95	336.68	337	405.99	288.9	284.72	290.06	284.02	390.64
Existing Condition lung			Surcharging (2-year)	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	ON	ON	ON	ON	NO	ON	YES	ON	ON	ON	ON	YES
isting	2-vear	2 -ycai	Max. Total Inflow (2- year) (cfs)	2.64	8.67	6.38	12.15	7.93	1.3	19.6	25.01	13.26	7.84	24.96	16.05	16.4	16.6	25.09	3.34	39.48	16.24	13.9	1.39	13.85	13.82	0.25	0.25	42.02	500.05	354.22	321.94	53.5	3.81	0	1.69	0 0	0
Ŧ			Max. Lateral Inflow (2- year) (cfs)	2.64	7.59	0.72	0	0	0	19.6	0	8.94	0	15.53	0	1.48	0	7.81	0	0 0	2.32	13.9	0	0 0	13.82	0.25	0	0	0	0 0	4.32	0	3.81	0	1.69	0 0	0
			Max. HGL (2-year) (feet)	433.16	388.15	383.79	373.66	355.78	338.14	351.54	346.6	366.81	361.01	355.96	354.54	352.95	351.78	351.77	388.29	349.52	372.92	374.48	441.48	413.05	415.54	336.12	309.4	329.92	311.46	336.61	336.85	405.31	288.88	284.72	290.05	284.02	390.64
			Depth (feet) (7.592	0 098 9	0.00	0	0	20.364	6.07	0	0	0 0	0 0	0	0	0	0	2.13	0 0	6.399	5.0		14.272	0.606	5.722	0	0	0	0.524	0	6.381	0	0	0 1	U L	
	pusions	21131313	Rim Elevation (feet)	2 440.412	387.525				9 406.459					5 354.155			(1)			7 348.967		378.66			421.106					442.524		4 405.421	2 288.98	2 287.162		269.023	

			M	isting	Existing Condition Junc	unctions		s Sum	Results Summary Table	a		
ensions				2-year			1	10-year				100-year
		Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total				2
Elevation	Depth (feet)	HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	(10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	(100-year)	Inflow Inflow	INIAX. Infl
(1661)		(feet)	year) (cfs)	year) (cfs)		year) (feet)	year) (cfs)	year) (cfs)		(reet)	(100-year) (cis)	ek-001)
439.133	7.133	432	0	0 [YES	432	0	0	YES	432	0	
438.767	11.207	445.67	28.54	4.53	YES	446.69	51.89	53	YES	428.47	91.28	
5 284.406	5	279.41	0	0	ON	279.41	0		ON	279.41	0	
	11	278.84	0	0	ON	278.84	0		NO	278.84	0	
7 288.337	11	277.34	0	0 0	ON Z	277.34	0	0	ON S	277.34	0	
890.068	0	397.83	15.9	20.75	YES	398.6	29.1	(1)	YES	399.78	49.7	
9 277.269	5	273.74	0	2.33	ON	274.27	0		ON	277.43	0	
	5	279.81	0	0.54	ON	279.85	0	0.6	ON	279.91		
	2		0	0	ON	282.61	0		ON	282.61		
278	4.5		0	0 ,	ON 2	274.23	0		ON 2	280.41	0	
5 288.1	3.6	285.1	0 0	4.34		285.31	0 0	7.61	ON ON	285.6		
2	5	2	0	4.33	ON	284.59	0		ON	285.05		
5 288.17	2.67	283.54	3.78	7.94	ON	283.97	6.8		ON	284.84	12.37	
	0	429.37	0	0.21	YES	429.39	0	0.3	YES	429.41		
	0		0	0	ON	335.96	0		ON	335.96	0	
	4.5		0	0	ON	302.98	0		ON S	302.98		
3 309.632	9.5	300.13	0	0 0	ON C	300.13	0		ON C	300.13	0	
		289.1	0	0	ON	289.1	0	0	ON	289.1		
		307.27	0	0	ON	307.27	0		ON	307.27		
	0	283.74	0	0	ON	283.74	0		ON	286.83		
2	0	279.94	0	75.13	ON	280.09	0		NO	283.52		
	9	309.5	0	10.82	ON	309.87	0		ON	310.27		
443.961 0 //2 850	0	444.09	0 0	4.80	YES	444.14	0	9.32	YES	444.2		
	0		0	20.87	YES	422.39	0		YES	422.39		
7	8.409		0	33.82	YES	410.1	0		YES	410.4		
4 330.639	0	334.67	0	156.9	ON	335.08	0		ON	335.64		
	2.918		0	33.05	ON	339.71	0	9	ON	339.88		
	4.5	391.97	0	2.53	YES	392.13	0	4	YES	392.34		
	0	399.37	0	0 3	YES	399.37	0		YES	399.37		
	4	395.78	0	41.89	YES	396			YES	396.38		
385.863	η C	402.33	0 0	0.64	YES	387.42	0 0	1.06	YES	387.67	0	
	2.889		0	165.68	YES	379.62	0	27	YES	380.69		
	1		0	3.29	YES	377.18	0		YES	378.11		
	0	374.31	0	189	YES	375.31	0	327.8	YES	376.26		
9.0798	0	370.79	0	242.43	YES	371.92	0	420.91	YES	372.79	0	

			> <u></u>	POLITA								
9												
ensions				z-year				10-year				100-year
i		Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total				
Rim Elevation	Depth (feet)	HGL (2-year)		Inflow (2-	Surcharging (2-year)	HGL (10-		Inflow (10-	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	Max. Inf
(reet)		(feet)	year) (cfs)	year) (cfs)		year) (feet)	year) (cfs)	year) (cfs)	•	(teet)	(100-year) (cfs)	(100-ye
6 432.66	4	428.66	0	0	YES	428.66		0	YES	428.66	0	
6 431.296	0	431.33	0	1.11	YES	431.34	0	1.93	YES	431.37	0	
7 419.927		420.77	0	21.19	YES	421.04	0	41.53	YES	421.3	0	
		376.71	0	82.95	YES	377.84	0	180.17		378.75	0	
3/3.41	0	3/6./2	0 00	18.6/	YES	377.85	7 4 7	20.78	YES	3/8/6	70.70	
7 364 917		365.24	00.0	3 18	YES	365.31	4.CT	441.02		350.00	0	
	0	340.79	0	403.75	ON	341.54	0	700.95	ON	343.08	0	
	0	340.82	3.88	281.68	ON	341.79	6.52	604.5	ON	343.46	10.72	
333.403	0	337.1	0	321.88	ON	337.41	0	453.49	ON	338.97	0	
314.352	0	314.83	0	15.76	ON	315.04	0	27.85	ON	315.68	0	
	11.5	424.45	0	53.3	YES	431.77	0	82.4			0	
1 451.752	7.652	444.61	0	3.14	YES	444.82	0	5.52			0	
	0	377.91	0	0.92	YES	377.91	0	1.53		377.92	0	
	4.2	383.91	0	0.26	YES	383.96	0	0.43		384	0	
		413.67	0	76.42	YES	414.67	0	86.08		417.08	0	
	4.498	401.1	0	79.26	YES	401.98	0	79.24		402.37	0	
	4.5	439.46	0	8.91	YES	439.48	0	10.09		439.5	0	
	5.5	441.49	0	0	YES	441.49	0	0		7	0	
	5.5	393.66	13.23	16.9	YES	394.19	21.96	28.45			35.22	
1)	י ר	348.35	0.35	25.52	YES	349.06	12.63	93.15		350.1	0.80	
334.52	4	383.48	1.37	338.20	YES	385.48	12.63	438.18	YES	386.74		
		381.93	0.18	20.31	YES	382.38	0.28	37.13				
6 280.66	0	282.75	0	551.4	ON	283.4	0	922.3	ON	285.38	0	
1 459.236	7.226	457.68	0	83.88	YES	459.58	0	114.86	YES	460.05	0	
5 428.38	3.88	425.61	7.02	7.02	YES	426.95	12.47	12.47	YES	428.95	21.85	
		452.14	1.18	5.64	YES	456.32	2.09	9.94		457.11	3.52	
		452.63	4.48	4.48	YES	456.45	8.14	8.14		457.11	14.2	
7 403.977		399.77	0	24.18	YES	400.21	0	37.9		403.61		
394.008	5.5	390.05	0.25	24.32	YES	390.77	0.59	38.32	YES	392.36	1.02	
m	4.5	369.38	6.52	7.56	YES	369.69	12.48	14.84		373.35	21.83	
.6 347.96	5.5	343.78	0	24.9	YES	344.48	0	45.03	YES	347.56	0	
.8 312.148	9	306.92	4.89	17	ON	307.19	8.33	30.59		307.6	14.99	
8 423.258	4.5	418.94	0.41	0.41	YES	418.98	0.64	0.64	YES	419.34	0.99	
4 331.454	0	333.52	0	329.81	ON	333.79	0	407.19		334.73	0	
.8 437.028	4.5	433.36	4.71	4.71	YES	433.73	7.95	7.95	YES	437.12	13.51	
	4.5	431.61	1.4	6.07	YES	431.89	2.32	10.17		434.42	3.86	
5 437.335	6.5	433.87	1.17	12.87	YES	434.06	1.97	12.96		434.18	3.27	
.,,	4	369.05	0.53	5.77	YES	369.26	0.87	10.37	YES	369.58	1.43	
9 430.99	0	431.26	1.54	2.88	YES	431.34	2.56	4.85	YES	431.43	4.27	

Max. Later. HGL Inflow HGL Inflow HGL Inflow HGL Inflow HGL Inflow HGL HGL HGL Year (feet) Year Year (feet) Year Yea	Existing C 2-year x. Max. ral Total ww Inflow (2- r) year) 0 0.13 4.16 14.4 0 3.09 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.79 0.78 0.70 0.78 0.70 0.78 0.70 0.78 0.70 0.78 0.70 0.78 0.70 0.78 0.70 0.78 0.70 0.78 0.70	Existing Condition Junctions 2-year Max.		Max. Lateral Inflow (10- year) (57) (165 1.65 1.65 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.67 1.68 1.69 1.6	10-year Max. Total Inflow (10- year) (cfs) (cfs) 0.21 2.1.3 2.46 5.46 5.46 5.46 5.46 6.27.99 7.1.07 7.1.07 7.1.07 6.27.96	Max. Max.	(100-year) (feet) (feet) (feet) (421.49 (421.4	Max. Lateral Inflow (100-year) (cfs)	Max. Infl (100-ye
Max. Late Max. Late Max. Late Max. Late Max. Late		YES	9 4 1 1 7 2 4 8 8 8 5 5 7	08057900	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Surcharging (10-year) YES YES YES YES YES YES YES YES NO NO NO NO NES YES YES YES YES YES YES YES YES YES Y	Мах. I (100-у (fee	Max. Lateral Inflow (100-year) (cfs)	Max. Infl
Rim (feet) Depth (feet) Max. (feet) Latel (feet) fleet) Max. (feet) Latel (feet) 367.455 0 367.46 441.439 0 421.39 441.439 0 421.39 441.439 0 421.39 441.439 0 421.39 441.439 0 421.39 441.439 0 421.39 441.439 0 421.39 402.346 4 401.93 337.274 3.5 336.9 400.05 400.16 1 401.538 0 400.16 420.806 0 400.16 442.916 5.916 421.43 442.916 5.916 421.43 442.916 5.916 421.43 442.916 5.916 421.43 442.91 3.67 401.05 433.397 3.67 401.05 433.397 3.874 431.17 433.312		YES	7 2 2 8 8 8 8 7 7 1 4 9 9	08027900		Surcharging (10-year) YES YES YES YES NO	(100-y	Max. Latera Inflow (100-year) (c	Max. Infl
Rim (feet) Depth (2-year) HGL (7-year) (7-year)<	E S S S S S S S S S S S S S S S S S S S	YES	7 2 2 8 8 3 8 4 7 7 1 1 4 9	08022900		Surcharging (10-year) YES YES YES YES YES NO	(100-y) (fee	Max. Latera Inflow (100-year) (c	Infl (100-ye
(feet) (feet) vean 367.455 0 367.46 421.182 0 421.39 441.439 0 440.82 404.026 7 397.14 404.026 7 397.14 405.57 4 401.93 407.07 4 401.93 407.07 4 401.34 407.07 4 401.33 420.004 0 400.16 426.838 6 421.54 401.538 0 400.16 426.838 6 421.54 426.838 6 421.54 426.838 6 421.54 426.838 6 421.54 426.838 6 421.54 426.838 6 421.54 426.838 6 421.54 427.43 425.63 421.63 448.526 5.5 446.36 433.397 3.67 431.63 436.91)	YES	(feet) 367.46 421.44 440.91 397.17 398.72 402.04 336.48 403.3 336.98 530.5 421.75	year) (cfs) 0 6.78 0 1.65 1.27 3.46 0 0 1.07 1.07 1.07 0 14.39 0	year) (cfs) (cfs) 0.21 21.3 21.3 5.46 1.65 1.65 1.67 29.35 27.96	YES	(fee	(100-year) (cl	(100-ye
367.455 0 367.46 421.182 0 421.39 441.439 0 440.82 404.026 7 397.14 405.57 4 401.83 405.57 4 401.93 405.57 4 401.93 405.57 4 401.93 407.53 0 335.95 407.53 0 430.34 11 426.838 6 421.54 14 426.838 6 421.54 14 426.838 6 421.54 14 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 448.526 5.5 446.36 1 441.017 3.67 407.35 1 441.017 3.67 411.93 1 432.54 3.874 431.66 1 434.554 3.874 431.64 1 <td< th=""><th></th><th>YES YES YES YES YES YES YES YES YES YES</th><th>367.46 421.44 440.91 397.17 398.72 402.04 336.48 403.3 336.98 530.5 421.75</th><th>0 6.78 0 1.65 1.27 3.46 0 0 1.07 27.96 27.96 14.39</th><th>21.3 21.3 21.3 5.46 1.65 1.27 3.46 627.99 1.07 29.35 27.96</th><th>YES YES YES YES NO NO</th><th></th><th></th><th></th></td<>		YES	367.46 421.44 440.91 397.17 398.72 402.04 336.48 403.3 336.98 530.5 421.75	0 6.78 0 1.65 1.27 3.46 0 0 1.07 27.96 27.96 14.39	21.3 21.3 21.3 5.46 1.65 1.27 3.46 627.99 1.07 29.35 27.96	YES YES YES YES NO			
421.182 0 421.39 441.439 0 440.82 404.026 7 397.14 402.346 4 398.64 402.346 4 401.93 402.347 4 401.93 407.07 4 401.93 407.07 4 403.25 407.07 4 403.25 430.004 0 490.34 1 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 427.338 425.36 427.43 431.382 4.5 427.43 411.017 3.67 411.93 434.594 3.874 431.6 434.594 3.874 431.6 438.41 46.5 447.53 3		YES YES YES NO NO NO NES YES YES YES YES YES YES YES	421.44 440.91 397.17 398.72 402.04 336.48 403.3 336.98 530.5 421.75	6.78 0 1.65 1.27 3.46 0 1.07 1.07 27.96 14.39	21.3 5.46 1.65 1.27 3.46 627.99 1.07 29.35 27.96	YES			
404.026 7 397.14 402.346 4 398.64 405.57 4 401.93 405.57 4 401.93 405.57 4 401.93 332.018 0 335.95 407.07 4 403.25 430.004 0 490.34 1 426.838 6 421.54 1 426.838 6 421.54 1 426.838 6 421.54 1 448.526 5.5 446.36 1 426.838 6 421.54 1 426.838 6 421.54 1 448.526 5.5 446.36 1 431.382 4.5 427.43 4 411.017 3.67 407.35 4 415.597 3.67 401.05 4 434.594 3.874 431.56 4 434.594 3.874 431.64 4 438.343		YES YES YES NO NO NO NO YES YES YES	397.17 398.72 402.04 336.48 403.3 336.98 530.5 421.75	1.65 1.27 1.27 3.46 0 1.07 0.41 27.96 14.39	1.65 1.65 1.27 3.46 627.99 1.07 29.35 27.96	YES NO NO NO NO NO NO NO NO NO N			
402.346 4 398.64 405.57 4 401.93 405.57 4 401.93 332.018 0 335.95 407.07 4 403.25 430.004 0 490.34 11 426.838 6 421.54 1 401.538 6 421.54 1 401.538 6 421.54 1 442.916 5.516 443.64 1 442.916 5.916 437.33 1 442.916 5.916 437.33 1 442.916 5.916 437.33 1 441.017 3.67 407.35 1 433.397 3.67 407.35 1 434.594 3.874 431.16 1 434.594 3.874 431.16 1 434.594 3.874 431.65 2 434.594 3.874 447.53 1 444.286 4.5 447.53 1 444.286 4.5 447.53 1 44		YES YES NO NO YES YES YES	398.72 402.04 336.48 403.3 336.98 530.5 421.75	1.27 3.46 0 0 1.07 0.41 27.96 14.39	1.27 3.46 627.99 1.07 29.35 27.96	YES YES NO YES NO			
405.57 4 405.57 4 407.07 4 407.07 4 430.004 0 426.838 6 426.838 6 426.838 6 426.838 6 420.56 5.5 448.526 5.5 448.526 5.916 442.916 5.916 442.916 5.916 443.43 4.25 441.017 3.67 431.382 4.5 411.017 3.67 431.382 4.5 432.397 3.67 434.594 3.874 434.594 3.874 434.594 3.874 434.594 3.874 434.594 3.874 434.594 3.874 441.286 4.5 441.286 4.5 441.286 4.5 441.286 4.5 441.304 398.77 441.304 398.77 444.898 4.5 444.898 4.5 444.898 4.5 444.898 4.5 444.898 4.5 444.696 4.5 444.696 <td></td> <td>YES NO NO NES YES YES YES</td> <td>402.04 336.48 403.3 336.98 530.5 421.75</td> <td>3.46 0 1.07 0.41 27.96 14.39</td> <td>3.46 627.99 1.07 29.35 27.96</td> <td>YES NO NO</td> <td></td> <td></td> <td></td>		YES NO NO NES YES YES YES	402.04 336.48 403.3 336.98 530.5 421.75	3.46 0 1.07 0.41 27.96 14.39	3.46 627.99 1.07 29.35 27.96	YES NO			
332.018 0 335.95 407.07 4 403.25 407.04 3.5 336.93 430.004 0 490.34 1 426.838 6 421.54 1 426.838 6 421.54 1 401.538 0 400.16 1 448.526 5.5 446.36 1 431.382 4.25 446.36 1 442.916 5.916 437.33 3 410.017 3.67 407.35 427.43 411.017 3.67 407.35 427.43 415.597 3.67 407.35 427.43 433.397 3.874 431.17 433.26 2 434.594 3.874 431.17 434.56 2 434.594 3.874 431.17 447.53 447.53 414.286 4.5 447.53 447.53 444.286 4.5 447.53 443.69.12 444.898 4.5 440.75 440.75 444.898 4.5 440.75		NO VES VES VES	336.48 403.3 336.98 530.5 421.75 400.17	1.07 0.41 27.96 114.39	1.07 29.35 27.96	YES YES YES			
337.73 3.5 36.93 430.004 0 490.34 1 426.838 6 421.54 1 401.538 0 400.16 1 401.538 0 400.16 1 426.838 6 421.54 1 401.538 0 400.16 1 442.916 5.916 437.33 1 442.916 5.916 437.33 1 442.916 5.916 437.33 1 441.017 3.67 407.35 1 411.017 3.67 407.35 1 433.397 3.874 431.17 1 434.594 3.874 431.17 1 383.112 4 379.45 1 451.107 4.25 447.53 1 442.286 4.5 447.53 1 444.286 4.5 432.63 1 444.286 4.5 440.75 3 444.898 4.5 440.75 440.75		NO YES YES	336.98 530.5 421.75 400.17	27.96 14.39 0	29.35	NO		0 0 1	
430.004 0 490.34 1 426.838 6 421.54 1 401.538 0 400.16 1 448.526 5.5 446.36 1 448.526 5.5 446.36 1 442.916 5.916 437.33 1 431.382 4.25 322.11 1 431.382 4.5 427.43 1 411.017 3.67 407.35 1 415.597 3.67 401.05 1 439.296 0 401.05 1 434.594 3.874 431.17 1 337.71 0 339.29 2 451.107 4.25 447.53 1 414.286 4.5 447.53 1 444.286 4.5 410.16 1 444.898 4.5 440.75 444.898 4.5 440.75		YES YES YES	530.5 421.75 400.17	27.96 14.39 0	27.96	YES			
426.838 6 421.54 401.538 0 400.16 450.56 5.5 446.36 1 448.526 5.5 446.36 1 442.916 5.916 437.33 423.43 431.382 4.25 322.11 427.43 411.017 3.67 407.35 407.35 415.597 3.67 407.35 407.35 433.397 3.87 431.6 2 434.554 3.874 431.17 2 434.54 3.874 431.17 2 438.312 4 379.45 2 451.107 4.25 447.53 1 414.286 4.5 410.16 447.53 444.286 4.5 410.16 432.63 444.898 4.5 440.75 444.898 4.5 440.75		YES	421.75	14.39	119				
401.538 0 400.16 450.56 5.5 446.36 1 448.526 5.5 443.64 1 442.916 5.916 437.33 1 431.382 4.5 327.11 1 431.382 4.5 427.43 1 411.017 3.67 407.35 1 415.597 3.67 407.35 1 433.397 3.87 431.56 1 434.594 3.874 431.17 2 383.112 4 379.45 2 451.107 4.25 447.53 1 414.286 4.5 447.53 1 414.286 4.5 432.63 1 442.9012 4.5 432.63 1 444.898 4.5 440.75 1 444.898 4.5 40.75 1 444.898 4.5 440.75 1		YES	400.17	0	C.+.	YES	7	23.9	
430.56 5.5 440.56 448.526 5.5 443.64 442.916 5.916 437.33 325.387 4.2 322.11 431.382 4.5 427.43 411.017 3.67 407.35 415.597 3.67 407.35 433.397 3.87 411.93 434.54 3.254 431.56 434.594 3.874 431.17 383.112 4 379.45 451.107 4.25 447.53 414.286 4.5 447.53 414.286 4.5 410.16 414.286 4.5 432.63 413.045 398.79 444.898 4.5 40.16 444.898 4.5 40.075			770	2000	4.6	YES			
442.916 5.916 437.33 325.387 4.25 322.11 431.382 4.5 427.43 411.017 3.67 407.35 415.597 3.67 401.05 439.296 0 401.05 433.397 3.254 431.56 434.594 3.874 431.17 383.112 4 379.45 451.107 4.25 447.53 414.286 4.5 410.16 436.912 4.5 432.63 444.896 4.5 440.75		YES	446.94	15.07	15.07	YES	454.07	26.44	
325.387 4.25 322.11 431.382 4.5 427.43 411.017 3.67 407.35 415.597 3.67 407.35 439.296 0 401.05 434.594 3.874 431.56 434.594 3.874 431.17 383.112 4 379.45 451.107 4.25 447.53 414.286 4.5 410.16 436.912 4.5 410.16 444.898 4.5 440.75		YES	437.42	2.4	6.82	YES			
431.382 4.5 427.43 411.017 3.67 407.35 415.597 3.67 407.35 433.397 3 430.63 434.554 3.254 431.56 434.594 3.874 431.17 383.112 4 379.45 383.371 0 339.29 4451.107 4.25 447.53 413.045 4.5 410.16 436.912 4.5 432.63 444.898 4.5 441.75	4.6 19.46	ON	325.68	7.96	22.57	ON	326.02	13.46	
411.017 3.67 407.35 415.597 3.67 407.35 415.597 3.67 411.93 399.296 0 401.05 434.554 3.254 431.56 434.594 3.874 431.17 383.112 4 379.45 451.107 4.25 447.53 414.286 4.5 410.16 438.477 0 398.79 444.898 4.5 440.75 444.898 4.5 440.75	5.2	YES	427.62	4.45	8.96	YES		7.3	
415.597 3.67 411.93 399.296 0 401.05 433.397 3.254 431.56 434.594 3.874 431.17 383.112 4 379.45 451.107 4.25 447.53 414.286 4.5 447.53 436.912 4.5 432.63 444.896 4.5 440.75		YES	407.35	0	0	YES			
399.296 0 401.05 433.397 3 430.63 434.554 3.254 431.56 434.594 3.874 431.17 383.112 4 379.45 337.71 0 339.29 2 451.107 4.25 447.53 388.343 28 361.28 1 414.286 4.5 410.16 436.912 4.5 432.63 444.898 4.5 440.75		YES	411.93	0	0	YES	7		
434.554 3.254 431.56 434.594 3.874 431.17 383.112 4 379.45 337.71 0 339.29 2 451.107 4.25 447.53 1 414.286 4.5 410.16 1 436.912 4.5 432.63 1 413.045 398.79 413.045 3 444.898 4.5 440.75	3.43	YES	401.08	0 8	6.12	YES	401.1	n 0	
434.594 3.874 431.17 383.112 4 379.45 337.71 0 339.29 2 451.107 4.25 447.53 1 412.286 4.5 410.16 1 436.912 4.5 432.63 3 398.477 0 398.79 444.898 4.5 40.75		YES	431.63	1.06	1.06	YES		1.7	
383.112 4 379.45 337.71 0 339.29 2 451.107 4.25 447.53 388.343 28 361.28 1 414.286 4.5 410.16 436.912 4.5 432.63 398.477 0 398.79 413.045 3 413 444.898 4.5 440.75	1.23 1.87	YES	431.32	2.07	3.12	YES	432.56	3.42	
337.71 0 339.29 2 451.107 4.25 447.53 1 388.343 28 361.28 1 414.286 4.5 410.16 1 436.912 4.5 432.63 1 413.045 398.79 413.045 3 444.898 4.5 440.75		YES	379.55	1.54	1.54	YES	(1)		
451.107 4.25 447.53 388.343 28 361.28 1 414.286 4.5 410.16 436.912 4.5 432.63 398.477 0 398.79 413.045 3 413 444.898 4.5 440.75	7	ON	339.93	46.63	84	ON		ω	
306.343 20 301.20 414.286 4.5 410.16 436.912 4.5 432.63 398.477 0 398.79 413.045 3 413 444.898 4.5 440.75	3.18	YES	447.84	29.9	29.62	YES	450.87	9.54	
436.912 4.5 432.63 398.477 0 398.79 413.045 3 413 444.898 4.5 440.75		YES	410.29	19.17	6 16	YFS			
398.477 0 398.79 413.045 3 413 444.898 4.5 440.75		YES	432.7	3.19	3.19	YES			
413.045 3 413 444.898 4.5 440.75	-	YES	399.01	0	24.92	YES			
444.898 4.5 440.75	3.48 3.48	YES	413.05	6.47	6.47	YES	5 413.11	10.83	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		YES	440.85	3.6	3.6	YES			
436.958 3 437.41	0.57 2.72	YES	437.45	0.0	4.48	YES	5 437.49	1.41	
387.672 0 387.82	4.8	YES	387.85	8.33	8.33	YES		13.83	
449.983 0 449.98		YES	449.98	0	0	YES			
4.5 303.94		ON :	304.4	4.94	151.23	OZ :			
302.901 5 304.42 11		ON 2	304.92	20.47	211.33	ON Z		(1)	
302.863 3.363 303.69 325.489 4 5 221.21	1.3 5/.//		304.1	2.19	32.28	OZ CZ	304.52	3.53	
324.764 4.5 320.51			320.6	1.49	4.34				
0.424 371.99	Ħ	YES	372.47	0	246.05	YES			

		100-year	Max. Inf (100-ye																																					
			Max. Lateral Inflow (100-year) (cfs)	6.18	42.32	16.6	31.03		2.45		0	0	6.18			40.11 6.85	0.00		6.2	22.6		15.75	0	0.4	1 29			17.04	39.91			,		7.29			12.2		4.42	0
	a		Max. HGL (100-year) (feet)	311.97	288.32	434.39	430.57	444.36	462.61	458.92	470.13	438	450.19		7	402.9	436.11	301.93	428.07	366.68	365.09	365.09	351.73	352.67		338	29	358.91	330.65	330.33	316.37	325.65	344.38	388.85	16.70C	315 04	292.47	294.37	297.85	282.91
:	Junctions Results Summary Table		Surcharging (10-year)	ON		YES			YES			YES	YES			YES					YES	YES		YES				YES	ON					YES					ON	ON
	s Sum	10-year	Max. Total Inflow (10- year)		O,	9.55	(1		1.54		0	3.73	3.76			29.66	83.1	7		12.98	38.08			0.28			01		85.69				D	4.28		ľ			2.92	0.02
	Result	—	Max. Lateral Inflow (10- year)	3.67	24.95	9.55	19	0 ,	1.54	0	0	0	3.76	0	10.29	78.27	† C	0	3.82	12.97	16.68	8.96	0	0.28	0 79	4.35	0	10.68	24.04	3.21	13.2	24.21	3.42	4.28	67.7		7.31	22.11	2.69	0
•	ctions		Max. HGL (10- year) (feet)	311.67		434.03			462.51		470.13	437.95	450.02			398.49	41			365.31	363.62				358.17				330.28					388.68						282.91
	Existing Condition June		Surcharging (2-year)	ON	ON	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	ON	YES	YES	YES	YES	YES	YES	YES	ON	ON	YES	ON	ON	ON	ON	YES	YES	IES	ON ON	ON	ON	ON	ON
	isting	2-year	Max. Total Inflow (2- year)	3.95	553.29	5.41	11.18	0.91	16.38	0	0	2.14	2.16	0	5.82	15.66	55.63	238.7	2.21	7.36	22.45	5.1	0.34	0.17	0.7	59.39	540.95	57.97	48.91	98.65	124.61	120.64	36	2.37	0.42	334.73	19.41	17.12	1.69	0.02
1	Ж		Max. Lateral Inflow (2- year)	2.01	14.5	5.41	10.62	0	0.91	0	0	0	2.16	0	5.82	12.83	0	0	2.21	7.36	9.59	5.1	0	0.17	0 77	2.5	0	6:39	13.88	1.9	7.84	14.16	2.03	2.37	00.4		4.17	12.69	1.6	0
			Max. HGL (2-year) (feet)	311.44	285.96	433.8	427.32	444.34	462.43	458.92	470.13	437.92	449.89	450.54	449.82	397.84	437.31	299.55	427.8	362.63	360.49	360.59	351.71	352.56	358.06	336.99	296.75	358.47	329.92	325.74	310.19	319.91	344.13	388.55	20.733	313 52	291.13	294.05	273.68	282.91
			Depth (feet) (0	0	2	4.5	0 0	3.67	0	0	0	4.5	0	0	4 T	7.997			4.5	5	4.5	0	m c	0 0	9	0	9	5			6.5	0	4.5	J. C		4		4.25	0.247
		ensions	Rim Elevation (feet)	4 311.124	9 283.829	438.124	3 430.8		465.85/		5 470.135	9 437.849	8 453.968		3 449.513	400.521				.2 366.442	7777.8363.777	1 363.551			359.717				.8 329.518					392.678			1 290.991		1 276.601	9 283.147

								•					
				ũ	kisting	Existing Condition Junctions Results Summary Table	ctions	Result	s Sum	mary Table	വ		
5	ensions				2-year			1	10-year			1	100-year
	Rim Elevation	Depth		Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL (10-	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL (100-year)	Max. Lateral Inflow	Max. Infl
	(feet)	(teet)	(2-year) (feet)	(2- year) (cfs)	(2- year) (cfs)	(2-year)	year) (feet)	(10- year) (cfs)	(10- year) (cfs)	(10-year)	(feet)	(100-year) (cfs)	(100-ye
ლ	292.293	4		1.0		ON		1.7		ON		2.8	
ლ დ	381.253	0	381.25	1 61	1 61	YES	381.25	3.02	3.07	YES	381.25	0	
) [299.021				33	ON			505.61	ON		0	
7	341.772	0		0	1.63	ON	m	0	3.07	ON	341.86	0	
و	364.496					YES				YES		0	
2 ,	367.832			0.3	0.3	YES		9.0	0.6	YES		1.04	
н и	390.481	0	390.48	0	0	YES	390.48	0 6	0	YES	390.48	0	
4	370.964					YES				YES		0	
o,	381.949					YES			0	YES		0	
κ'n	339.343	0	339.34	0	0	ON			0	ON	339.34	0	
9	289.196	0	291.69	0	540.88	ON	292.35	0	897.76	ON	293.38	0	
٩	359.086			0.89		YES		1.56	1	YES		2.56	
<u>ლ</u> (330.918				8.0	ON		0	1.5	ON		0	
7 9	361.332		361.33		0	YES	361.33	0	0	YES	361.33	0	
1 0	325,299	0		0	2.0	NO			3.6	NO		0	
4	335.384			2.0		ON		3.6	3.61	ON		5.9	
Ж	311.633	4.5	308	3.74	4.95	ON		6.3	8.11	ON	311.79	10.67	
2	310.685	4.25	306.96	1.93	7.02	ON	309.37	3.38	22.78	ON	311.55	5.73	
ιÚ	313.645					ON				ON			
.	326.631	4.2				ON		24.5	26.3	ON		43.8	
7 0	344.652					YES				YES		3.29	
7 0	325.417	0 0	325.47	0.19	0.19	ON ON	325.42	0.31	0.31	OZ OZ	325.42	0.48	
	360.875					YES			0	YES		0	
2	361.564	6.564		1.91	12.92	YES		3.4	22.79	YES	357.36	5.69	
3	361.523	5	357.18	11.02	11.02	YES	357.44	19.37	19.37	YES	358.09	33.06	
Н	414.837					YES			0	YES		0	
<u> </u>	355.797					YES				YES	m	0	
שׁ עַ	389.259			7		YES		-		YES		74.7	
၅ က	389.726	4.5	386.02	1./8	12.39	YES	386.42	3.09	21.82	YES	388.31	5.16	
7	409.422			0.31		YES		0.54		YES		0.86	
9	328.439	2.	326.35	1.46	1.46	ON	330.03	2.36	64.6	ON	331.07	3.78	
<u>0</u>	335.339		331.04	. 0.92		NO	331.09	1.45		ON	331.15	2.3	
4 (351.184		(,,,	0.3		YES		0.6		YES		1.03	
7 0	373.862	4.5	369.6	0 217	2.16	YES	369.67	0	3.64	YES	369.75	0 2 2	
7	432.923	0.				YES						3.76	

							-					
			EX	ıstıng	Existing Condition Junctions Results Summary Table	ctions	Result	s Sum	mary Table	(I)		
ensions				2-year			1	10-year				100-year
Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year) (cfs)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	Max. Infl (100-ye
9 387.39		387.75	0	1.22	YES	388.02		2.13	YES	3		
		446.64	7.24	9.95	YES	446.8		17.75	YES			
.0 448.482	8.482	446.64	2.35	4.56	YES	446.84	3.95	4.5	YES	446.99	6.34	
	4.5	399.05	2.02	2.02	YES			3.35				
9 426.099	0	426.31	0	7.03	YES			12.92	YES			
2 415.325	0	415.04	1.9	2.27	YES	415.05	2.93	3.57	YES	415.06	4.5	
	5	490.85	0.25	0.27	YES	490.9		9.0	YES			
	5	498.27	1.33	1.33	YES	498.36		2.37	YES		,	
	4.5	497.1	0.32	0.32	YES	497.15	0.5	0.56	YES	7		
1 492.591	5.	487.33	1.19	1.54	YES	487.41		2.73	YES		3.2	
3 395.33	χ, (τ	392 73	0 0	0 L	YES	397.85		ט א	YES	393 03		
7	3.832	407.33	5.12	5.12	YES		8.0	8.07	YES		12.6	
3 409.773	0	409.77	0	0	YES	409.77	0	0	YES	409.77	0	
6 410.656	3	407.66	0	0	YES	407.66	0	0	YES	407.66	0	
5 429.025	3	426.05	0	2.21	YES	426.06	0	3.82	YES	426.08	0	
	œ į	408.18	0	0	YES			0	YES			
1 426.291	4.5	422.31	0.93	1.44	YES			2.48	YES			
	4.5	428.77	0.51	0.51	YES	428.82	0.88	0.88	YES		1.4	
407.316	m m	404.5	0 22	2.81	YES	404.55	1 28	1.28	YES	404.61	0 0	
	ט וט	451.75	0.53	2.39	YES			4.34	YES			
	2	456.73	1.87	1.87	YES	456.83		3.44	YES			
9 400.5	1.5	400.33	0	15.86	YES	400.69	0	26.9	YES	400.81	0	
.1 424.141	4.5	419.82	0.51	0.51	YES		0	0.8	YES	419.92	1.24	
	0	358.14	0	24.55	YES			41.31	YES			
5 431.625	3.5	428.32	0.86	0.86	YES	428.37		1.38	YES			
	3.5	428.4	0.9	0.9	YES	428.46		1.44	YES			
7 482.094	5.094	477.IV	0.35	0.54	YES	17.1/4	0.54	0.83	YES	47.7.25		
	4.3	60.774	0.19	0.19	IES IES	477.06		0.29	YES		0.43	
467.093		463.60	1.03	1.03	YES		1.0	T.0	YES			
	3.5	474.89	1.57	1.57	YES		2.56	2.56	YES		7	
	4.5	441.06	1.18	1.18	YES			1.85	YES	7		
3 440.393	5	435.74	0.1	4.79	YES			7.61	YES		0.24	
.9 284.96		286.93	0	460.04	ON	286.99	0	527.84	ON	288.89	0	
440.704	4.5	436.68	0.41	3.52	YES	436.81	0.67	5.61	YES	436.98	1.06	
	4	437.89	99.0	99.0	YES			1.05	YES			
4 440.934	4.5	436.99	2.46	2.46	YES	437.16		3.91	YES			
7 401.57	3.5	399.13	4.91	7.18	YES	401.88	9.23	12.71	YES	402.57	16.01	

					1							
			LX LX	isting (Existing Condition Junc	unctions		s Sum	Results Summary Table	a)		
ensions				2-year			1	10-year				100-year
Rim	Depth	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral	Max.
(feet)	(feet)	(2-year) (feet)	(2- year) (cfs)	(2- year) (cfs)	(2-year)	(10- year) (feet)	(10- year) (cfs)	(10- year) (cfs)	(10-year)	(100-year) (feet)	(100-year) (cfs)	100-ye
1 400.271	3	394.67	0.41	0.41	YES	394.68	1.09	1.09	YES	394.68	1.96	
.6 402.676		400.02	0.15	1.51	YES	401.94	0.24	2.84	YES	402.63	0.38	
4				1.35	YES	414.23	0	2.7	YES		0	
9 274.05	2.1	.,		16.82	ON	274.14	0	110.59	ON		0	
419.451	0	419.3	0	0 0	YES	419.3	0	0	YES	419.3	0	
			2.0	2.03	YES	443.04	3.61	3.61	YES		5.91	
				1.38	YES	410.47	2.62	2.62	YES	,	4.53	
9 417.249	3	414.25	0	0	YES	414.25	0	0	YES	414.25	0	
.2 396.072		393.63	0.07	2.04	YES	393.8	0.16	3.68	YES		0.28	
.6 444.926			0	0	YES	441.93	0	0	YES		0	
			1.4	1.49	YES	418.56	2	2.9	YES		4	
332.392	0 7	392.44	3 23	1.81	YES NO	392.46	0 2	3.38	YES	392.49	10 38	
				394.73	02	274.05	0	729	ON ON		0	
			2	5.5	OZ	317.53	4.0		ON		7.0	
			m	3.89	ON	312.83			ON		1	
	5.5		7.09	10.96	ON	309.22	12.9	20.04	ON	309.47	22.1	
311.908				11.44	ON	306.62		21.72	ON			
			0.26	27.57	ON Z	305.6		50.96	ON Z		0.61	
311.098	4.5 C	306.75	0.65	0.65	OZ Z	306.8	2 16	2 16	OZ CZ	306.86	1.88 3.66	
		30.		2.65	ON	307.68		4.1	ON			
	4			5.18	YES	370.47	01	9.51	YES			
5 393.765	0	393.94	4.51	4.51	YES	394	8.05	8.05	YES	394.07		
			11	11.18	YES	386.73	20	20.03	YES			
			2.8	2.8	YES	382.86		8.09	YES			
424.458	2.458	425.15	5.31	5.31	YES	425.25	9.28	9.28	YES	425.33	15.6	
2 403,582				5.91	YES	403.88		9.79	YES			
	4			4.19	YES	388.19	7.66	8.48	YES			
7 392.087		385.87	9.42	87.68	YES	386.53	16.22	154.03	YES	387.21	27.11	
4 394.034	5	389.25	0.77	0.77	YES	389.35	1.32	1.32	YES	394.24	2.17	
.6 406.916	7	401.47	29.9	71.79	YES	402.07	11.92	127.24	YES	402.27	20.65	
366.056				0	YES	365.9		0	YES			
				65.86	YES	409.78	21	120.61	YES		,	
			2	54.25	YES	414.2	4.8	99.93	YES	7	8.13	
7				56.17	YES	412.78		104.05	YES	4	8.52	
7 432.97				3.75	YES	429.66		6.72	YES		11.25	
				3.73	YES	418.77		6.52	YES			
3/8.202	0	3/2.82	5./1	10.61	YES	3/3.04	9.78	19.22	YES	3/3.35	16.82	

			EX	isting	Existing Condition Junc	unctions	Results Summary	s Sum	mary Table	(D)		
ensions				2-year			1	10-year			, 1	100-year
Rim	Depth	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral	Max.
Elevation (feet)	(feet)	(2-year) (feet)	(2- year) (cfs)	(2- year) (cfs)	(2-year)	(10- year) (feet)	(10- year) (cfs)	(10- year) (cfs)	(10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	Infl (100-ye
.7 417.747	5	413.68	0	15.38	YES	415.09	0	27.35	YES	418.3	0	
8 294.138	0	298.66	0	437.03	ON	298.83		530.03	ON			
3 351.043	4.5	347.18	2.9	5.65	YES	347.42	S	9.76	YES	347.84	7.8	
	4.5	355.86	5.34	9.84	YES	356.85	11.38	17.26	YES		1	
37	9	371.15	7.94	19.38	YES	371.58	13.9	34.63	YES	(1)	24.13	
7 376.7	7 7	375.7	0	0 33	YES	375.7	0 57	0 0	YES	375.7	0	
	0	421.34	0.00	0.19	YES	421.35	0	0.31	YES			
7 432.207	3	431.68	0.88	0.99	YES	431.69	1.38	1.55	YES		2.14	
.3 444.13	3	441.22	0.16	0.16	YES	441.24	0.25	0.25	YES	441.26	0.38	
	0	303.2	0	374.13	ON	303.5	0	482.9	ON		0	
	4.5	357.95	1.38	1.38	YES	358.07	2.5	2.5	YES	358.21	4.09	
3 347.593	0 10	343.87	8.52	8.83	YES	344.65	15.3	16.2	YES	m	26.14	
	10	376.01	7.35	17.2	YES	376.39		31.15	YES	377.46	22.85	
8 386.778	3	385.93	0.22	0.26	YES	385.93	0.41	0.47	YES	385.94	99:0	
	3	379.79	0.11	0.11	YES	379.82		0.2	YES			
	C 0	377.63	0.75	0.86	YES	378.08	ij	1.79	YES		2.8	
3 403.981	0 4 5	404.16	76.0	0.26	YES	404.26	0 47	0.46	YES	404.89	92.0	
	0	312.62	0.27	515.98	NO	313.84	0	792.24	NO		0	
.6 445.346	3	442.62	3	3	YES	442.72	5.43	5.43	YES	442.83	9.28	
	3	417.24	0.18	0.18	YES	417.28	0.31	0.31	YES	417.31	0.5	
	3	436.64	0.1	0.1	YES	436.65	0.1		YES		0.2	
7 418.498	m L	411.92	0 0	0.27	YES	411.93	0	0.46	YES	411.93	0	
7 459.463	1.054	424.79	100	10.79	VES	423.30		13.14	VES		12.21 0 25	
	3.5	453.79	0.21	0.28	YES	453.8	0.35	0.46	YES		0.54	
2 452.592	0	452.61	0	0.27	YES	452.61	0	0.45	YES	7		
2 456.732	0	456.98	0	0.02	YES	456.98	0	0.04	YES	456.98	0	
	4.5	421.56	1.29	1.29	YES	421.65			YES			
.1 337.321	0	337.56	0.35	0.35	OZ	337.63	0.55	0.55	ON	337.71	0.85	
1 416.855	0	416.86	0	1.27	YES	416.89		2.31	YES			
	0	404.3	0	2.37	YES	404.32		4.32	YES			
7 439.355	0	439.58	1.38	1.38	YES	439.66	2.58	2.58	YES	439.75	4.35	
	2 003	446.33	0.78	0.72	VES	446.44	1.23	1.55	VES		2.01	
	0	404.63	0,0	0.84	YES	404.65	0	1.53	YES			
3 424.723	3	421.77	0.08	0.08	YES	421.78	0.1	0.12	YES		0.1	
	0	401.31	0.31	0.54	YES	401.37	0.63	1.08	YES	401.42	1.06	

Surcharging (2-year) HGL (10-) (Ë	isting (Existing Condition Junc	tions	Result	s Sum	Junctions Results Summary Table			
Max. Max Max					2-year				10-year				100-year
(4c) (2-) (2-) (2-) (1-) <th< th=""><th></th><th>May</th><th>ر ن</th><th>Max. Lateral Inflow</th><th>Max. Total Inflow</th><th>Surcharging</th><th>Max. HGL (10-</th><th>Max. Lateral Inflow</th><th>Max. Total Inflow</th><th>Surcharging</th><th>Max. HGL (100-year)</th><th>Max. Lateral Inflow</th><th>Max. Inf</th></th<>		May	ر ن	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL (10-	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL (100-year)	Max. Lateral Inflow	Max. Inf
0 0 YKS 4677 0 VKS 4627 0 0 0 YKS 4582.71 0 0 YKS 4637.11 0 0 0 0 0 0 0 YKS 463.71 0 0 0 0 0 0 0 YKS 463.71 0.45 37.68 YKS 463.21 0 0 YKS 443.82 1.0.1 50.2 YKS 419.18 0.73 YKS 4419.83 1.0.2 50.2 YKS 419.18 0.73 YKS 4419.83 1.0.2 1.0.3 1.0.4 0.0 YKS 4419.83 441.77 1.0.3 1.0.6 0.0 0 0.0 YKS 4419.83 1.0.6 1.0.6 0.0 0 0 0 0 0 1.0.8 1.0.6 0 0 0 0 0 0 0 0 <th>(reet)</th> <th>(fee</th> <th>ar) :t)</th> <th>(2- year) (cfs)</th> <th>(2- year) (cfs)</th> <th>(2-year)</th> <th>year) (feet)</th> <th>(10- year) (cfs)</th> <th>year)</th> <th>(10-year)</th> <th>(feet)</th> <th>(100-year) (cfs)</th> <th>(100-ye</th>	(reet)	(fee	ar) :t)	(2- year) (cfs)	(2- year) (cfs)	(2-year)	year) (feet)	(10- year) (cfs)	year)	(10-year)	(feet)	(100-year) (cfs)	(100-ye
0 VES 459.71 O VES 459.71 0 0 VES 459.71 O O VES 465.81 0 0 0 VES 465.81 O O VES 465.81 0.42 3.22 VES 465.81 O VES 465.81 465.81 1.30 3.248 VES 473.13 0.03 VES 473.72 421.12 1.17 51.28 VES 465.21 3.31 94.13 VES 440.23 421.13 <td< td=""><td>0</td><td></td><td>487</td><td></td><td></td><td>YES</td><td>487</td><td></td><td></td><td>YES</td><td>487</td><td>0</td><td></td></td<>	0		487			YES	487			YES	487	0	
0 VES 445841 0 0 VES 445841 0 0 VES 445841 0 0 VES 465841 0.25 2 VES 445181 0.78 6538 VES 46284 1.50 5.048 7 66.28 VES 46112 42.88 1.50 5.024 VES 4417.31 2.03 VES 4418.33 2.03 VES 4418.66 1.13 5.2.48 VES 4417.31 2.03 VES 4417.71 412.71 412.72 412.73 42.67 VES 4417.71 412.72 412.73	0	7	159.71	0	0	YES	459.71	0	0	YES	459.71		
0.2 2.2.2 YYES 445.84 0 VYES 445.84 0 VYES 445.84 0 VYES 421.82 421.82 1.5.01 5.03.2 YYES 449.18 0.78 66.88 YYES 421.82 1.5.01 5.5.2.8 YYES 449.13 0.78 66.83 YYES 421.82 1.1.1 5.5.2.8 YYES 449.23 2.03 YYES 440.33 1.7.6.3 1.7.6.3 1.7.6.3 3.4.13 YYES 440.33 YYES 440.33 1.7.6.4 1.7.6.3 YYES 416.21 3.3.1 YYES 440.33 1.7.6.4 1.7.6.3 YYES 460.21 YYES 430.33 YYES 440.33 1.7.7.6 1.7.6.3 YYES 430.62 YYES 434.89 YYES 434.89 1.7.7.7 YYES 440.62 7.26 2.26 YYES 434.89 1.7.7.7 YYES 434.90 7.26 2.26 YY		4	58.21	0	0	YES	458.21	0	0	YES	458.21	0	
0.45 3.72 YES 4.31 C.C. C.C. C.C. C.C. C.C. C.C. C.C. C.C. A.1.1.2 A.1.1.2 <td>0 7</td> <td>7</td> <td>165.84</td> <td>760</td> <td>0 0</td> <td>YES</td> <td>465.84</td> <td>0 16</td> <td>0</td> <td>YES</td> <td>465.84</td> <td></td> <td></td>	0 7	7	165.84	760	0 0	YES	465.84	0 16	0	YES	465.84		
15.01 50.22 YES 418.12 2.6.31 92.67 YES 419.83 1.83 52.48 YES 417.31 3.13 96.53 YES 417.71 1.83 52.48 YES 40.29 3.3 96.53 YES 430.3 1.75 3.16 YES 420.25 3.0 6.61.3 YES 430.3 1.73 3.16 YES 420.25 3.0 6.61.3 YES 420.23 0.93 0.93 YES 420.25 3.0 6.61.3 YES 420.23 0.93 0.93 YES 43.66 2.0 YES 424.99 0.93 0.93 YES 43.66 2.9 YES 424.99 0.94 YES 43.68 2.9 6.0 YES 43.99 0.95 YES 43.68 2.9 YES 43.99 YES 43.99 0.86 YES 43.71 4.18 4.1 YES		1 4	18.47	0.45	37.68	YES	421.11	0.78	69.88	YES	421.12		
123 512 YES 4133 203 943 YES 4186 1153 5248 YES 41621 331 96.53 YES 40177 1163 1753 YES 405.01 312.1 312.1 YES 403.3 1163 1375 YES 405.01 NO 324.33 78.1 1399 18.75 YES 405.64 72.6 32.30 YES 421.49 1399 18.75 YES 439.48 7.0 60.65 YES 421.49 1399 18.75 YES 439.48 7.0 60.65 YES 421.49 1399 18.75 YES 439.48 7.0 60.05 YES 434.93 1390 18.75 YES 434.88 7.0 0.0 YES 434.85 1390 18.26 XES YES 434.85 43.2 43.2 43.2 1390 18.26 XES YES		7	117.38	15.01	50.32	YES	418.12	26.91	92.67	YES	419.83	7	
188 52.48 YYE 416.71 3.31 96.53 YES 417.7 1.0 40.24 YYE 430.10 31.21 96.60 NO 324.13 1.0 420.35 NO 322.9 0 66.60 NO 324.13 1.1 3.16 YYE 420.55 3.29 YYE 421.58 1.0 1.3 1.36 YYE 420.55 3.2.39 YYE 421.58 1.0 1.36 YYE 430.20 YYE 420.59 421.58 421.58 1.0 1.36 YYE 430.20 YYE 433.93 72.34 421.58	12.361		116.59	1.21	51.2	YES	417.33	2.03	94.13	YES	418.96		
17.63 17.63 VYS 430.9 31.21 31.21 VYS 430.3 17.63 13.763 NO 32.24 NO 324.13 S 1.73 33.75 NYS 430.25 3.08 66.13 NYS 420.33 3.99 18.75 YYS 430.23 2.06 YYS 421.49 0.93 1.36 YYS 439.23 2.06 YYS 434.29 1.36 1.36 YYS 439.23 2.06 YYS 434.29 1.36 YYS 439.23 2.06 YYS 434.29 2.37 YYS 439.24 2.06 YYS 434.29 2.39 YYS 437.21 4.16 YYS 434.25 2.39 YYS 437.21 4.16 YYS 434.25 2.39 YYS 437.21 4.16 YYS 437.83 2.39 YYS 437.21 4.16 YYS 437.83 2.30	7	Ì	415.39	1.83	52.48	YES	416.21	3.31	96.53	YES	417.7	5.66	
1.73 3.34 VK 4.05.53 9.06.65 NO 324.13 3.99 1.87.5 VK 4.20.53 3.23 VKS 420.43 3.99 1.87.5 VKS 4.20.6 2.06 VKS 4.34.83 1.36 1.87.5 VKS 4.34.63 2.06 2.06 VKS 4.34.83 1.36 1.136 VKS 4.34.83 2.06 VKS 4.34.83 0.02 0.03 VKS 4.34.83 0.0 VKS 4.34.83 0.26 2.56 VKS 4.34.83 0.0 VKS 4.34.83 0.26 2.56 VKS 4.40.91 0.45 4.57 VKS 4.41.06 0.26 2.56 VKS 4.40.91 0.45 4.57 VKS 4.41.06 0.27 2.35 VKS 4.40.91 0.45 4.27 VKS 4.40.85 0.28 2.36 VKS 4.04.18 0.76 1.27 VKS 4.40.85<			430.1	17.63	17.63	YES	430.19	31.21	31.21		430.3	55.9	
3.99 18.75 YES 42.26 7.26 32.39 YES 42.26 0.93 18.75 YES 43.64 7.26 32.39 YES 43.92 1.36 YES 43.68 2.06 YES 43.48 43.75 0.03 YES 43.48 2.06 YES 43.48 43.75 0.26 2.56 YES 43.76 8.95 9.64 YES 43.48 0.26 2.56 YES 43.76 8.95 9.64 YES 43.75 0.26 2.56 YES 440.91 0.05 YES 43.75 0.27 2.46 2.26 YES 440.91 0.05 YES 43.75 0.28 2.56 YES 440.75 1.27 YES 443.89 0.8 0.0 YES 440.75 1.27 YES 443.89 0.8 0.0 YES 44.79 YES 440.78 440.78 <td< td=""><td>5.25</td><td></td><td>322.32</td><td>1 73</td><td>429.37</td><td>NO</td><td>322.9</td><td>3 08</td><td>606.05</td><td></td><td>324.13</td><td></td><td></td></td<>	5.25		322.32	1 73	429.37	NO	322.9	3 08	606.05		324.13		
0.93 0.93 VES 439.23 2.06 2.06 VES 439.37 1.36 1.36 1.36 VES 434.66 2.36 VES 434.99 0.0 0.03 VES 434.83 2.36 VES 434.93 2.35 2.4 VES 437.71 4.16 4.16 VES 437.83 2.35 2.4 VES 437.71 4.16 4.15 VES 437.83 2.35 2.4 VES 437.71 4.16 4.15 VES 437.83 2.35 2.38 VES 437.71 4.16 4.15 VES 437.83 0.5 1.39 VES 442.93 0.76 12.73 VES 443.06 0.6 0.7 VES 440.75 12.73 VES 440.18 7.24 0.7 0.8 VES 440.75 12.73 VES 440.18 7.24 0.8 0.7 VES 440.75			419.07	3.99	18.75	YES	419.64	7.26	32.39	YES	421.49	1	
1.36 1.36 YES 434.66 2.36 2.36 YES 434.99 4.97 4.97 YES 437.66 8.95 9.64 YES 437.71 4.97 4.97 YES 437.71 4.16 YES 437.73 2.35 2.36 YES 4.67 YES 441.06 2.35 2.36 YES 4.67 YES 441.06 2.35 2.36 YES 4.67 YES 441.06 2.35 2.36 YES 4.37 YES 443.68 0.5 11.36 YES 4.37 YES 441.06 0.5 11.36 YES 4.37 YES 443.68 0.0 N YES 4.34 N YES 4.34 0.0 N YES 4.34 N YES 4.40 N 0.0 N YES 4.34 N YES 4.40 N YES 4.40	0		439.11	0.93	0.93	YES	439.23	2.06	2.06		439.37		
0 0 0 0 0 0 434.85 2.35 2.49 YES 434.71 4.16 4.16 YES 437.7 2.35 2.4 YES 440.91 0.45 4.5 YES 441.06 2.35 2.35 YES 442.93 4.2 4.2 442.93 4.2 4.2 443.99 0.0 1.136 YES 442.93 4.2 4.2 4.2 443.99 443.99 443.99 443.99 443.99 443.89 440.18 440.01 4.2 4.2 441.06 443.99 440.18 <td>0.522</td> <td></td> <td>434.45</td> <td>1.36</td> <td>1.36</td> <td>YES</td> <td>434.66</td> <td>2.36</td> <td>2.36</td> <td></td> <td>434.99</td> <td></td> <td></td>	0.522		434.45	1.36	1.36	YES	434.66	2.36	2.36		434.99		
4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.97 4.16 YES 4.37 4.37 4.16 YES 4.37 4.39 4.37 4.39 4.37 4.39 4.39 4.33 4.30 4.39 4.39 4.30 4.39 4.30 4.39 4.30 4.39 4.30 4.30 4.39 4.41 4.39 4.30 4.41 4.39 4.41 4.41 4.41 4.41 4.41 4.41 4.41 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.42 4.43 4.43 4.43 4.43 4.43 4.43 4.43 4.43 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4.44 4	0		434.81	0	0.03	YES	434.83	0	0.02	YES	434.85		
2.35 2.4 YES 437.71 4.16 4.16 YES 447.83 2.36 2.56 YES 440.91 0.45 4.25 YES 441.06 2.35 2.35 YES 442.93 4.2 7.5 443.99 0.5 11.36 YES 440.91 0.76 12.73 YES 443.96 1.08 YES 440.78 0.76 12.73 YES 443.96 3 1.08 YES 440.75 19.29 YES 440.88 3 0.0 YES 479.02 6.11 6.82 YES 440.88 3 0.05 YES 479.02 6.11 6.82 YES 440.88 3 0.56 O.56 YES 479.02 6.11 6.73 YES 440.88 3 0.56 YES 479.02 6.11 6.73 YES 440.81 3 0.56 YES 479.02 6.11 10.2	0		437.63	4.97	4.97	YES	437.66	8.95	9.64	YES	437.7		
2.35 7.53 7.53 4.2. 3.4 4.2. 4.2. 4.2. 4.2. 4.2. 4.3.9 4	2 525		437.64	2.35	2.4	YES	437.71	4.16	4.16	YES	437.83		
0.5 11.36 YES 438.64 0.76 12.73 YES 449.65 10.89 10.89 YES 440.18 0.76 12.73 YES 440.48 10.89 10.89 YES 440.78 10.29 12.29 YES 440.48 10.89 YES 440.78 10.29 YES 440.85 3.3 0.6 3.7 YES 449.46 0.0 6.11 6.82 YES 440.85 0.56 0.56 VES 449.00 0.76 YES 449.04 0.57 YES 469.01 0 6.79 YES 469.04 0.56 VES 492.07 0 7.7 YES 482.73 0.58 VES 484.73 1.71 18.03 YES 488.1 0.59 VES 484.13 1.71 18.03 YES 488.1 13.93 16.77 YES 448.13 1.71 18.03 YES 432.1 </td <td>4.5</td> <td></td> <td>442 65</td> <td>2.52</td> <td>2:35</td> <td>VFS</td> <td>442 93</td> <td>CT:0</td> <td>4.2</td> <td>YES</td> <td>443 99</td> <td></td> <td></td>	4.5		442 65	2.52	2:35	VFS	442 93	CT:0	4.2	YES	443 99		
0 0 YES 404.18 0 0 YES 404.18 10.89 10.89 YES 440.75 19.29 19.29 YES 440.85 3.4 3.71 YES 440.75 19.29 19.29 YES 440.85 0.56 3.7 YES 499.46 0 0 YES 440.85 0.56 0.56 0.56 YES 492.07 1 1 YES 492.13 0.56 0.56 YES 492.07 1 1 YES 492.13 0.57 0.56 YES 434.07 0 7.7 YES 493.14 0.98 1.77 YES 434.07 0 7.7 YES 448.14 0.98 1.5.42 YES 434.07 0 7.7 YES 448.14 0.98 1.5.42 YES 448.15 7.7 YES 448.16 1.6.40 YES 448.15 7.7 <t< td=""><td>e c</td><td></td><td>437.85</td><td>0.5</td><td>11.36</td><td>YES</td><td>438.64</td><td>0.76</td><td>12.73</td><td>YES</td><td>439.6</td><td></td><td></td></t<>	e c		437.85	0.5	11.36	YES	438.64	0.76	12.73	YES	439.6		
10.89 10.89 VES 440.75 19.29 19.29 VES 440.85 0 0 VES 479.46 0.0 VFS 479.46 0 3.7 VES 479.02 6.11 6.82 VFS 489.27 0.56 0.56 VFS 492.07 0.1 1 VFS 469.04 0.56 0.56 VFS 492.07 0.1 7 VFS 492.07 0.57 0.59 VFS 492.07 0.0 6.0 492.03 492.07 0.05 5.59 VFS 492.07 0.0 7.7 VFS 492.13 0.07 4.05 VFS 438.75 0.0 7.7 VFS 438.41 0.08 4.05 7.7 7 VFS 449.93 7.7 VFS 443.15 0.09 0.0 VFS 449.95 7.7 7 VFS 424.21 1.3.9 0.0 VFS 441.15	0		404.18	0	0	YES	404.18	0	0	YES	404.18		
0 VES 479.46 0 0 VES 479.46 3.4 3.71 VES 479.02 6.11 6.82 VES 482.27 0.5 3.7 VES 469.01 0 6.79 VES 469.04 0.5 6.5 VES 469.07 1 C 492.13 492.13 0.0 4.05 VES 492.07 1 VES 434.14 <	3.5		440.02	10.89	10.89	YES	440.75	19.29	19.29	YES	440.85		
3.4 3.71 YES 479.02 6.11 6.82 YES 482.27 0.56 3.7 YES 469.01 0.79 YES 469.04 0.56 0.56 0.56 YES 492.07 1 1 7 469.04 0.56 0.56 YES 492.07 1 1 7 469.04 469.04 0.67 4.05 YES 438.75 0 7.7 YES 448.13 0.7 4.05 YES 448.13 1.71 18.03 YES 448.16 1.5.4 1.5.4 YES 448.13 1.71 18.03 YES 448.16 0.0 YES 448.13 1.71 18.03 YES 448.15 1.3.93 16.77 YES 448.45 0 YES 448.45 0 YES 411.45 25.01 25.02 YES 411.54 1.14 70.57 YES 411.54 21.87 YE	2.67		479.46	0	0	YES	479.46	0	0	YES	479.46	0	
0 3.7 YES 469.01 0 6.79 YES 469.04 0.56 0.56 YES 442.07 1 1 YES 492.13 0.56 0.56 YES 434.07 0 7.7 YES 434.14 0.08 1.77 YES 448.13 1.71 18.03 YES 438.81 1.5.42 1.5.42 YES 448.13 1.71 18.03 YES 438.81 0.08 YES 449.95 27.77 27.77 YES 448.16 13.43 16.77 YES 440.81 27.77 27.77 YES 448.45 13.53 16.77 YES 411.45 25.01 25.92 YES 408.45 13.53 16.77 YES 411.45 25.01 25.92 YES 411.64 2.7 XES 411.33 6.41 21.87 YES 411.64 3.0 YES 411.52 2.02 XES <td>4</td> <td></td> <td>478.74</td> <td>3.4</td> <td>3.71</td> <td>YES</td> <td>479.02</td> <td>6.11</td> <td>6.82</td> <td>YES</td> <td>482.27</td> <td>10.47</td> <td></td>	4		478.74	3.4	3.71	YES	479.02	6.11	6.82	YES	482.27	10.47	
0.56 0.56 YES 492.07 1 1 YES 492.13 0 5.59 YES 434.07 0 10.2 YES 434.14 0 4.05 YES 438.75 0 7.7 YES 448.16 15.42 15.51 YES 448.13 1.71 18.03 YES 448.16 15.42 15.51 YES 449.95 27.77 27.77 YES 448.16 15.42 15.51 YES 448.13 YES 448.16 488.16 13.93 16.77 YES 448.15 7.77 27.77 YES 448.16 13.93 16.77 YES 414.21 408.45 7.77 YES 448.45 13.93 16.77 YES 411.45 25.01 25.02 YES 411.64 13.93 16.74 YES 411.51 7.83 41.24 41.16 13.04 YES 411.53 6.43 2	0		468.96	0	3.7	YES	469.01	0	6.79	YES	469.04	0	
0 5.59 YES 434.07 0 10.2 YES 434.14 0.98 11.77 YES 438.75 0 7.7 YES 438.81 1.5.42 11.77 YES 448.13 1.71 18.03 YES 448.16 15.42 15.51 YES 449.95 27.77 27.77 YES 448.16 13.93 16.77 YES 449.95 27.77 27.77 YES 448.16 13.93 16.77 YES 449.95 27.77 27.77 YES 448.45 13.93 16.77 YES 411.45 25.01 YES 441.16 2.7 21.0 YES 411.54 411.54 411.54 2.7 21.0 YES 411.54 411.51 411.54 2.7 22.0 YES 411.54 411.54 411.54 3.0 YES 411.58 421.33 421.33 421.33 421.33 421.33 421.3	0		492.02	0.56	0.56	YES	492.07	1	1	YES	492.13	1.61	
0.98 4.05 YES 438.75 0 7.7 YES 438.81 0.98 11.77 YES 448.13 1.71 18.03 YES 448.16 15.42 15.51 YES 449.95 27.77 27.77 YES 450.07 0 0 YES 424.21 0 0 YES 424.21 13.93 16.77 YES 414.45 25.01 25.92 YES 411.64 2.7 21.6 YES 411.45 25.01 25.92 YES 411.64 2.7 21.6 YES 411.33 6.41 21.87 YES 411.51 2.7 21.6 YES 411.52 2.02 81.73 YES 412.14 3.07 30.01 YES 413.84 5.36 52.69 YES 404.96 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 6.22 81.03 YES	3.5		434.02	0	5.59	YES		0	10.2	YES	434.14	0	
0.98 11.77 YES 448.13 1.71 18.03 YES 448.16 15.42 15.51 YES 449.95 27.77 27.77 YES 448.16 0 YES 449.95 27.77 27.77 YES 450.07 0 YES 424.21 0 YES 424.21 13.93 16.77 YES 411.45 25.01 25.92 YES 411.64 13.93 16.77 YES 411.33 6.41 21.87 YES 411.64 2.7 21.6 YES 411.53 6.41 21.87 YES 411.51 3.07 30.01 YES 411.52 2.02 81.73 YES 414.16 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 6.24 3.07 YES 404.64 8.07 95.72 YES 404.96 6.25 81.03 YES 404.56 0.43	3.33		438.71	0	4.05	YES		0	7.7	YES	438.81		
15.42 15.41 15.42 15.47 27.77 27.77 YES 449.55 27.77 27.77 YES 420.07 0 0 0 0 YES 424.21 408.45 424.21 13.93 16.77 YES 411.45 25.01 25.92 YES 411.64 3.53 19.31 YES 411.33 6.41 21.87 YES 411.64 2.7 21.6 YES 411.58 4.72 24.31 YES 411.51 3.07 30.01 YES 411.52 2.02 81.73 YES 412.18 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 0.26 81.03 YES 404.56 0.43 87.85 YES 404.96 0.27 18.13 YES 425.13 0.35 32.45 425.46	0		448.1	0.98	11.77	YES	448.13	1.71	18.03	YES	448.16		
0 VES 424,21 O O VES 424,21 13,93 16,77 YES 411,45 25,01 25,92 YES 408,45 2,7 21,6 YES 411,45 25,01 25,92 YES 411,64 2,7 21,6 YES 411,58 4,72 24,31 YES 412,24 3,07 30,01 YES 411,52 2.02 81,73 YES 412,18 4,62 76,22 YES 404,64 8.07 95,72 YES 404,96 0,26 81,03 YES 404,56 0.43 87,85 YES 404,96 0,22 18,13 YES 404,56 0.43 87,85 YES 404,96 0,22 18,13 YES 404,56 0.43 87,85 YES 404,96 0,22 18,13 YES 425,13 0.35 32,45 YES 404,96	0 0		449.86	15.42	15.51	YES	449.95	71.17	71.17	YES	450.07		
13.93 16.77 YES 411.45 25.01 25.92 YES 411.64 3.53 19.31 YES 411.45 25.02 25.92 YES 411.51 2.7 21.6 YES 411.58 4.72 24.31 YES 411.51 1.14 70.57 YES 411.52 2.02 81.73 YES 412.18 3.07 30.01 YES 411.52 2.02 81.73 YES 414.16 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 0.26 81.03 YES 404.56 0.43 87.85 YES 404.96 0.27 18.13 YES 425.13 0.35 32.45 YES 425.46	0 0		424.21 408 45		0 0	VES	12.424		0 0	VES	424.21		
3.53 19.31 YES 411.33 6.41 21.87 YES 411.51 2.7 2.16 YES 411.58 4.72 24.31 YES 411.51 3.07 30.01 YES 411.52 2.02 81.73 YES 412.18 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 0.26 81.03 YES 404.56 0.43 87.85 YES 404.93 0.22 18.13 YES 425.13 0.35 32.45 YES 404.93	0 4		410 74	13 93	16 77	VEX	411.45	25.01	75 97	YES	411 64		
2.7 21.6 YES 411.58 4.72 24.31 YES 412.24 1.14 70.57 YES 411.52 2.02 81.73 YES 412.18 3.07 30.01 YES 413.84 5.36 95.72 YES 414.16 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 0.26 81.03 YES 404.56 0.43 87.85 YES 404.93 0.22 18.13 YES 425.13 0.35 32.45 YES 425.46	4.59		410.21	3.53	19.31	YES	411.33	6.41	21.87	YES	411.51	11.34	
1.14 70.57 YES 411.52 2.02 81.73 YES 412.18 3.07 3.07 30.01 YES 413.84 5.36 52.69 YES 414.16 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 0.26 81.03 YES 404.56 0.43 87.85 YES 404.93 0.22 18.103 YES 425.13 0.35 32.45 YES 425.46	5.362		409.01	2.7	21.6	YES	411.58	4.72	24.31	YES	412.24		
3.07 30.01 YES 413.84 5.36 52.69 YES 414.16 4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 0.26 81.03 YES 404.56 0.43 87.85 YES 404.93 0.22 18.13 YES 425.13 0.35 32.45 YES 425.46	9		408.46	1.14	70.57	YES	411.52	2.02	81.73	YES	412.18		
4.62 76.22 YES 404.64 8.07 95.72 YES 404.96 0.26 81.03 YES 404.56 0.43 87.85 YES 404.93 0.22 18.13 YES 425.13 0.35 32.45 YES 425.46	9		409.67	3.07	30.01	YES	413.84	5.36	52.69	YES	414.16	8.71	
0.26 81.03 YES 404.56 0.43 87.85 YES 404.93 0.22 18.13 YES 425.13 0.35 32.45 YES 425.46	6.5		404.09	4.62	76.22	YES	404.64	8.07	95.72	YES	404.96		
0.22 18.13 YES 425.13 0.35 32.45 YES 425.46	7		403.91	0.26	81.03	YES	404.56	0.43	87.85	YES	404.93		
	9		424.9	0.22	18.13	YES	425.13	0.35	32.45	YES	425.46	0.53	

			FX	isting (Existing Condition ling	linctions	Recult	Silm	Recults Summary Table			
pucione				2-vear			1	10-vear				100-vea
CIIOICIIS				z-yeai			- 1	U-year				-טט-אבמ
Rim	Depth	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL	Max. Lateral	Max
(feet)	(feet)	(2-year) (feet)	(2- year) (cfs)	(2- year) (cfs)	(2-year)	year) (feet)	(10- year) (cfs)	(10- year) (cfs)	(10-year)	(feet)	(100-year) (cfs)	(100-ye
2 424.362	9	419.91	7.64	24.53	YES	420.51	13.14	41.43	YES	421.44	21.72	
424.22	9 (419.16	0.0	25.33	YES	419.46	1.59	44.1	YES	420.27	2.67	
	2.5	430.00	2.19	16.42	YES	451.11	3.68	27.6	YES	431.47		
	9	432.83	13.15	13.15	YES	433.02	23.59	23.59	YES	433.27	7	
443.024	3	442.17	0.29	0.29	YES	442.18	0.44	0.44	YES	442.18	0.67	
3 439.703	0	439.82	0.22	0.22	YES	439.84	0.35	0.35	YES	439.87	0.5	
	0 1	437.68	0	0.24	YES	437.69	0 10	0.36	YES			
470.031	9.5	461.33	0.16	9.49	YES	461.33	0.27	9.65	YES		0.42	
	3.5	452.37	1.62	16.68	YES	452.5I	m c	15.52 77 A	YES	452.59	2.6	
3 453.3	0 4	263.30 454 04	0 28 2	11 92	VEC	454.23	7 0	77 97	VES	263.01	0 17 78	
46	4.5	469.15	0.18	12.35	YES	469.4	0.27	15.25	YES	469.48	0.42	
	4.5	465.75	0.21	12.41	YES	465.76	0.32	13.04	YES	465.77	0.5	
7 470.307	4.5	471.67	11.21	19.32	YES	471.72	20.09	28.87	YES	471.8	35.2	
	3	505.67	0	0	YES	202.67	0	0	YES	505.67	0	
	3.709	202	0	0	YES	202	0	0	YES	502		
	0	510.1	0	0	YES	510.1	0	0	YES			
	0	486.59	0	0	YES	486.59	0	0	YES		0	
	4	502.39	2.1	2.17	YES	502.59	3.88	3.88	YES	502.9	6.5	
373.308	0 1	373.69	0 0	1.95	YES	373.7	0 0	3.25	YES	3/3.72		
3 493.173	4.5	494.3	1.73	7.41	YES	494.00	3.12	11.7	YES	498.74	5.33	
1 488.751	4.5	485.49	3.73	10.99	YES	488.94	6.75	16.95	YES	489.2	11.81	
.5 478.345	4.5	479.05	2.5	13.33	YES	479.31	4.1	12.19	YES	479.45	6.42	
7 436.677	2	434.68	0	0	YES	434.68	0	0	YES	434.68	0	
	3	509.28		0.13	YES	509.3	0.23	0.23	YES			
4	Ω !	415.8	6.23	6.42	YES	415.96	11.03	11.37	YES	416.19	18.39	
	2.75	408.8	1.46	12.83	YES	411.94	2.23	23.57	YES	412.31	3.39	
414.29	3.09	411.94	4.8	4.94	YES	413.58	8.12	17.7/	YES	415.78	13.94	
		405.78	2.49	15.03	YES	405.56	4.18	24.08	YFS	405.39		
		401.79	8.72	48.24	YES	402.05	15.35	59.67	YES	402.44		
399.884	4.264	401.04	0.41	106.68	YES	401.98	0.65	107.04	YES	402.36	1.02	
	5.631	401.02	3.02	149.96	YES	401.98	4.73	153.34	YES	402.35		
402.342	9.802	395.17	0.51	143.72	YES	395.61	0.81	152.11	YES	395.83	1.29	
4 402.531	12.291	395.01	3.55	144.75	YES	395.45	5.69	153.3	YES	395.67	9.05	
.1 447.011	4.5	442.86	2.5	3.12	YES	442.96	4.14	5.19	YES	443.08	92'9	
8 447.108	4.5	443	0.63	0.63	YES	443.11	1.06	1.06	YES	443.23	1.67	
	4.5	441.08	0.28	3.41	YES	441.15	0.48	2.67	YES	441.23		
3 438.023	6.5	434.24		85.61	YES	434.4	8.31	91.68	YES	434.55	13.21	

2.69 2.74 0.65 17.97 1.36 17.1 10.13 0.17 25.32 13.45 11.06 37.95 29.85 29.85 11.84 7.9 7.9 7.9 7.9 7.9 7.9 7.9 7.9		0.05 0.05 0.05 0.05 0.13 0.17 0.13 0.17 0.18 11.06 8.36 8.36 8.36 11.06 0.72 11.06 0.72 0.72 11.06 0.72 0.72 11.06 0.72 0.72 0.74 0	445.48 2.69 445.36 0.05 446.38 0.05 434.52 0 434.52 0 45.8 7.37 457.03 0.13 440.36 0.17 441.08 9.86 435.4 0.72 435.4 7.48 435.4 7.48 435.4 7.48 435.4 7.48 435.4 7.48 437.69 4.47 448.23 0 447.82 0 453.02 6.14 430.83 6.14
	6.14 YES 453.1 10.77 1 0.73 YES 432.26 0.98 4.07 YES 434.31 6.85 7.52 YES 431.85 13	6.14 6.14 6.14 YES 453.1 10.77 0.54 0.73 YES 432.26 0.98 4.07 4.07 YES 434.31 6.85 7.52 7.52 YES 431.85 13	453.02 6.14 6.14 6.14 7ES 453.1 10.77 1 430.83 0.54 0.73 YES 432.26 0.98 0.98 434.13 4.07 4.07 4.07 6.85 6.85 6.85 431.72 7.52 7.52 7.52 13 13
YES 445.87 YES 445.87 YES 445.87 YES 445.24 YES 456.48 11 YES 456.48 11 YES 457.32 YES 440.68 YES 435.61 YES 435.61 YES 435.62 11 YES 438.14 YES 438.14 YES 448.23 YES 443.31 YES 434.31 YES 434.31 YES 434.31 YES 434.31	2.09 YES 440.47 2.74 YES 445.87 0.65 YES 445.87 17.97 YES 448.72 17.1 YES 450.2 10.13 YES 456.48 1 10.13 YES 457.32 1 0.17 YES 440.68 1 13.45 YES 435.61 1 11.06 YES 435.62 1 11.84 YES 435.62 1 29.85 YES 438.09 2 11.84 YES 438.09 2 7.9 YES 448.23 0 0 YES 448.23 0 0 YES 448.23 1 0 YES 454.58 1 0 YES 454.58 1 0 YES 454.58 1 0 YES 454.31 1 0 YES 434.31 1 0 YES 434.31 1	0.05 2.73 4.6.74 0.05 2.74 YES 445.87 0.05 0.65 YES 448.72 0.06 0.06 448.72 448.72 0.07 1.36 YES 450.2 0.13 YES 456.48 1 0.13 10.13 YES 456.48 1 0.14 0.17 YES 456.48 1 0.17 0.17 YES 440.68 1 0.17 0.17 YES 440.68 1 0.72 13.45 YES 435.61 1 11.06 11.06 YES 435.61 1 11.84 11.84 YES 435.62 1 11.84 11.84 YES 438.09 1 0 7.9 YES 448.23 1 0 0 YES 448.23 1 0.54 0.73 YES 454.58 1 0.	443.46 2.03 2.03 7.03 7.03 445.36 0.05 2.74 YES 445.47 446.38 0.05 2.74 YES 445.47 446.98 1.05 17.97 YES 445.48 446.98 1.05 17.36 YES 435.48 1 457.03 0.13 10.13 YES 445.48 1 457.03 0.17 0.17 YES 445.48 1 440.36 0.17 0.17 YES 440.68 1 435.43 8.36 25.32 YES 435.41 1 435.43 8.36 25.32 YES 435.61 1 435.43 8.36 25.32 YES 435.61 1 435.43 8.36 37.95 YES 435.61 1 435.43 11.84 YES 438.22 2 437.69 4.47 31.86 YES 436.28 448.23
YES YES	2.09 YES 2.74 YES 0.65 YES 17.97 YES 13.6 YES 10.13 YES 25.32 YES 13.45 YES 13.6 YES 29.85 YES 29.85 YES 29.85 YES 11.84 YES 29.85 YES 11.84 YES 10 YES 11.02 YES 6.14 YES 4.07 YES 7.52 YES	0.05 2.74 YES 0.05 2.74 YES 0.05 0.65 YES 0.06 0.07 YES 0.136 YES 0.13 YES 0.14 YES 0.15 YES 0.16 YES 0.17 YES 0.72 13.45 YES 11.06 11.06 YES 11.84 11.84 YES 0 0 YES 4.47 31.86 YES 0	445.48 2.69 2.69 YES 445.36 0.05 2.74 YES 446.3 0.65 0.65 YES 446.38 1.05 1.36 YES 434.52 0 1.36 YES 434.53 0.13 10.13 YES 457.03 0.13 10.13 YES 440.36 0.17 YES YES 440.36 0.17 0.17 YES 435.4 0.72 13.45 YES 435.43 8.36 37.95 YES 435.43 8.36 37.95 YES 435.43 8.36 37.95 YES 435.49 1.1.84 YES 437.69 4.47 31.86 YES 448.23 0 0 YES 447.82 0 0 YES 447.82 0.10 0 YES 430.83 0.54 0.73 YES 431.7
	2.03 2.74 0.65 17.97 1.36 17.1 10.13 0.17 25.32 13.45 11.06 37.95 29.85 11.84 7.9 0 0 0 0 1.02 6.14 6.14	0.05 2.74 0.05 2.74 0.05 1.36 0.05 1.36 0.13 10.13 0.17 0.17 0.17 0.17 0.17 0.17 0.18 29.85 11.84 11.84 0 7.9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	445.48 2.69 2.09 445.36 0.05 2.74 446.3 0.65 0.65 446.98 1.05 17.97 434.52 0 1.36 457.03 0.13 10.13 440.36 0.17 0.17 441.08 9.86 25.32 435.4 0.72 13.45 439.69 11.06 11.06 435.43 8.36 37.95 438.07 11.84 11.84 387.86 0 7.9 448.23 0 0 447.82 0 0 447.82 0 0 447.82 0 0 447.82 0 0 447.82 0 0 447.83 0.74 0.73 430.83 0.54 0.73 431.72 7.52 7.52
2.69 2.74 0.05 17.97 1.36 1.36 10.13 0.17 25.32 25.32 25.32 25.32 11.06 37.95 29.85 29.85 11.84 7.99 0 0 0 0 0 0.73 7.52		0.05 0.05 0.05 0.03 0.13 0.17 0.17 0.72 11.06 8.36 8.36 7.48 11.84 0 0 0 0 0 0 1.02 6.14 6.14 6.14 6.14	445.48 2.69 445.36 0.05 446.3 0.65 446.98 1.05 434.52 0 457.03 0.13 440.36 0.17 440.36 0.17 435.4 0.72 435.43 8.36 435.43 8.36 435.43 447 448.23 0 447.82 0 447.82 0 447.82 0 447.82 0 447.82 0 430.83 0.54 430.83 0.54 431.72 7.52
	0.65 1.05 0.03 0.13 0.13 0.17 0.17 1.06 8.36 8.36 8.36 8.36 1.1.84 0 0 0 0 0 1.02 0 0 0 0 0 0 0 0 0 0 0 0 0		446.3 446.98 434.52 455.8 457.03 440.36 441.08 435.43 435.43 435.43 435.43 435.43 437.69 447.82 447.83 447.83 447.83 447.83 447.83 447.83 447.83

							1					
			EX	isting	Existing Condition Junctions Results Summary Table	ctions	Result	s Sum	mary Table	a)		
ensions				2-year			1	10-year			1	100-year
Rim Elevation	Depth	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging (2-year)	Max. HGL (10-	Max. Lateral Inflow	Max. Total Inflow	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	Max. Infl
(feet)		(feet)	year) (cfs)	year)		year) (feet)	year) (cfs)	year) (cfs)		(feet)	(100-year) (cfs)	(100-уе
2 441.72	5	437.77	92.0	17.28	YES	438.13	1.25	26.7	YES	439.68	2.04	
47	4.5	441.58	2.6	2.6	YES	444.78	4.57	4.57	YES	445.18	7.44	
5 444.5	5	441.53	0.21	12.21	YES	444.65	0.33	19.78	YES	444.89	0.51	
450.064	5	446.07	6.53	9.68	YES		11.72	16.85	YES	450.23	20.09	
	4.299	447.05	3.21	3.21	YES		5.78	5.78	YES	451.24	10.04	
401.528	0	401.64	8.44	8.44	YES	401.98	14.12	14.12	YES	402.36	22.9	
1 458.571	3.5	455.84	1.51	1.51	YES		2.66	2.66	YES	457.83	4.44	
5 459.083	4.583	455.71	0.92	3.02	YES	456.21	1.66	5.39	YES	456.99	2.73	
5 457.025	2	457.48	5.64	5.64	YES	457.53	76.6	9.97	YES	457.59	17.08	
	3	454.33	4.02	6.62	YES	454.39	7.23	13	YES	454.45	12.57	
		439.48	3.71	3.71	YES		6.73	6.73	YES	439.64	11.67	
5 440.895	9	434.46	0.06	0.06	YES	434.48	0.09	0.00	YES	434.5	0.15	
	0 0	443.03	4.32	3.48	VES	7445.37 737 06	16.7	6.71	VEC	444.41	13.00	
		497.31	0 0	0.32	Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z		0 0	0.56	VES	438.02		
1 464.611		464.72	0.28	0.28	YES	7	0.46	0.36	YES	464.78	0.7	
	0	455.1	0	0.27	YES		0	0.44	YES	455.12		
	0	461.3	1.52	1.52	YES		2.86	2.86	YES	461.35	4.73	
5 451.022	2.872	450.07	2.72	3.28	YES	450.94	4.83	4.95	YES	451.06	8.12	
	2.501	450.08	0.58	0.58	YES		0.99	0.99	YES	450.98	1.61	
448.928	3.5	449.6	3.71	7.82	YES	449.73	6.55	9.99	YES	449.81	11	
		449.77	90.7	7 0.7	VES		12.34	12.34	VEC	443.9	0.00	
	3.87	445.86	1.67	10.29	YFS		2.91	17.19	YES	449.39	4.94	
		448.43	0.94	7.44	YES		1.67	13.96	YES	448.68	2.75	
1 491.421	0	491.57	0	1.78	YES	491.61	0	2.96	YES	491.66	0	
.8 450.128	3.5	447.07	2.37	2.37	YES	448.56	4.09	4.09	YES	450.05	6.83	
		442.9	0	1.69	YES	442.99	0	2	YES	443.09	0	
6 447.356		448.46	0	2.09	YES	448.64	0	4.12	YES	448.83	0	
	3.5	432.41	0 10	0 10	YES	432.41	0 0	0 ,	YES	432.41	0 0	
	n c	416.59	2.85	7.85	YES	416.63	4.81	4.81	YES	416.68	1./3	
	0	459.84	5.60	5.95	YES		10.74	10.74	YES	459.9	19.15	
7 450.207	0 0	450.3	0.22	0.42	YES	450.32	0.36	0.35	YES	450.34	0.57	
	o c	464.62	† 0	0.4	VEC	760.52	4,.0	0.07	VEC	404.03	T:T	
7 447.867	3.5	445.2	4.89	4.89	YES		8.78	8.79	YES	446.31	14.51	
468.354	5.5	464.5	2.42	36.19	YES	468.51	3.88	65.06	YES	468.7	6.15	
6 449.976	4.25	445.87	0.49	0.49	YES	445.91	0.82	0.82	YES	445.96	1.29	
.5 434.445	5	430.82	8.25	18.58	YES	435.11	14.7	30.25	YES	435.29	26.53	
3 434.883	5	431.09	9.86	10.34	YES	435.45	17.56	18.37	YES	435.73	31.53	

	100-year	Max.	Int (100-ye																																			
		Max. Lateral	Inflow (100-year) (cfs)	12.07	0		1.4	10.24	13.44		8.06		0.71		1.14	98.12		5.86	27.79		8.3	0	19.3			15.06	7.5			0	17.8		8.2		9.05			3.7
a)		Max. HGL	(100-year) (feet)	408.41	433.52	376.35	391.67	392.08	345.31	358.29	404.67	376.19	350.33	336.32	335.77	335.98	335.46	336.04	335.7	335.92	335.54	3302	368.27	368.2	419.5	382.83	400.45	401.99	421.07	389.14	383.86	382.33	378.05	454.55	378.11	377.16	363.65	395.57
mary Table		Surcharging	(10-year)	YES			YES	YES		YES	YES		YES	ON	ON 2		ON	NO	ON		ON	YES			YES	YES	YES			YES	YES			YES	YES			YES
s Sum	10-year	Max. Total Inflow	(10- year)			(1)	0.92	31.43			43.27		0.45			10.40	36	117.4	64.47		370.9	0	13.7			9	4.52			0	265.11				5.5			2.26
Results Summary	1	Max. Lateral Inflow	(10- year)	7.21	0	7.18	0.92	6.16	8.01	11.29	0.19	0	0.45	2.25	0.72	10.01	0.48	3.26	16.21	17.29	5.19	0	11.14	5.51	4.49	8.79	4.52	9.05	1.07	0	10.97	2.04	4.86	0 1	7.87	5.99	4.72	2.26
Junctions		Max. HGL	(10- year) (feet)	408.04	433.52	372.19	391.67	391.79	342.66	357.95	404.64	376.18	350.31	334.71	335.08	333.04	334.65	335.19	335.13	335.2	334.89	399	368.12	368.08	419.35	382.49	400.28	401.29	421	388.85	381.7	381.32	376.46	454.48	376.33	375.98	362.61	394.29
Existing Condition Junc		Surcharging	(2-year)	YES	YES	YES	YES	YES	NO	YES	YES	YES	YES	ON	ON	ON	ON	ON	ON	ON	ON	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES
isting	2-year	Max. Total Inflow	(2- year)	37.47	0	21.31	0.61	17.35	33.06	28.7	0.12	0.12	0.28	175.91	29.02	9.34	121.03	75.84	40.38	112.23	352.62	0 0	9.22	3.1	2.83	54.27	2.55	41.86	0.65	0	156.87	1.19	2.75	0.72	3.29	10.58	2.88	1.28
EX		Max. Lateral Inflow	(2- year)	3.99	0	4 6	0.61	3.38	4.79	6.25	0.12	0	0.28	1.33	0.45	9.00	0.31	1.86	9.41	10.28	3.07	0	6.24	3.1	2.83	4.89	2.55	4.89	0.65	0	6.57	1.19	2.75	0	3.29	3.43	2.88	1.28
		Max. HGL	(2-year) (feet)	407.73	433.52	371.47	391.67	391.55	341.98	357.61	404.62	376.18	350.29	329.01	330.93	321.73	329.17	330.73	334.76	334.76	331.06	399	367.89	367.9	419.24	378.49	400.13	400.93	420.95	388.85	380.4	381.25	374.55	454.42	370.24	374.39	361.62	393.99
		Depth		7.139	0	8.5	0	9	4.5	5.5	5.5	0	4	6	0 1	6.7 6.75	6	6	1.809	4.5	∞ ′	0 0	0 4	4	0	5.5	4.5	5.087	3	3.5	6		4	0	7 2	2 2	2	1.869
	ensions	Rim	Elevation (feet)	6 413.699			393.886	8 396.88			4 408.524		6 354.206			333.274		5 333.895	332.109		333,	399					404.231		7	.8 392.348	1 386.131				8 377.128			3 395.169

			FX	isting	Existing Condition lunc	tions	Result	Sum	lunctions Besults Summary Table			
ensions				2-vear			10	10-vear				100-vear
Rim Elevation	Depth	Max. HGL	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL (10-	Max. Lateral Inflow	Max. Total Inflow	Surcharging	Max. HGL (100-year)	Max. Lateral Inflow	Max.
(feet)	(leer)	(feet)	year) (cfs)	year) (cfs)	(z-year)	year) (feet)	year) (cfs)	year) (cfs)	(10-year)	(feet)	(100-year) (cfs)	(100-уе
.2 432.672	2.83	429.84	0	0	YES	429.84	0	0	YES	429.84	0	
429.564	m d	429.62	0.67	79.0	YES	429.64	1.15	1.15		429.67	1.86	
5 430.595	2 0 0 0	429.62	0 66	0.16	YES	429.64	0 7 7	0.02	YES	429.67	1 96	
	3.33	428.47	2.59	3.21	YES	430.21	4.61	5.78		430.24	7.94	
1 427.304	0.594	426.81	0	3.07	YES	426.83	0	4.52		426.84	0	
	0	438.7	1.11	1.11	YES	438.78	1.94	1.94	YES	438.87	3.14	
7	4.5	430.54	3.62	6.57	YES	430.91	6.48	13.01		435.62	11.48	
7 411.97	4.5	407.77	1.01	1.01	YES	408.09	1.59	1.59	YES	408.44	2.51	
	2.07	414.87	117	1 17	YES	415.1	1 84	1 8/1		415.33	3.62	
	4.5	392.84	5.47	7.39	YES	397.18	9.14	24.48		397.59	15.34	
		396.81	8.42	25.41	YES	397.22	14.05	57.76		397.59		
	9.812	386.79	0.45	236.79	YES	387.8	0.71	444.63	YES	390.31	1.11	
1 396.401	5	391.74	0.16	4.17	YES	392.06	0.25	15.71	YES	392.76	0.39	
	5	392.02	0.64	1.05	YES	392.06	1.05	1.6		392.14	1.7	
985.206	9.5	378.67	2.35	240.91	YES	380.04	3.83	453.76	YES	383.38	6.13	
	18.016	379.83	9.64	65.27	YES	380.9	16.3	133		384.39	27.58	
	9	385.33	0.4	48.51	YES	385.38	0.63	85.11		385.44	0.97	
	ω <	377.09	3.88	51.03	YES	377.99	6.4	49.99	YES	378.89	10.45	
378.011	4 0	376.00	17.7	36.54	YES	9/5	1.99	32.93	YES	379.34	3.1	
8 379.258	0 10	376.82	10.42	41.01	YES	377.91	17.1	49.56		378.81	27.92	
	0	376.72	3.56	242.17	YES	377.86	6.03	470.59	YES	378.76	96.6	
7 380.507	6	373.22	3.36	63.29	YES	373.76	5.37	106.53	YES	374.83	8.52	
	8.746	360.73	2.93	109.85	YES	361.83	4.89	200.16		369.27	8.09	
	∞	363.97	5.6	81.39	YES	364.89	9.33	152.78		370.58	15.43	
5 363.095	0 1	363.78	0	3.18	YES	364.1	0	5.22	YES	364.53	0	
9 256 029	U II	251 43	0 0	12.11	YES	419.64	0 64 0	50.72		429.08	10,	
3 352.053	9	349.62	2.96	11.68	YES	351.54	4.87	21.22		352.81	7.95	
	2	349.63	5.88	90.6	YES	351.53	9.58	14.9		353.2	15.5	
4 348.189	4.189	344.42	8.04	8.04	YES	344.7	13.82	13.83	YES	348.13	24.79	
9372.266	5.5	367.72	2.69	29.26	YES	368.05	4.47	49.27	YES	369.1	7.33	
.6 359.345	7.185	353.81	4.38	33.39	YES	358.72	7.11	75.8	YES	360.52	11.42	
7 359.394	7.724	353.64	2.41	58.46	YES	358.7	3.98	129.04	YES	360.65	6.5	
5 375.755	9	370.73	1.77	26.5	YES	371.04	2.95	44.68	YES	371.5	4.85	
	4.612	367.04	3.2	3.2	YES	367.2	5.25	5.25	YES	367.4	8.51	
.6 364.556	6.5	329.06	0.22	24.16	YES		0.33	32.97	YES	359.39	0.49	
	Ŋ	421.16	14.18	14.18	YES		25.52	25.52		431.22	43.31	
3 341.436	5.136	342.37	1.91	136.11	ON	343.19	3.03	230.79	YES	344.99	4.8	

					'							
			ΓX	Isting	EXISTING Condition June	unctions		s Sum	Results Summary Lable	a)		
ensions				2-year			1	10-year			1	100-year
i		Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total				
Kim Elevation	Depth (feet)	HGL (2-vear)	Inflow (2-	Inflow (2-	Surcharging (2-vear)	HGL (10-	Inflow (10-	Inflow (10-	Surcharging (10-vear)	(100-year)	Max. Lateral Inflow	Max. Infl
(feet)		(feet)	year) (cfs)	year) (cfs)		year) (feet)	year) (cfs)	year) (cfs)		(feet)	(100-year) (cfs)	(100-ye
951.106	0	351.11	0	0	YES	351.11	0	0	YES	351.42	0	
	24	420.55	0.24	9.19	YES	420.72	0.37					
	က	417.96	0.24	9.3	YES	417.99	0.36				0.55	
6 451.91	0	400.34	0.23	4.94	YES	402.55	0.35	18.79	YES	403.80	0.54	
	4.75	418.43	10.59	10.59	YES	418.73	18.53	18	YES	424.26	31.83	
397.005	4.5	397.32	3.26	39.5	YES	397.88	5.39	113.68	YES	398.31	8.77	
1 401.341	7.75	401.4	7.79	46.63	YES	401.79	13.15		YES		22.08	
8 402.658	7.95	402.31	0.3	113.4	YES	402.99	0.49	136.63	YES	403.24	6.70	
	2 4 5	403.03	2.51	10 31	VES	403.07	5.63				0.30	
	4.5	417.03	6.59	6:59	YES	418.18	11.43				19.08	
.5 406.25	4	406.63	0.94	1.79	YES	406.79	1.5	1.5	YES		2.38	
	2	406.6	8.43	25.33	YES	406.76	14.25				24.18	
	. 2	406.66	5.84	34.87	YES	406.85	9.69			407.04	15.98	
9 407.859	4.5	408.61	22.64	22.64	YES	408.68	39.86	39.86	YES	408.77	72.26	
	С. , д	407.87	7.00	7.7	VES	407.00		21.00			28.62	
	5.5	413.32	2.99	15.51	YES	416.34	5.38			420.03	9.43	
	5	411.71	5.5	20.95	YES	411.86	9.26			411.94	15.44	
5 409.905	4.5	410.68	1.47	30.64	YES	411.06	2.4	65.98	YES	411.34	3.88	
	4.5	413.17	1.33	10.05	YES	414.88	2.21		YES		3.57	
4 419.934 2 417.722	4.5	417.79	14.86	4.59	YES	419.93	76.35	76.84	YES	420.15	13.15	
	4.034	409.77	3.34	35.11	YES	409.83	5.58				9.13	
8 410.315	5.535	409.33	0.95	34.12	YES	409.53	1.54	33.81	YES	409.63	2.46	
	4.863	412.06	4.15	91.95	YES	412.08	7.02			412.1	11.52	
	5.479	416.62	0.78	61.04	YES	416.74	1.25				1.96	
	0 10	416.8	1.23	08.88	YES	416.92	2.04		YES	7	3.31	
416.282	4.25	410.58	3.42	67.18	YES	416.69	5.59	112.44		416.8	8.76	
	9	423.85	0.34	67.79	YES	424.5	0.55				0.87	
	4	422.41	0.63	0.63	YES	422.46	1.01		YES	422.53	1.59	
	5.5	428.37	3.93	3.93	YES	428.47	6.53		YES	429.37	10.51	
5 355.168	0	354.87	1.04	10.75	YES	355.04	1.82	20.55	YES	355.21	2.91	
	6.463	416.98	8.79	60.81	YES	417.39	14.81		YES	417.81	24.34	
416.672		417.25	1.31	58.64	YES	417.94	2.14		YES	418.37	3.44	
	6.24	419.62	1.06	54.36	YES	419.97	1.76	ω	YES	421.43	2.83	
	0	431.14	0.91	0.91	YES	431.21	1.47			431.58	2.31	
		421.11	0.96	0.96	YES	421.17	1.52	1.5		421.31	7:37	
/70.724	0	422.03	0	0	YES	422.03	0 10	0 10	YES	422.03	0	

	100-year	Max. Inf (100-ye																																			
		Max. Lateral Inflow (100-year) (cfs)	12.33	4.05	3.8					0	12.7		0				25.1																			0	0
a		Max. HGL (100-year) (feet)	432.46	435.36	323.71	322.9	304.38	432.97	431.51	427.34			436.32	334.52	431.89			398.34	446.92		419.34			451.88	463.54		(,,	345.58	369.6	366.87	356.59	456.25	429.84			407.16	420.25
mary Table		Surcharging (10-year)	YES	YES	ON	ON		YES	YES	YES			YES			YES			YES						YES			YES	YES				YES			YES	YES
s Sum	10-year	Max. Total Inflow (10- year) (cfs)	11.48	27.91				9.35			(1)		5.09	25			,		86.01	(1)	12.04		12.04		6.86	1		9.75	34.32		31.11		7.37	39.4	67.57	79.64	32.36
Results Summary	1	Max. Lateral Inflow (10- year) (cfs)	7.33	2.56	2.45	4.9	0	o c	0	0	7.51	0		0	0	0	14.67	0	0 0		0	0	0	0	0		0	0	0	0	0			0	0	0	0
Junctions		Max. HGL (10- year) (feet)	430.08	430.04	323.47	322.78	304.11	432.72	431.26	426.89	424.34	432.83	774.75	333.79	431.65	426.41	330.98	396.38	446.81	399.35	418.93	427.49	416.43	451.73	463.37	474.42	378.74	345.36	369.27	364.41	352.3	455.51	429.74	352.75	413.7	406.75	419.79
Existing Condition June		Surcharging (2-year)	YES	YES	ON	ON	ON 2	YES	YES	YES	YES	YES	YES	ON	YES	YES	ON	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES	YES
isting	2-year	Max. Total Inflow (2- year) (cfs)	6.19	15.55	3	90.9	26.77	5.24	5.43	16.34	23.14	2.56	3.02	462.21	4.05	4.53	8.44	4.52	84.31	24.01	7.55	6.84	7.55	5.28	4.32	56.16	2.78	5.64	19.39	17.2	17.19	5.57	1.36	1.34	46.04	68.69	18.07
Ex		Max. Lateral Inflow (2- year) (cfs)	4.14	1.59	1.54	2.85	0	0	0	0	4.23	0	0 0	0	0	0	8.44	0	0 0	0	0	0	0	0	0	0 0	0	0	0	0	0	0	0 0	0	0	0	0
		Max. HGL (2-year) (feet)	429.85	429.45	323.25	322.68	303.79	432.54	431.08	426.56	424.1	432.72	773.67	328.93	431.45	426.32	330.75	396.25	446.62	399.17	418.71	427.3	416.24	451.62	463.24	474.33	378.67	345.2	369.04	364.06	351.86	451.66	429.66	352.1	409.59	405.36	419.53
		Depth (feet)	4.5	5.5	4.5	4.5	3.237	0 9	2	5	∞	י ט	6 442	9.876	11.5	6.852	0	2	10.002	. c	4.5	5.03	4.5	4.5	4.5	4.931	4.5	4.5	11	2	70 10	6.25	V 17	0	7	9	9
	ensions	Rim Elevation (feet)	9 433.809	9 433.639				2 438.002		7 430.727			2 278 440			7			8 448.002					7		470.931		349.224	8 379.338		355.907			351.864		5 408.785	9 424.779

			EX	isting	Existing Condition Junc	Junctions		s Sum	Results Summary Table	a)		
ensions				2-year			1	10-year				100-year
Rim	-	Мах.	Max. Lateral	Max. Total		Max. HGL	Max. Lateral	Max. Total		Max. HGL	Max. Lateral	Max.
Elevation (feet)	(feet)	HGL (2-year) (feet)	(2- year)	(2- year)	Surcnarging (2-year)	(10- year)	(10- year)	(10- year)	Surcnarging (10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	Infl (100-ye
			(cfs)	(cfs)		<u> </u>	(cfs	(cfs)				
3 425.383 5 442.035	4.5	422.04	11.29	11.29	YES	425.9	19.11	19.11	YES	426.38	31.95	
	10.778	427.02	0	36.37	YES		0	54.07	YES	7		
	5.062	445.56	0	17.92	YES			30.52	YES	446.27	0	
	0 .	360.11	0	142.72	YES			244.27	YES	361.74	0	
3 448.216	4.5 7.	445.43	0 0	18 17	YES	446.22	0 0	30.52	YES	447.45		
	4.109	440.36	0	9.07	YES			10.44	YES	440.96	0	
442.924	5.5	440.36	0	0.35	YES	440.64	0	0.61	YES	440.97		
	5.5	440.39	0	0	YES			0.3	YES	440.99		
3 433.943	4.5	430.82	0	4.6	YES			7.94	YES	433.98	0	
431.63	4	430.61	0	8.91	YES	431.49	0	10.19	YES	431.93		
5 398,179	3.679	398.46	0	17.09	YES		0	17.15	YES		0	
	2.256	446.77	0	1.41	YES			2.52	YES			
9 440.479	4	441.01	0	14.38	YES			24.16	YES			
407.686	5.5	403.16	0	20.3	YES	403.56		32.17	YES	405.64		
423.704	13.5	411.44	0	20.41	YES			32.34	YES		0	
	2.5	404.49	0	20.35	YES			32.27	YES			
450.986	4.986	446.68	0 77 77	3.22	YES	448.58	0 00	5.66	YES	451.06	0 25 18	
3 441.431	0.3	394.89	11.4/ 0	15.28	YES			27.54	YES			
	5.5	367.76	0	57.55	YES			71.77	YES			
363.664	5	362.03	0	2.95	YES		0	2.97	YES	363.86	0	
.3 412.513	5.5	408.92	0	28.81	YES	409.4		42.52	YES	409.81	0	
(1)	0	375.56	0	21.61	YES			42.72	YES		0	
	7	401.83	0	29.83	YES			45.01	YES			
395.809	15 493	397.68	0 0	190.93	YES	394.39		124.89	YES	395.//		
.1 388.741	11.5	379.16	0	66.77	YES		0	132.98			0	
	7	369.95	0	63.35	YES			106.49				
	6	362.93	0	79.32	YES			147.69	YES	369.99		
.6 353.326	8.5	349.62	0	172.77	YES	351.52		295.03	YES	352.67	0	
4 351.647	7.647	349.06	0	174.16	YES	350		299.2		351.13	0	
36	11	353.41	0	163.27	YES			292.58		360.42		
9 343.9	2	344.04	0	50.23	YES			32.96	YES	350.28		
	0	421.14	4.4	9.63	YES		7.7	18.79	YES	421.26	13.4	
		396.09	0	3.54	YES			5.76	YES	400		
		400.07	0 0	157.31	YES			156.07	YES	401.07		
	5.751	402.7	0 0	114.09	YES	403.43		114.72	YES	403.65		
407.482	7.002	407.65	0	53.94	YES			57.31	YES	408.52		

Existing Condition Junctions Results Summary Table

ensions				2-year			1	10-year				100-year
Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year) (cfs)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	Max. Infl (100-ye
5 415.863	3 6.363	416.52	0	95.24	YES	416.62	0	97.57	YES	416.7	0	
8 431.528	8	425.19	0	67.62	YES	425.66	0	91.11	YES	427.65	0	
430.278	3 5.5	426.63	0	59.97	YES	427.42	0	78.06	YES	429.28	0	
6 423.639	0	422.29	0	3.73	YES	422.31	0	69.9	YES	422.33	0	
6 423.23	10.87	417.59	0	58.46	YES	418.49	0	90.13	YES	420.07	0	
9 425.391	1.601	419.18	0	56.53	YES	419.56	0	90.21	YES	421.28	0	
2 425.322	9 6	420.22	0	9.7	YES	420.51	0	15.98	YES	421.3	0	
.5 389.345	9	383.07	0	154.07	YES	384.22	0	261.3	YES	386.14	0	
5 413.305	9	414.18	1.54	15.8	YES	414.4	2.5	23.64	YES	414.61	3.92	
406.134	9 1	406.71	0	53.7	YES	406.89	0	52.8	YES	407.08	0	
435.976	5 4	435.58	1.81	33.42	YES	435.84	3.03	36.17	YES	436.07	4.88	
338.727	7 1.198	337.99	3.45	3.45	ON	338.19	6.34	6.34	ON	338.64	10.74	
.6 299.416	9	302.9	26.22	313.07	ON	303.76	47.33	386.5	ON	304.92	86.57	
13 437.593	3 0	438.23	5.72	5.72	YES	438.7	9.95	9.95	YES	439.56	17.71	
6 412.966	5 0	413.63	4.93	27.13	YES	413.84	9.04	47.39	YES	414.15	14.79	
366.82	4	362.99	3.86	4.12	YES	363.07	6.76	7.42	YES	363.16	11.91	
7 335.897	7	332.3	3.48	37.31	ON	333.45	6.03	99.99	ON	333.76	9.79	
408.368	3 0	408.71	99:0	0.91	YES	408.85	1.2	1.66	YES	409.05	1.95	
9 407.959	9 5.5	403.36	0	18.94	YES	403.59	0	29.02	YES	404.55	0	
2 495.702	0	495.78	0.28	0.28	YES	495.8	0.46	0.46	YES	495.83	0.74	
.8 488.148	3 0	488.86	31.91	33.89	YES	489.13	57.94	61.37	YES	489.54	107.15	
7 398.897	0	400.32	1.01	16.52	YES	400.68	1.9	28.67	YES	400.78	3.17	
3 452.563	3 0	453.23	4.94	4.94	YES	453.69	9.1	9.1	YES	455.26	15.82	

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		Q_{con}		
0	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	(10-year) (cfs)	Qcon vs Qcap32	(1)
1 68	11 17	0 16	1 0	CIRCULAR RECT CLOSED	0.51503 CMP	CMP	0 617 05			0	
69	ט נט	16	1 1	RECT_CLOSED	0.0104	CMP	623.55				
187	2	0	1	CIRCULAR	0.13435	RCP	8.05	0.1	47.38		
	5.5	0	1	CIRCULAR	0.01427	RCP	144.83				
	3.5	0	3 6	SIRCULAR	0.03785	CMP	289.03		408.3		
	4	80	1	RECT_CLOSED	0.01601	RCB	295.61				
	4 4	8 0	1	RECT_CLOSED	0.05066	RCB 3CP	296.94		408.32		
	3.3	0	1 1	CIRCULAR	0.2311	RCP	5.2				
	3.5	0	1	CIRCULAR	0.02399	RCP	9.17				
	2 2	0	1 -	CIRCULAR	0.00681	RCB	117.73	0.55	205.8	0.96	
	2	0	1 1	CIRCULAR	0.0271	RCP	14.63				
	4	0	1	CIRCULAR	0.00832	RCP	45.24				
	1.5	0	1	CIRCULAR	0.08918	RCP	9.73				
	Т	0	1	CIRCULAR	0.10304	Other	5.01				
	1	0	1,	CIRCULAR	0.6801	Other	2.81	0.07		0.12	
	2	0	1	CIRCULAR	77770.0	CMP	8.24				
	2	0	1 -	CIRCULAR	0.06256	CONC	0.71		1.26		
	n m	0	1 1	CIRCULAR	0.00597	CONC	15.43				
	2	0	1	CIRCULAR	0.0109	Other	15.62				
	2	0	1	CIRCULAR	0.00912	CONC	0.59				
	2	0	H 7	CIRCULAR	0.00314	CMP	2.51		3.0		
	2	0	1 1	CIRCULAR	0.05453	CONC	0				
	3.5	0	1	CIRCULAR	0.02442	RCP	12.78	0.0			
	2	0	1	CIRCULAR	0.01107	CONC	7.28				
	2	0		CIRCULAR	0.00682	CONC	2.66	0.14	4.4		
	2	0	1 1	CIRCULAR	0.00884	COINC	2.93				
	2	0	1 1	CIRCULAR	0.00682	CONC	5.47				
	2	0	1	CIRCULAR	0.01281	CONC	7.69				
	1	0	1	CIRCULAR	_	CONC	0.93				
	2.5	0	H .	CIRCULAR	0.00683	CONC	14.19				
	1.5	0	3 8	CIRCULAR		CONC	1.09	0.04			
	1.5	0	7	CIRCULAR		CONC	1.61		2.59	0.31	
	2.5	0	1	CIRCULAR	0.00759	CONC	18.71				
	2	0	1	CIRCULAR		CONC	1.72				
	2	0	1	CIRCULAR	0.00619	CONC	1.21		1.87	0.1	
	3.5	0	1 11	CIRCULAR		CONC	22.15	0.29			
	3.5	0	1	CIRCULAR	-	CONC	47.66				
	2	0	1	CIRCULAR		CONC	13.08		25.15		
	2	0	T	CIRCULAR	0.8828.0	CONC	13.1				
	1 E	0	1 1	CIRCULAR	_	RCP	15.28	0.19			
	4	0	1	CIRCULAR		CONC	61.62				
	4	0	1	CIRCULAR	0.00778	CONC	65.78	0.52		0.69	
	2.5	0	1	CIRCULAR	0.03688	CONC	36.12		71.61		
	2.2	0	1	CIRCULAR	0.1602	RCP	12.51	0.1		2.0	
	2	0	1	CIRCULAR	0.11358	RCP	13.6		23.96		
	4	0	T	CIRCULAR		RCP	52.51				
	S	0	- 1	CIRCULAR	0.00215	RCP	54.06	0.45	94.77		
	2	0	1 11	CIRCULAR	0.26307	CONC	0.91			0.01	
	2	0	1	CIRCULAR	0.28416	CONC	1.07				
	1.5	0	1	CIRCULAR	0.01915	RCP	1.31				
	1.5	0	1 1	CIRCULAR	0.0997 F	RCP	2.55			0.13	
	1.5	0	1	CIRCULAR	0.03039	RCP	2.51				

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		Q_{con}		
0	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	(10-year) (cfs)	Qcon vs Qcap32	(1)
	1.5	0 0	1 1	CIRCULAR	0.12254 RCP	RCP	1.26	0.03	2.11	0.06	
	1.5	0 0	1	CIRCULAR	0.00439	RCP RCP	12.79				
	1.5	0	П	CIRCULAR	0.00862	RCP	11.88				
	1.5	0	1	CIRCULAR	0.02045	RCP	12.92				
	1.5	0	1	CIRCULAR	0.0199	RCP RCP	12.93				
	1.5	0	T	CIRCULAR	0.08713	RCP	1.12				
	1.5	0	1	CIRCULAR	0.01599	RCP	2.3				
	3.5	0	1	CIRCULAR	0.02105	RCP	112.84				
	1.5	0		CIRCULAR	0.01148	RCP	4.64				
	1.5	0	1	CIRCULAR	0.02806	RCP	20.09			1.44	
	2	0	1	CIRCULAR	0.28995	RCP	20.99				
	2.5	0	1	CIRCULAR	0.0249	CONC	23.94				
	1.5	0	T	CIRCULAR	0.25101	CONC	1.93	0.04	3.15	0.06	
	2	0	1	CIRCULAR	0.07585	CONC	12.79				
	2	0	1	CIRCULAR	0.01	RCP	1.94		3.25		
	2	0	1	CIRCULAR	0.00913	RCP	4.1				
	2	0	T	CIRCULAR	0.06722	RCP	2.27				
	2	0	1	CIRCULAR	0.50682	RCP	0.27				
	2	0	1	CIRCULAR	0.06722	RCP	2.02				
	2 2	0	1	CIRCULAR	0.06722	RCP	0.78	0.01	1.22	0.02	
	2		T	CIRCULAR	0.04271	RCP	169.0				
	3	0	1	CIRCULAR	0.01895	RCP	4.9				
	4	0	1	CIRCULAR	0.0126	CONC	63.83				
	2	0	1	CIRCULAR	0.05673	CONC	0.26			0.01	
	7	0	I	CIRCULAR	0.0063	CONC	2./3	0.15			
	2	0	1	CIRCULAR	0.28118	CONC	0.31		0.5		
	2	0	1	CIRCULAR	0.0076	CONC	1.77	0.0		7 0.15	
	2	0	1	CIRCULAR	0.03135	CONC	2.04				
	2	0	1	CIRCULAR		CONC	2.6	0.07	4.19		
	2	0	1	CIRCUI AR		CONC	2.19	0.11	3.59	0.18	
	2	0	T	CIRCULAR	0.04885	CONC	6.35	0.13			
	2	0	П	CIRCULAR	0.0155	RCP	1.12	0.04			
	4	0	1	CIRCULAR	0.05904	CONC	48				
	2	0		CIRCULAR	0.34511	CONC	10.53	0.08			
	7	0		CIRCULAR	0.00922	CONC	9.9/		16.64	0.7/	
	1.5	0	1	CIRCULAR		CONC	0.32				
	1.5	0	1	CIRCULAR		CONC	1		1.66	5 0.22	
	1.5	0	1	CIRCULAR		CONC	16.63				
	2 4	0	T E	CIRCULAR	0.01884	CONC	120.63		0.63	3 0.02	
	2	0	1	CIRCULAR		CONC	1.49	0.04			
	2	0	1	CIRCULAR	.01155	CONC	1.97	80:0			
	2	0	1	CIRCULAR		CONC	0.28	0.02			
	2	0	1	CIRCULAR	.06713	CONC	1.39	0.02		0.10	
	4	0	1	CIRCULAR	0.04016	CONC	43.11	0.15	54.1		
	2	0	1	CIRCULAR	0.27741	CONC	41.88				
	2	0	T -	CIRCULAR	.07911	CONC	1.14	0.02		0.03	
	2	0 0	T	CIRCUIAR	0.15303	COINC	40.11			17.77	
	2	0	1	CIRCULAR	.08633	CONC	0.48		0.74		
	2	0	1	CIRCULAR		CONC	40.15	1.03			
	2 0	0	1 1	CIRCULAR		CONC	0.32	0.01			
	2 2	0	1	CIRCULAR	0.15413	CONC	3.42	0.04		0.07	
	2	0	1	CIRCULAR	0.02973	CONC	36.19	0.93	45.47		
	2	0	1	CIRCULAR	0.02972	CONC	3.7	0.09		0.17	

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		Q		
0	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	(10-year) (cfs)	Qcon vs Qcap32	(1)
	T	0	1	CIRCULAR	0.00272	CONC	4.03				
	1 2		I	CIRCULAR	0.02845	HDPE	1.34				
	2	0	1	CIRCULAR	0.00117	CONC	4.56	0.59		0.89	
	2		1	CIRCULAR	0.0333	CONC	9.28				
	2	0	T	CIRCULAR	0.00117	CONC	12.77				
	2.5		1	CIRCULAR	0.22562	CONC	8.79				
	2.5		1	CIRCULAR	0.00514	CONC	9				
	2.5		1	CIRCULAR	0.00118	CONC	22.33				
	2.5		1	CIRCULAR	0.00118	CONC	22.48				
	2.5	0	1	CIRCULAR	0.00117	CONC	23.37		32.77	2.33	
	2.5		1	CIRCULAR	0.00118	CONC	27.31				
	4.5		1	CIRCULAR	0.00118	CONC	155.04		226.08		
	4.5		1	CIRCULAR	0.00117	CONC	178.42				
	2		T	CIRCULAR		CONC	0.56				
	2			CIRCULAR	0.01325	CONC	0.66	0.03	1.08	0.04	
	2		1 -	CIRCULAR	0.0143	CONC	0.81				
	2	0	1 1	CIRCULAR	0.00604	CONC	0.52		0.84		
	1.5		1	CIRCULAR	0.27246	RCP	0.02				
	2.5		1	CIRCULAR	0.08137	RCP	2.48	0.02		0	
	2.5		1	CIRCULAR	0.14974	CONC	16.74		30.43		
	2 2		₩ .	CIRCULAR	0.0177	RCP	13.52	0.45			
	2		1	CIRCULAR	0.03073	RCP	11 01		1941	0.41	
	2		1	CIRCULAR	0.04312	RCP	10.11				
	9		1	CIRCULAR	0.00902	RCP	103.69	0.26	203.71	0.51	
	4		1	CIRCULAR	0.01009	RCP	60.46				
	2		1	CIRCULAR	0.01528	RCP	12.94				
	2	0	1	CIRCULAR	0.36589	RCP	12.95				
	2	0	1	CIRCULAR	0.31957	RCP	12.95				
	2 3	0		CIRCULAR	0.00616	RCP	12.91				
	7	0	T	CIRCULAR	0.00941	CONC	3.18				
			1	CIRCULAR	0.00918	RCP	20.05				
	n (n	0	1	CIRCULAR	0.01035	CONC	24.74				
	8	0	1	CIRCULAR	0.03263	RCP	50.65				
	2.5		1	CIRCULAR	0.14147	RCP	50.7				
	2.5		1	CIRCULAR	0.04496	RCP	48.3				
	1.5		1	CIRCULAR	0.06107	RCP	0.62		0.98		
	1.5		1	CIRCULAR	0.02665	RCP	3.35				
	2	0	1	CIRCULAR	0.00693	RCP	1.58	0.08	2.66		
	1.5		1 (CIRCULAR	0.033	RCP	9.61				
	1.5		1 ~	CIRCULAR	0.04284	RCP	3.1				
	1.5		1	CIRCULAR	0.06509	RCP	9.82	0.37		0.66	
	1.5		1	CIRCULAR	0.0756	RCP	0.62				
	1.5		1	CIRCULAR	0.01109	RCP	0.75				
	1.5		1	CIRCULAR	0.01744	RCP	5.06				
	1.5	0	1	CIRCULAR	0.0543	RCP	4.91		8.85	0.36	
	T.3		1	CIRCULAR	0.05533	RCP	24.63	0.46	4		
	1.5		+	CIRCULAR	0.03164	RCP	2.23	0.12			
	2		1	CIRCULAR	0.07428	RCP	9.69				
	2.5		1	CIRCULAR	0.03291	RCP	46.6				
	1.5		П	CIRCULAR	0.06934	RCP	1.37				
	1.5		1	CIRCULAR	0.16109	RCP	1.4				
	1.5	0	-	CIRCULAR	0.08181	RCP	9.1	0.3			
	1.5		1	CIRCULAR	0.05659	RCP	3.1				
	1.5		1	CIRCULAR	0.08591	RCP	2.24				
	1.5	0	1	CIRCULAR	0.03075 RCP	RCP	2.21	0.12	3.9	0.21	
	2.5		1	CIRCULAR	0.01501	RCP	37.03				

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		Dir	Dimensions			2	2-year	10	10-year	
D' or H'						Q _{con}		O _{con}		
(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	(10-year) (cfs)	Qcon vs Qcap32	(1)
1.5	0	1 (CIRCULAR	0.07376 RCP	RCP	4.18	0.15	7.14	1 0.25	
1.5	0	1	CIRCULAR	0.03348	RCP	2.21				
2	0	, L	CIRCULAR	0.05196	RCP	24.63		7		
1 2	0		CIRCULAR	0.05642	RCP	11.45				
1.5	0	1 1	CIRCULAR	0.127	RCP	1.28		2.04		
2.5	0	1	CIRCULAR	0.02463	RCP	25.76				
2.5	0	1	CIRCULAR	0.00989	RCP	25.79				
2.5	0	1	CIRCULAR	0.03491	RCP	25.66				
1.5	0	7 [CIRCULAR	0.01969	RCP	2.42				
1.5	0	1,	CIRCULAR	0.24242	RCP	4.25				
1.5	0		CIRCULAR	0.02704	RCP	4.07				
1.5	0	7	CIRCULAR	0.0339	RCP RCP	3.4				
1.5	0	1	CIRCULAR	0.01441	RCP	0.6				
1.5	0	1	CIRCULAR	0.01153	RCP	19.33				
1.5	0	e .	CIRCULAR	0.06287	RCP	0.3				
L.5	0	7	CIRCULAR	0.02156	RCP	7.39		4.22	L.3	
1.5	0	1 11	CIRCULAR	0.02279	RCP	2.28				
1.5	0	1	CIRCULAR	0.16671	RCP	4.11				
1.5	0	1	CIRCULAR	0.02839	RCP	2.15				
1.5	0	el ;	CIRCULAR	0.01689	RCP	20.21	1.48	22	1.61	
T.3	0	1 1	CIRCULAR	0.00792	RCP	1.3				
1.5	0	1	CIRCULAR	0.00825	RCP	7.66				
1.5	0	1	CIRCULAR	0.0085	RCP	10.05				
1.5	0	1	CIRCULAR	0.023	RCP	2.6			0.35	
1.5	0	1	CIRCULAR	0.00889	RCP	4.36	0.44			
1.5	0	1 1	CIRCULAR	0.0321	RCP	1,73		2.98	0.37	
1.5	0	1	CIRCULAR	0.03202	RCP	1.1				
1.5	0	1	CIRCULAR	0.02974	RCP	2.8				
1.5	0	1	CIRCULAR	0.13965	RCP	0.53		1.99	0.05	
1.5	0	1	CIRCULAR	0.02338	RCP	0.62	0.04	1.09		
1.5	0	1 1	CIRCULAR	0.11492	RCP	7.0		1.51	0.04	
1.5	0	1 11	CIRCULAR	0.05558	RCP	21.09		24.41		
1.5	0	1	CIRCULAR	0.03617	RCP	3.29		6.34		
9 ,	0	-	CIRCULAR	0.00788	RCP	180.98		312.42	0.83	
1 1	0	1	CIRCULAR	0.12586	RCP	13.02	0.05	1.06		
1.5	0	1 [CIRCULAR		RCP	11.85		13.91	1.23	
1.5	0	1,	CIRCULAR	0.04832	RCP	1.11		2.16		
1.5	0	-	CIRCULAR	0.02709	RCP	3.29		6.1		10
1.5	0 0	I	CIRCULAR CIRCULAR	0.08051	RCP RCP	4.39	0.15	99.7 59.0	0.27	
1.5	0	H	CIRCULAR	0.00923	RCP	9.24		11.71		
1.5	0	1	CIRCULAR	0.12857	RCP	0.99		1.83		
1.5	0	-	CIRCULAR	0.07572	RCP	0.99				
2.5	0	7 7	CIRCULAR	0.11242	CONC	3.79	0.03	77.7	3.000	
1.5	0	1 (CIRCULAR	0.0122	RCP	12.41		,		
1.5	0	1,	CIRCULAR	0.16693	RCP	4.86				
2.5	0		CIRCULAR	0.0872	CONC	6.84		13.1	0.1	
1.5	0	1	CIRCULAR	0.37845	RCP	75.61	0 0	33 88		
1.5	0	1 11	CIRCULAR	0.50056	RCP	0.16				
2.75	0	1	CIRCULAR	0.05563	RCP	23.12			0.2	
2	0	7	CIRCULAR	0.09183	RCP	0.8		2.29		
2 2	0	1 1	CIRCULAR	0.30285	CMP	1.36	0.02		0.04	
2	0	1	CIRCULAR	0.19298	CMP	0.7				
2	0	1	CIRCULAR	0.36985	CMP	1.96				

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		O _{con}		
0)	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	=	Qcon vs Qcap32	(1)
	9	0	1	CIRCULAR	0.00414 RCP	RCP	184.62	0.68	339.04	1.24	
	2 2	0	1 1	CIRCULAR	0.03612	RCP	33.78				
	2	0		CIRCULAR	0.02814	RCP	22.18				
	7.2	0	-	CIRCULAR	0.02642	RCP RCP	3.47				
	1.5	0	1	CIRCULAR	0.04388	RCP	4.63				
	9	0	1	CIRCULAR	0.0059	RCP	103.3				
	7 2	0	-	CIRCULAR	0.02862	RCP	7.6				
	1.5	0	1	CIRCULAR	0.02792	RCP	0				
	1.5	0	1	CIRCULAR	0.02613	RCP	3.07				
	2	0	Π .	CIRCULAR	0.23975	CONC	21.4			0.33	
	2.5	0	1	CIRCULAR	0.01058	CONC	3.84	0.16	6.61		
	2	0	1	CIRCULAR	0.15624	CONC	8.83				
	2	0	1	CIRCULAR	0.0284	CONC	1.24				
	2	0		CIRCULAR	0.09169	RCP	8.94				
	2.5	0	T	CIRCULAR	0.01802	Ž &	35.41	0.06	2.89	0.1	
	4	0	1	CIRCULAR	0.00253	RCP	38.75				
	1.5	0	1	CIRCULAR	0.01602	CONC	13.07				
	1.5	0	₽ ₹	CIRCULAR	0.04258	CONC	17.16				
	C.T.			CIRCULAR	0.004443	SCP	10.89				
	2.5	0	1	CIRCULAR	0.08958	RCP	31.24	0.25	49.1	0.4	
	2.5	0	1	CIRCULAR	0.04171	RCP	19.12				
	1.5	0	I	CIRCULAR	0.7111	RCP	22.14				
	1.5	0	1	CIRCULAR	1 6800.0	RCP	9:0				
	1.5	0	1	CIRCULAR	0.11704	RCP	3.55				
	1.5	0	1	CIRCULAR	0.0505	RCP	19.62				
	1.5	0		CIRCULAR	0.03914	RCP SCB	6.25				
	2.5	0		CIRCULAR	0.03/19	RCP	31.3				
	1.75	0	1	CIRCULAR	0.01023	RCP	10.03				
	1.75	0	1	CIRCULAR	0.04099	RCP	5.85		11.91		
	4.5	0	1	CIRCULAR	0.01555	RCP	224.32		261.46	1.07	
	2.5	0	1	CIRCULAR	0.01245	RCP	22.08	0.48	40.18		
	1.5	0	T	CIRCULAR	0.027374	RCP	13.92		25.14		
	1.5	0	1	CIRCULAR	0.15811	RCP	16.94		29.29		
	2	0	1	CIRCULAR		RCP	13.85		24.83		
	2	0	т .	CIRCULAR	0.0138	RCP	13.85		24.86	0.94	
	1.5	0	1	CIRCULAR	0.01622	RCP RCP	2.42				
	1.5	0	1	CIRCULAR		RCP	5.07	0.26	8.77	0.46	
	2	0	1	CIRCULAR	0.2531	НОРЕ	0				
	2.5	0	1 1	CIRCULAR	0.02991	RCP 3CP	1.25	0.02	2.32	0.03	
	2.2	0	1 1	CIRCULAR	0.15358	RCP	0		0		
	2	0	1	CIRCULAR	0.07147	RCP	0				
	3.5	5.5	1	CIRCULAR	0.00541 F	RCP	92.62				
	3.5	5.5	1	CIRCULAR	0.00895	RCP	92.62	0.97	110.25	1.16	
	2	0	1	CIRCULAR	0.05404	RCP	0.54			0.0	
	2	0	1	CIRCULAR	0.05318	RCP	0.53	0.01	0.95		
	2	0	1	CIRCULAR	0.00612	RCP	5.93				
	1.5	0	1 1	CIRCULAR	0.0664	RCP	0.76	0.03	2.05	0.08	
	2 2	0	1 1	CIRCULAR	0.0095	RCP	0		0		
	2	0	1	CIRCULAR	0.01855	RCP	0				
	2	0	т.	CIRCULAR	0.00971	RCP	4.34				
	2	0	Η Η	CIRCULAR	0.00472	RCP	4.33	0.43	7.61	0.34	
	2	0	1	CIRCULAR	0.02473	RCP	4.33				

			Ξ	Dimensions			7	2-year	10	10-year	
	D' or H'						Qcon		Q		
4)	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	(10-year) (cfs)	Qcon vs Qcap32	(1)
	1.5	0	1	CIRCULAR	0.04249	RCP	0 2			0	
	3 0		Τ .	CIRCULAR	0.00279	RCP BCP	10.27				
	m m	0	1	CIRCULAR	0.0074	RCP	10.33	0.18	19.25		
	4		₽ .	CIRCULAR	0.02767	RCP	35.44				
	1.5	0	П	CIRCULAR	0.02594	RCP RCP	36.23				
	4		1 1	CIRCULAR	0.2143	RCP	1.02				
	2.5		1	CIRCULAR	0.00377	CONC	15.43				
	2.5		1	CIRCULAR	0.00524	CONC	15.39				
	7		T	CIRCULAR	0.01283	RCP	412.83				
	4.75	0	1	CIRCULAR	0.00246	ABS	7.24	0.06		0.27	
	1	0	1	CIRCULAR	0.06325	ABS	0.67	0.07			
	1	0	1	CIRCULAR	0.07322	RCP	3.43	0.36			
	1		1	CIRCULAR	0.04763	ABS	2.1	0.27			
	1.5		ਜ ਦ	CIRCULAR		RCP	5.91	0.36	10	0.64	
	1 2	0	1	CIRCULAR	0.0277	ABS	3.66	0.95		1.06	
	6.5		1	CIRCULAR	0.00964	RCP	330.59	0.64	510.01		
	5.5	4	1	CIRCULAR	0.00554	RCP	191.53				
	3	5.5	1	CIRCULAR	0.01271	RCP	50.82		60.82		
	5.5		T	CIRCULAR	0.00637	RCP	216.48				
	3 3		T	CIRCULAR	0.02425	CONC	9.08	90.0	15.03	0.14	
	1.5		1	CIRCULAR	0.03165	RCP	2.15				
	1.5		1	CIRCULAR	0.14235	RCP	1.79			0.08	
	1	0	1	CIRCULAR	0.02113	ABS	0.92		1.53		
	1		1	CIRCULAR	0.08778	RCP	1.86	0.18			
	1.5		н .	CIRCULAR	0.02043	SP	0.26	0.03	0.46		
	4	0 80	Τ .	RECT CLOSED	0.07320	RCB	237.43	0.37	72.07.2	0.42	
	1.5		1	CIRCULAR	0.19522	RCP	6:39			0.25	
	1.5		τ	CIRCULAR	0.03309	ABS	17.58				
	2	0	1	CIRCULAR	0.03023	ABS	10.7	0.27			
	1	0	1	CIRCULAR	0.01262	RCP	0.32				
			T	CIRCULAR	0.0057	RCP	0.05	0.02			
	1.5	0	L	CIRCULAR	0.13779	RCP	5.7	0.15	10.34	0.27	
	9		T	CIRCULAR	0.0133	RCP	122.04	0.25			
	5		1	CIRCULAR	0.00365	RCP	118.66				
	00		T	CIRCULAR	0.00391	RCP	259.47				
	∞ (T	CIRCULAR	0.00341	RCP	248.43				
	9	0	1	CIRCULAR	0.01039 RCP	RCP	237.93		416.48	96.0	
			1	CIRCULAR	0.02475	RCP	98.43				
	5		1	CIRCULAR	0.00709	RCP	101.98				
	3.5		Ħ,	CIRCULAR	0.0077	RCP	53.29				
	3.5		ਜ ਜ	CIRCULAR	0.03572	RCP	96.18				
	n		+ +	CIRCULAR	0.06052	RCP	12.71	0.08			
	1.25		1	CIRCULAR	0.0109	HDPE	0.65	0.1			
	1.25		1	CIRCULAR	0.00612	НДРЕ	2.86				
	1.25		1	CIRCULAR	0.0342	НDРЕ	2.85				
	1.25			CIRCULAR	0.04641	HDPE	1.06	0.08	1.8	0.13	
	T.25	0	+ [CIRCULAR	0.03596	RCP	1.85	0			
	1 8		1	CIRCULAR	0.01075	RCP	528.97		926.5	86:0	
	1.5		1	CIRCULAR	0.1456	RCP	2.15				
	1.5		1	CIRCULAR	0.01633	RCP	2.51				
	1.5	0	1 -	CIRCULAR	0.0151	RCP	2.5	0.19		0.33	
	3.5		1 [CIRCULAR	0.00089	RCP	51.58		81.98		
	1.25		1	CIRCULAR	0.00845	НОРЕ	3.14		5.52		
	1.25		1	CIRCULAR	0.01821	RCP	3.09	0.35			

0.17

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		O _{con}		
a	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	<u></u>	Qcon vs Qcap32	(1)
	9	0	1	CIRCULAR	0.00147 RCP	RCP	22.87	0.14	53.02	0.33	
	2	0	1	CIRCULAR	0.07171	RCP	5.21				
	1.5	0	1	CIRCULAR	0.14905	RCP	2.41				
	1.5	0	1	CIRCULAR	0.02518	RCP	1.57				
	e e	0	1	CIRCULAR	0.00345	RCP	54.43				
	2	0	1	CIRCULAR	0.01003	RCP	5.42				
	2	0	1	CIRCULAR	0.02382	RCP	5.43				
	2	0	1	CIRCULAR	0.01737	RCP	11.2				
	2.5	0	1	CIRCULAR	0.02144	RCP	16.45				
	w c	0	1	CIRCULAR	0.06449	RCP	23.16		39.62		
	29:0	0	τ τ	CIRCULAR	0.16213	PVC	0.91	0.18			
	2.5	0	1	CIRCULAR	0.02387	RCP	21.28				
	2	0	c	CIRCULAR	0.0155	RCP	2.56				
	2	0	T	CIRCULAR	0.07858	RCP	2.55				
	1	0	1	CIRCULAR	0.08978	PVC	2.21				
	1.5	0	1	CIRCULAR	0.08805	RCP	2.23				
	1.5	0	T .	CIRCULAR	0.10047	CMP	2.14	0.12		0.21	
	2.3	0	T	CIRCULAR	0.00716	RCP RCP	12.17				
	ı m	0	1	CIRCULAR	0.11572	RCP	0.34				
	1.5	0	1	CIRCULAR	0.02669	RCP	7.33	0.43	12.97	0.76	
	3.5	0	1 7	CIRCULAR	0.02534	RCP	47.37		ì		
	4 25		1	CIRCULAR	0.0315	RCP SCP	124.13		111.99		
	4	0	1	CIRCULAR	0.02168	RCP	112.8				
	4.5	0	1	CIRCULAR	0.02175	RCP	128.08				
	3.5	0	1	CIRCULAR	0.03355	RCP	63.27			0.59	
	1.5	0	c	CIRCULAR	0.02837	3	2.37				
	2	0	1	CIRCULAR CIRCULI AR	0.03008	200	21.13				
	2	0	T	CIRCULAR	0.00332	RCP	8.98				
	2.25	0	1	CIRCULAR	0.0059	RCP	5.01		5.45		
	1.25	0	1	CIRCULAR	0.08432	RCP	6.91		11.71		
	2	0	1	CIRCULAR	0.00453	RCP	0.96	90.0	1.77	0.12	
	1.5	0	T	CIRCULAR	0.06693	RCP	1.01	0.0			
	1	0	1	CIRCULAR	0.00305	RCP	0.24			0.24	
	1	0	1	CIRCULAR	0.17878	CMP	0.83		1.53		
	IN U	10		RECT_CLOSED	0.01659	RCB	308.85		353.06		
	1.5	0	T	CIRCULAR	0.01274	SCP SCP	4.94		8.1		
	2	0	1	CIRCULAR	0.0304	RCP	14.72	0.37	26.42	29:0	
	1.5	0	1	CIRCULAR	0.00323	RCP	3.18		5.4		
	1.5	0	1	CIRCULAR	0.27678	RCP	5.98		10.21		
	4		1	CIRCULAR	0.02993	ACP RCP	0.34	0.02	0.54	0.03	
	1.5	0	H	CIRCULAR	0.14772	RCP	0.83				
	2	0	1	CIRCULAR	0.01324	RCP	10.69				
	2	0	1	CIRCULAR	0.15634	RCP	12.41		21.96		
	× 7	0	1	CIRCULAR	0.00422	RCP	189.62				
	L:3		T	CIRCULAR	0.08/12	KCP	PC 24.11.			1.13	
	1.5	0	T	CIRCULAR	0.06116	RCP	0.88				
	2	0	1	CIRCULAR	0.02205	RCP	1.42		2.36		
	1.5	0	1	CIRCULAR	0.00966	RCP	2.16				
	1.25	0	1	CIRCULAR	0.02919	HOPF	0.24				
	1.25	0	1	CIRCULAR	0.04105	CMP	0.26				
	1.5	0	1	CIRCULAR	0.06929	RCP	1.88				
	1.5	0	1	CIRCULAR	0.00/83	83 RCP 89 RCP	13.17	0.66		1.07	

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		Q _{con}		
4)	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	<u> </u>	Qcon vs Qcap32	(1)
	1.5	0	1	CIRCULAR	0.15237 RCP	RCP	3.37				
	1.5		I	CIRCULAR	0.00506	RCP	5.83				
	7		1	CIRCULAR	0.00263	RCP	167.14	0.51		96.0	
	1.5	0	1	CIRCULAR	0.01929	RCP	4.35				
	1.5	0	1	CIRCULAR	0.00704	RCP	3.84				
	1.5		1	CIRCULAR	0.27655	CMP	0				
	1.5		1	CIRCULAR	0.19015	CMP	3.46				
	2.5		1	CIRCULAR	0.09578	RCP	19.06				
	1.5			CIRCULAR	0.03988	RCP	1.33				
	4.5	0		CIRCULAR	0.00564	CMP	98.16	0.66	1/8./9	11.21	
	1.5	0	1	CIRCULAR	0.04587	RCP	6:39				
	2	0	1	CIRCULAR	0.00784	RCP	8.04				
	0.5	0	1	CIRCULAR	0.87276	PVC	1.17				
	ע ר	0		CIRCULAR	0.00576	RCP	50.55	0.26	60.13		
	L.S.	0		CIRCULAR	0.04554	RCP	0.94	0.04	1.50	0.0/	
	n m	0	1	CIRCULAR	0.00379	RCP	25.56	0.62	55.89		
	2	0	1	CIRCULAR	0.00517	RCP	1.31	0.08			
	3	0	1	CIRCULAR	0.03181	RCP	104.34				
	w .		,	CIRCULAR	0.0469	RCP	104.24		146.31		
	1.5	0	1	CIRCULAR	0.04287	RCP	6.35	0.11	3.83	0.18	
	1.5		1 1	CIRCULAR	0.02149	HDPE	2.01	0.13			
	2.5		1	CIRCULAR	0.00601	RCP	0.37	0.01	0.82	0.03	
	2		1	CIRCULAR	0.00605	RCP	0.33				
	2.5		1	CIRCULAR	0.09391	RCP	0.19				
	1.5		1	CIRCULAR	0.02797	RCP	0.32				
	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0	1 -	CIRCULAR	0.03348	RCP	1.53		7.30		
	2		1	CIRCULAR	0.1509	CONC	5.05				
	5	0	1	CIRCULAR	0.01522	RCP	94.4	0.29	16		
	1.5		1	CIRCULAR	0.14643	CMP	2.81				
	1.5		1	CIRCULAR	0.00976	RCP	1.43				
	1.5		1	CIRCULAR	0.17017	RCP	0.51		0.88		
	2	0	1	CIRCULAR	0.04798	HDPE	1.87	0.04		0.07	
	2		. 1	CIRCULAR	0.46873	HDPE	2.39				
	1.5	0	1	CIRCULAR CIRCUI AR	0.03369	RCP	16.7	0.12	4.09	0.2	
	4	0	1	CIRCULAR	0.10334	CONC	18.95				
	1.5		1	CIRCULAR	0.04903	HDPE	0.86				
	1.5	0	ī	CIRCULAR	0.03154	НОРЕ	0.89			80:0	
	1.5			CIRCULAR	0.03585	HDPE	1.72				
	1.5	0	T	CIRCULAR	0.02862	HDPE	2.5				
	1.5			CIRCULAR	0.01638	HDPE	0.91	0.03	0.63		
	2		1	CIRCULAR	0.02458	RCP	14.2				
	1.5		1	CIRCULAR	0.04004	RCP	4.91				
	1.5		1	CIRCULAR	0.02909	НДРЕ	4.21		6.68		
	1.5	0	1	CIRCULAR	0.01614	HDPE	0.19		0.29	0.02	
	7.3	0	1	CIRCULAR	0.13082	HDPE	4.53	90.0	7.69		
	1.5		1 1	CIRCULAR	0.01652	HDPE	1.57	0.12	2.56		
	1.5		1	CIRCULAR	0.03322	HDPE	2.05				
	1.5		1	CIRCULAR	0.01452	НОРЕ	1.03		1.59		
	1.5	0	1	CIRCULAR	0.02852	НОРЕ	1.28				
	1.5	0	1	CIRCULAR	0.04167	HDPE	4.22				
	- L	0		CIRCULAR	0.08/83	RCP	0.66	90.0		0.1	
	1.5		1	CIRCULAR	0.02495	RCP	3.52				
	1.5		1	CIRCULAR	0.06935	RCP	1.18				
	2	0	1	CIRCULAR	0.10685	RCP	4.79	90.0	7.61	0.1	
	1.5		-	CIRCULAR	OCTOO	RCP	7.19				

0.71

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			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		Q _{con}		
<u> </u>	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material		Qcon vs Qcap3	<u>-</u>	Qcon vs Qcap32	(1)
	1.5	0	1 0	CIRCULAR	0.00934 RCP	RCP RCP	3.22	0.32	5.82	0.57	
	2	0	1	CIRCULAR	0.06925	RCP	3.88				
	2.5	0	T	CIRCULAR	0.05923	RCP	10.94				
	m m	0	T	CIRCULAR	0.03148	RCP	10.88				
	1.5	0	1	CIRCULAR	0.06224	RCP	1.07				
	4	0	T	CIRCULAR	0.01105	RCP	26.68				
	1.5	0	T T	CIRCULAR	0.07414	RCP	0.64 26.1				
	2.5	0	1	CIRCULAR	0.02111	RCP	16.97				
	2.5	0	7	CIRCULAR	0.06037	RCP	24.28				
	1.3	0	1 1	CIRCULAR	0.04587	RCB	21.01				
	2	0	1	CIRCULAR	0.02502	RCP	12.6				
	7 0	0 0	1 .	CIRCULAR	0.02587	RCP	11.2		20.07		
	1.5	0	7 [CIRCULAR	0.02778	CMP	3.17	0.33			
	2	0	1	CIRCULAR	0.01345	HDPE	6.31				
	1.5	0	1	CIRCULAR	0.12358	ABS	4.19				
	4 0	0	7	CIRCULAR	0.0162	RCP	72.19		12		
	7 4	0	7	CIRCULAR	0.07062	RCP	78.79				
	4	0	H	CIRCULAR	0.03356	RCP	61.5				
	4	0	1	CIRCULAR	0.00678	RCP	61.41				
	4	0	T	CIRCULAR	0.0181	RCP	59.12	0.31	97.52		
	33 1	0	1	CIRCULAR	0.03747	RCP	3.73				
	1.5	0	1	CIRCULAR	0.0509	CMP	5.4				
	8	0	1	CIRCULAR	0.09784	CMP	10.59	0.05			
	9 7	0	- 1	CIRCULAR	0.03933	RCP	118.12		2.		
	1.5	0	T	CIRCULAR	0.01682	ABS	2.78	0.05	4.75	0.09	
	1.5	0	1	CIRCULAR	0.02226	ABS	5.64				
	1.5	0	1	CIRCULAR	0.06198	ABS	5.63				
	2	0	П .	CIRCULAR	0.00607	RCP	4.87		8.74	0.5	
	20	0		CIRCULAR	0.01527	RCP	119.29	0.23	34.42		
	· ·	0	1 11	CIRCULAR	0.0082	RCP	19.38	0.32	34.44	0.57	
	3	0	1	CIRCULAR	0.10425	RCP	11.41	0.05	20.68		
	1.5	0		CIRCULAR	0.00806	CMP	6.55	1.28	9.47	1.85	
	2 2 1.5	0	7	CIRCULAR	0.01033	RCP	1.34	0.09	19.02		
	2	0	1 1	CIRCULAR	0.00787	RCP	79.7		13.39		
	2	0	1	CIRCULAR		RCP	14.65				
	2 7	0	1	CIRCULAR	0.04249	RCP	14.64	0.31			
	2	0	1	CIRCULAR	0.01891	RCP	9.41			0.53	
	2	0	1	CIRCULAR	0.22315	CONC	2.98	0.04			
	2	0	1	CIRCULAR	0.00435	ABS	7.11		12.66	3:0	
	0.5	0	1	CIRCULAR	0.04295	ABS	0 0	0 0		0 800	
	1.5	0	1 1	CIRCULAR		RCP	1.28	0.07	2.32		
	1.5	0	1	CIRCULAR	0.0967	RCP	1.31				
	1.5	0	1	CIRCULAR	0.04935	ABS	2.05		3.55		
	w r	0		CIRCULAR	0.01085	CMP	20.55	0.55			
	1.5	0	7	CIRCULAR	0.0132	RCP	0.03	0.29		0.12	
	1.5	0	1	CIRCULAR	0.01514 RCP	RCP	5.65				
	1.5	0	1	CIRCULAR	0.01978	RCP	5.55				
	1.5	0	7	CIRCULAR	0.00456	HDPE	4.05				
	1.5	0	7 [CIRCULAR	0.03134	RCP	1.18			0.12	
	4	0	1	CIRCULAR	0.00646 RCP	RCP	39.62	0.34	29.69		
	4	0	1	CIRCULAR	0.00902	RCP	54.04			0.67	
	14	0	IT	CIRCULAR	0.01441	RCP	07.66	CC.U	27,42		

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		O _{con}		
0)	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	(10-year) (cfs)	Qcon vs Qcap32	(1)
	1.5	0	1	CIRCULAR	0.15746 CMP	CMP	1.36	0.06		0.1	
	3.3	0	1	CIRCULAR	0.00884	RCP	2.34				
	0.92	2.67	1	RECT_CLOSED	0.00802	RCB	2.57		4.63		
	2	0	1 7	CIRCULAR	0.00666	RCP	10.88				
	U.Y.	0	1	CIRCULAR	0.07756	SP	7.03				
	0.33	0	1	CIRCULAR	0.13726	HDPE	0.87				
	3	0	1	CIRCULAR	0.00492	RCP	20.26				
	8	0	т,	CIRCULAR	0.01641	RCP	40.31				
	4	0	T -	CIRCULAR	0.00819	RCP	85.12				
	1 4	0	1	CIRCULAR	0.00833	RCP	93.23				
	3	0	1	CIRCULAR	0.00403	RCP	23.31				
	6	0	1 7	CIRCULAR	0.02132	RCP	4.78				
	1.5	0	T	CIRCULAR	0.05786	RCP RCP	18:07		32.36	0.7	
	3	0	1	CIRCULAR	0.03919	RCP	17.98	0.14			
	3	0	1	CIRCULAR	0.01655	RCP	17.86		29.43		
	m r	0	1,	CIRCULAR	0.03188	RCP	27.84				
	w .c	0	1	CIRCULAR	0.00483	RCP	13.86				
	n m	0	1	CIRCULAR	0.07015	RCP	13.13				
	2.5	0	1	CIRCULAR	0.01333	RCP	28.05				
	2.5	0	1	CIRCULAR	0.05245	CMP	28.19				
	m n	0	1	CIRCULAR	0.02697	RCP	28.65	0.26	50.53	3 0.46	
	n (r)	0	1	CIRCULAR	0.00358	RCP	5.66				
	3	0	1	CIRCULAR	0.00366	CMP	29.91				
	1.5	0	1	CIRCULAR	0.01859	RCP	6.59	0.46	11.35	0.79	
	1.5	0	7	CIRCULAR	0.01746	RCP	80 77 77				
	C.1.	0	T	CIRCULAR	0.0426/	RCP RCP	4.03	0.21	3.73	0.78	
	1.5	0	1	CIRCULAR	0.02067	RCP	9.54				
	2	0	1	CIRCULAR	0.01369	RCP	13.01				
	2.5	0	1	CIRCULAR	0.01937	RCP	13.15		22.7	0.4	
	2.5	0	H -	CIRCULAR	0.01908	HDPE	15.7		27.54		
	6.2	0	T	CIRCULAR	0.00199	200	110.08	0.58	30.00		
	9	0	1	CIRCULAR	0.00114	RCP	274.05		375.58		
	9	0	1	CIRCULAR	0.00155	RCP	254.72		337.99	2.03	
	9	0	1	CIRCULAR	0.0177	RCP	270.2		359.91		
	9 2 7	0	c	CIRCULAR	0.02642	RCP	255.97	0.37	336.33		
	i m	0	2	CIRCULAR		RCP	58.65		100.17	0.58	
	2	0	1	CIRCULAR	0.02256	CMP	6.14		10.46		
	2	0	1	CIRCULAR	0.04862	PVC	6.38		11.31		
	1.5	0	1	CIRCULAR	0.00483	RCP	0.63	0.09	1.07	0.15	
	1.3	0	T (F	CIRCULAR	0.00776	CMP	189.11		275.46		
	1.5	0	1	CIRCULAR	0.3513	RCP	3.41		5.67	0.09	
	4	0		CIRCULAR	0.01352	RCP	119.1				
	3.5	0	2	CIRCULAR	0.05692	RCP	150.22		2		
	3.5	0	7	CIRCULAR	0.02261	RCB RCD	142.84	0.47	201.6	0.67	
	3.3	0	1	CIRCULAR	0.02844	RCP	45.25				
	1.5	0	1	CIRCULAR	0.01439	RCP	0.02		0.03		
	1.5	0	1	CIRCULAR	0.04342	RCP	11.19		18.94		
	2.75	0	- 1	CIRCULAR	0.01865	RCP	33.79			0.78	
	i v	0	1	CIRCULAR	0.00575	RCP	125.48	0.6	182.86	0.93	
	1.5	0	1	CIRCULAR	0.01936	RCP	4.71				
	1.5	0	1 7	CIRCULAR	0.06851	CMP	6.44	0.7	10.7	0.3	
	2.5	0	1	CIRCULAR	0.00743	13 RCP	14.67		25.56	0.72	
	1.5	0	1	CIRCULAR	-0.01328	RCP	0.16	0.01			

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		O _{con}		
<u> </u>	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	(2-year) (cfs)	Qcon vs Qcap3	(10-year) (cfs)	Qcon vs Qcap32	(1)
	2.5	0	1	CIRCULAR	0.01465 HDPE	HDPE	16.89	0.34	32.12	0.65	
	2	0	1	CIRCULAR	0.0205	RCP	16.03				
	2	0	п	CIRCULAR	0.02143	RCP	9.33				
	7	0	T	CIRCULAR	0.01468	ABS	12.58				
	2	0	1	CIRCULAR	0.01632	RCP	8.67				
	1.5	0	1	CIRCULAR	0.00337	RCP	2.69				
	1.5	0	1	CIRCULAR	0.19239	HDPE RCP	0.62	0.01	0.96		
	1.5	0	1	CIRCULAR	0.00462	RCP	3.08				
	1.5	0	1	CIRCULAR	0.00992	RCP	3.01				
	1.5	0	1	CIRCULAR	0.01926	RCP	3.02				
	2	0	1 1	CIRCULAR	0.03828	RCP	9.27		18.38		
	2.5	0	1	CIRCULAR	0.00368	RCP	0.31				
	9	0	1	CIRCULAR	0.00103	RCP	39.88	0.29			
	w r	0	1	CIRCULAR	0.01924	RCP	39.37		70.52		
	2.3	0	1	CIRCULAR	0.03195	RCP	22.98	0.57	37.	0.93	
	2.5	0	1	CIRCULAR	0.03125	RCP	0				
	4	0	1	CIRCULAR	0.00867	RCP	62.19				
	2.5	0	-	CIRCULAR	0.11215	RCP	0.72				
	2.5	0		CIRCULAR	0.00731	ICP ICP	11.72				
	3.5	0	1	CIRCULAR	0.00581	RCP	36.26	0.47	87.42	1.14	
	1.5	0		CIRCULAR	0.01189	RCP	4.66				
	2 2 1.			CIRCULAR	0.01529	RCP BCP	7.54				
	T	0	1	CIRCULAR	0.03061	PVC	0.2				
	1.5	0	1	CIRCULAR	0.01932	RCP	4.02				
	2	0	1	CIRCULAR	0.01945	RCP	12.14				
	1.5	0		CIRCULAR	0.00379	HDPE	0.9				
	6:3	0		CIRCULAR CIRCULAR	0.00328	RCB.	16.98				
	2	0	1	CIRCULAR	0.02354	RCP	15.39				
	2	0	1	CIRCULAR		RCP	17.63		29.94		
	2.5	0	1	CIRCULAR	0.01699	RCP	17.03		29.91	0.56	
	3	0	1	CIRCULAR		RCP	28.08		42.34		
	4.3	0	T	CIRCULAR	0.00444	RCP	2.05	0.29		0.51	
	1.5	0	1	CIRCULAR	0.05891	RCP	4.23				
	1.5	0	1	CIRCULAR	0.0115	RCP	5.1		8.72		
	9 1	0	1	CIRCULAR	0.00425	RCP	152.69		267.56		
	2.5	0	1	CIRCULAR	0.05264	RCP	3.2	0.03		0.09	
	9	0	1	CIRCULAR	0.04159	RCP	2.14		16.75		
	2.5	0	1	CIRCULAR	0.05905	CONC	13.99	0.14			
	9 9	0	1 1	CIRCULAR	0.00317	CONC	14.55				
	1.5	0	1 1	CIRCULAR		RCP	8		14.17	98:0	
	9	0	1	CIRCULAR		RCP	157.37				
	4.5	0	1	CIRCULAR	0.01699	RCP	162.83				
	9	0	1 ,	CIRCULAR	0.00709	RCB	162.69	0.46	286.18	0.8	
	2.5	0	T 1	CIRCULAR	0.06048	RCP	19.31				
	2	0	1	CIRCULAR	0.02815	RCP	21.08				
	2.5	0	1	CIRCULAR	0.02162	RCP	31.7				
	2.5	0	1	CIRCULAR	0.01984	RCP	40.15		63.58	1.1	
	4 %	0	T	CIRCULAR	0.005/3 1	RCP	45.24				
	n m	0	1	CIRCULAR	0.03267	RCP	41.76				
	4	0	1	CIRCULAR	0.0209	RCP	45.55				
	9	0	7	CIRCULAR	0.0082	RCP	152.02		266.75		
	9	0		CIRCULAR	0.00995	RCP	118,11	0.28		0.5	

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		Q _{con}		
0)	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	_	Qcon vs Qcap3	<u>-</u>	Qcon vs Qcap32	(1)
	2	0	1	CIRCULAR	0.02474 RCP	RCP 3RS	10.68	0.3	18.64	0.52	
	2	0	1 1	CIRCULAR	0.01744	1DPE	14.38				
	1.5	0	1	CIRCULAR	0.01806	ЧОРЕ	1.41				
	1.5	0	1 1	CIRCULAR	0.03489	HDPE	1.4				
	1	0	1	CIRCULAR	0.1717	4DPE	1.22				
	1	0	1	CIRCULAR	0.02095	НОРЕ	6.02				
	1.75	0	E -	CIRCULAR	0.09901	RCP 3.CP	10.56				
	1.3	0	1 1	CIRCULAR	0.01308	ABS	2.41				
	1.5	0	1	CIRCULAR	0.01369	RCP	3.22				
	1.5	0	1	CIRCULAR	0.01785	CMP	3.2				
	1.5	0	1	CIRCULAR	0.02559	3CP	2.6				
	2.5	0	1	CIRCULAR	0.02648	RCP	21.75				
	2.5	0		CIRCULAR	0.03535	RCP	21.72				
	2.5	0	1	CIRCULAR	0.00711	KCP.	45.53				
	, e	0	T	CIRCULAR	0.02089	3CP	46.51	0.48			
	1.5	0	1	CIRCULAR	0.00819	CMP	1.48				
	1.5	0		CIRCULAR	0.00287	CMP	2.13	7.0			
	1 7	3		KECI_CLOSED	-0.004 0 03087	40PF	7.7				
	3.5	0	1 1	CIRCULAR	0.0312	SMP.	90:0				
	3.5	0	1	CIRCULAR	0.03948	RCP	11.45	90:0	20.43	0.1	
	5.5	0		CIRCULAR	0.00689	RCP	42.05				
	0.0	0	1	CIRCULAR	0.03258	3CP	3.39				
	1	0	T	CIRCULAR	0.00581	ABS	0.58				
	1	0	1	CIRCULAR	0.00402	ABS	3.28				
		0	1	CIRCULAR	0.04015	ABS	5.02	0.7	4.75		
	1.5	0		CIRCULAR	0.00851	KCP	7.64				
	1.5	0	T	CIRCULAR	0.01417	RCP	2.35				
	1.5	0	1	CIRCULAR	0.05023	CMP	7.37				
	2.5	0	1	CIRCULAR	0.01482	RCP	10.29	0.21			
	τ,	0	1	CIRCULAR	0.01031	RCP	3.5	0.97			
	7	0	7	CIRCULAR	0.01128	HDPE	4.58	1.21			
	1.5	0	7 17	CIRCULAR	0.08646	30	15.7	0.51	1.01	0.01	
	2	0	1,	CIRCULAR	0.00692	RCP	10.31	0.55			
	2	0	1	CIRCULAR	0.03404	RCP	18.53	0.44			
	2	0	1	CIRCULAR	0.03487	RCP	21	0.5	37.26	0.88	
	1.25	0	1	CIRCULAR	0.23812	CMP	0.48				
	4	0	1	CIRCULAR	0.01979	4CP	33.52		61.6		
	4	0	1	CIRCULAR	0.01982	RCP	33.6			0.31	
	2	0	- F	CIRCULAR	0.10128	CONC	4.13	0.06			
	0 0	0	1 1	CIRCULAR	0.0085	3CP	15.27	0.25		0.45	
	1.5	0	1	CIRCULAR	0.05279	RCP	1.59	0.07			
	8	0	1	CIRCULAR	0.05562	RCP	17.35	0.11			
	m n	0	7 7	CIRCULAR	0.00673	RCP	21.28		39.21	0.72	
	u ruk	0	7 [CIRCULAR	0.02696	3CP	23.36	0.14			
	3	0	1,	CIRCULAR	0.08306	RCP	28.93	0.15		0.28	
	3	0	1	CIRCULAR	0.02342	RCP	33.3				
	П С	0	1,	CIRCULAR	0.16796	RCP	0.12		0.18	0.01	
	1	0	1	CIRCULAR	0.3433	RCP	9.30				
	9	0	1	CIRCULAR	0.00529	3CP	20.64				
	3.5	0	2 (CIRCULAR	0.01888	RCP	187.16				
	3.5	0	2 0	CIRCULAR	0.01451	RCP	116.96	0.48	183.26	0.76	
	9	0	1	CIRCULAR	0.01415	3CP	103.63				

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		O _{con}		
G I	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material		Qcon vs Qcap3	<u> </u>	Qcon vs Qcap32	(1)
	1 2	0	1	CIRCULAR	0.0107 CMP	CMP	9.26	0.4	16.31	0.7	
	4	0	1	CIRCULAR	0.01978	RCP	36.31				
	4	0	1	CIRCULAR	0.01978	RCP	37.09				
	-	0	H +	CIRCULAR	0.04044	HDPE	3.39				
	4.5	0		CIRCULAR	0.01978	RCP	180.58				
	4.5	0	1	CIRCULAR	0.02089	RCP	180.48				
	2	0	1	CIRCULAR	0.03843	RCP	1.18				
	9 .	0	1 7	CIRCULAR	0.00764	RCP	185.65				
	1.5	0	1	CIRCULAR	0.04813	HDPE	6.98				
	1	0	1	CIRCULAR	0.02166	CONC	3.27				
	2	0	1	CIRCULAR	0.19098	HDPE	13.91				
	1.5	0	1	CIRCULAR	0.00587	RCP	3.41				
	1.3	0	T	CIRCULAR	0.00621 HDPE	HDPE	1.27	0.45	2.24		
	1	0	1	CIRCULAR	0.03881	HDPE	3.05			4 0.77	
	3	0	1	CIRCULAR	0.06375	RCP	44.03				
	1 0	0	T .	CIRCULAR	0.0075	RCP	9.00				
	1.5	0	1	CIRCULAR	177770.0	RCP	5.24				
	2.5	0	1	CIRCULAR	0.05451	RCP	27.04				
	2.5	0	1	CIRCULAR	0.03714	RCP	28.19				
	1.5	0	1	CIRCULAR	0.01976	RCP	2 02	0.07	1.93	0.13	
	2.5		1	CIRCULAR	0.00486	RCP	28.36				
	4	0	1 4	CIRCULAR	0.04831	RCP	43.54				
	4	0	1	CIRCULAR	0.00818	RCP	28.08				
	6.5	0	1	CIRCULAR	0.00854	RCP	375.28			1.27	
	1.5	0	T	CIRCULAR	0.11696	RCP	9.02	0.25			
	6.5	0	1 1	CIRCULAR	0.00849	RCP	219.74		329.47	0.68	
	6.5	0	1	CIRCULAR	0.01041	RCP	156.46	0.29			
	6.5	0	1	CIRCULAR	0.01564	RCP	156.67				
	6.5	0	1	CIRCULAR	0.00271	RCP	170.86		265.03		
	m m	6	1	RECT_CLOSED	0.03795	RCB RCB	80.01	0.17		6 1 24	
	6.5	0	1	CIRCULAR	0.00716	RCP	166.08	0.37	264.69		
	2	0	1	CIRCULAR	0.05349	RCP	0.42	0.01			
	2	0	1	CIRCULAR	0.16129	RCP	1.05	0.01		6 0.02	
	6.5	0	1	CIRCULAR	0.0284	RCP	219.13	0.25	329.4		
	6.9	0	1	CIRCULAR	0.00167	RCP	10.36	0.13	38.32		
	4.5	0	1	CIRCULAR	0.00205	RCP	11.57	0.13		8 0.45	
	c	0	1	CIRCULAR	0.00355	RCP	7.74	0.19			
	2	0	-	CIRCULAR	0.013	HDPE	4.53	0.18			
	2		1	CIRCULAR	0.01304	HDPE	4.52	81.0	79.7	7 0.16	
	6.5	0	1	CIRCULAR	0.01265	RCP	386.15	9:0	35		
	2	0	1	CIRCULAR		RCP	3.14	0.2			
	4 4	0	I	CIRCULAR	0.0489	RCP	9.34	0.03			
	4.5	0	1	CIRCULAR	0.00166	RCP	13.38			7 0.49	
	4	0	1	CIRCULAR	0.01482	RCP	63.35	0.36	106.49		
	4	0	1	CIRCULAR	0.31215	RCP	63.34				
	2	0	Н .	CIRCULAR	0.03407	HDPE	3.46				
	6.7		1	CIRCULAR	0.05257	RCP BCP	37.15				
	2 20	0	2	CIRCULAR	0.01172	RCP	24.04			60:00	
	5	0	2	CIRCULAR	0.0071	RCP	199.05	0.45	352.08		
	N V	0	2	CIRCULAR	0.01882	RCP	263.28				
	1.5	0	1	CIRCULAR	0.00941	RCP 5 RCP	310.3		462.45	1.13	
	1	0	1	CIRCULAR	0.01495	ABS	0.78	0.18			
	9	0	1	CIRCULAR	0.00877	RCP	316.91	0.81	495.78	3 1.25	

			Dir	Dimensions			2	2-year	10	10-year	
	D' or H'						Q _{con}		Q _{con}		
6 1	(diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material		Qcon vs Qcap3	Ē	Qcon vs Qcap32	(1)
	1 2 5	0	1 0	CIRCULAR	0.05965 ABS	ABS	0.93	0.11		0.17	
	1.5	0	1 [CIRCULAR	0.04842	CMP	7.52				
	1.5	0	1	CIRCULAR	0.07663	CMP	21.89				
	w	4.6		CIRCULAR	0.00429	RCP	53.7				
	2.3	0	1 1	CIRCULAR	0.02019	CMP	1.44				
	2.5	0	1	CIRCULAR	0.03182	RCP	11.99				
	2.5	0	1	CIRCULAR	0.02222	RCP	15.4				
	2 2	0	1	CIRCULAR	0.02762	RCP	19.59				
	1.5	0	7 17	CIRCULAR	0.01657	RCP	4.56				
	2	0	1	CIRCULAR	0.01262	RCP	15.11	0.59	26.86		
	1.5	0	1	CIRCULAR	0.08025	CMP	3.38				
	m m	0	1	CIRCULAR	0.02419	RCP	67.79				
	2	0	1 [CIRCULAR	0.00207	RCP	127.1	1.07	183.98		
	1.25	0	1	CIRCULAR	0.10592	RCP	1.08				
	5	0	17	CIRCULAR	0.01039	CMP	126.26				
	2.5	0	T	CIRCULAR	0.001/4	KCP RCP	59.96				
	2.3	0	7 17	CIRCULAR	0.03132	RCP	75.79				
	3	0	1	CIRCULAR	0.04937	RCP	8.13	0.05		0.09	
	1	0	1	CIRCULAR	0.07018	HDPE	96:0				
	6.5	0	1	CIRCULAR	99600.0	RCP	317.33				
	1 ×	0	T	CIRCULAR	0.03/32	HUPE	0.63		1.0.1		
	0 0	0	1 1	CIRCULAR	0.01672	RCP	112.98				
	3.5	0	1	CIRCULAR	0.55138	RCP	0.79				
	9	0	1	CIRCULAR	0.02255	RCP	107.16		20	0.33	
	5.5	0	H -	CIRCULAR	0.05594	KCP	3.9				
	2.5		1 1	CIRCULAR	0.00685	RCP	6.78	0.00	14.89	0.44	
	2.75	0	1	CIRCULAR	0.02432	CMP	15.27				
	1.5	0	1	CIRCULAR	0.04093	RCP	10.27				
	1.5	0	1	CIRCULAR	0.16428	CMP	3.43		6.14		
	2 1	0	e e	CIRCULAR		RCP	79.78	0.55		1.21	
	1.5	0	1	CIRCULAR	0.03428	CMP	0.03				
	1	0	1 1	CIRCULAR	0.0673	CONC	0.7		1.2		
	2.5	0	1	CIRCULAR		CONC	10.28			0.31	
	4	0	1	CIRCULAR	0.03621	RCP	119.53	0.44	165.45		
	2	0	7	CIRCULAR	0.06139	RCP	9.23			0.33	
	8	0	T T	CIRCULAR		CONC	8.96	0.1	14.77	0.2	
	1.5	0	1	CIRCULAR	0.04998	RCP	0.24				
	3	0	1	CIRCULAR	0.20008	RCP	2.67				
	2.5	0	T .	CIRCULAR	0.07002	CONC	23.12	0.21	31.21	0.29	
	2.5	0	1	CIRCULAR	0.04492	CONC	16.38				
	1.5	0	1 1	CIRCULAR	0.01469	HDPE	4.01		6.87		
	2.5	0	1	CIRCULAR	0.02426	RCP	24.53				
	1.5	0	1	CIRCULAR	0.10623	RCP	4.3				
	2.5	0	T	CIRCULAR	0.04233	RCP	24.28	0.29	40.64	0.48	
	1.5	0	1 -	CIRCULAR	0.08841	RCP.	8.48				
	1.5	0	1 1	CIRCULAR	0.07287	RCP SCP	7.19			0.45	
	3	0	1	CIRCULAR	0.01118	RCP	24.09				
	3	0	1	CIRCULAR	0.00616	RCP	23.5		40.21		
	3 2 2 2	0	T	CIRCULAR	0.01387	RCP	31.04				
	1.5	0	1 [CIRCULAR	0.10761	RCP	19.02	0.55		86:0	
	1.5	0	1	CIRCULAR	0.01317	RCP	4.47				
	2.5	0	1	CIRCULAR	0.07204	RCP	16.04		2		
	1.5	0	1	CIRCULAR	0.04634 CMF 0.03611 RCP	CMP RCP	2.46	0.2	4.39	0.35	

			Dir	Dimensions			2	2-year	10	10-year	
6)	D' or H' (diameter) or (height)	B' (width) Barrels	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap32	(1)
	3	0	1	CIRCULAR	0.33922 CMP	CMP	19.27	0.09	33.52	0.16	
	4	0	1	CIRCULAR	0.02456 RCP	RCP	78.07	0.35	131.69	65'0	
	3	0	1	. CIRCULAR	0.04727 RCP	RCP	44.03	0.3	84.98	65'0	
	1.5	0	1	CIRCULAR	0.10367 RCP	RCP	5.26	0.16	8.96	0.26	
	1.5	0	1	CIRCULAR	0.07684 RCP	RCP	6.52	0.22	11.27	68.0	
	1.5	0	1	CIRCULAR	0.02637 RCP	RCP	6.77	0.4	11.67	89:0	
	2	0	1	CIRCULAR	0.02899 RCP	RCP	3.5	60.0	5.69	0.15	
	2	0	1	CIRCULAR	0.00558 RCP	RCP	7.04	0.42	12.13	0.72	
	2	0	1	CIRCULAR	0.02137 RCP	RCP	7.53	0.23	12.1	LE:0	
	1	0	1	CIRCULAR	0.05591 AC	AC	3.7	0.44	6.79	18.0	

			2	IIIEIISIOIIS			6-7	cal	OT	'yeal	
Q	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
1	1		1	CIRCULAR	0.51503	CMP	0	0			
1	30	20	1	RECT_OPEN	0.00662		0	o			
89	ις i		1	RECT_CLOSED	0.00155	RCB	617.05	1.12	923.17	1.67	
187	v c	IP	I	CIRCLI CLOSED	0.0104	000	9.05	0.44			
18/	5.5			CIRCULAR	0.01427 RCP	RCP RCP	8.03	1.0			
	0	0	1	IRREGULAR	0.09333	Earthen	4.81	0		0	
	4		1	CIRCULAR	0.08121	RCP	0	0		0	
	1	3	1	PARABOLIC	0.27746		1.78	0.02		0.53	
	8				0.28107		6.94	0.02		0.03	
	3.5	30 0		CIRCULAR RECT OPEN	0.03785		289.03	0.49	408.32	0.7	
	4			RECT CLOSED	0.01601	RCB	295.61	0.53	40	0.73	
	4		1	RECT_CLOSED	0.05066 RCB	RCB	296.94	0.3	40	0.41	
	30		1	RECT_OPEN	0.3131		43.09	0			
	30		1	RECT_OPEN	0.76122		2.01	0	3.34		
	30			RECT_OPEN	0.01627		260.03	0.01		0.01	
	30		1 1	CIBCLILAR	0.0104	RCP	1 48		2.8	0.21	
	8		1 [CIRCULAR	0.2311	RCP	5.2				
	2	20	1	TRAPEZOIDAL	0.01244		25.02	0.13			
	3.5		1	CIRCULAR	0.02399	RCP	9.17				
	2	0	1	CIRCULAR	0.00681	RCB	117.73		205.8	0.96	
	7		1	CIRCULAR CIRCUII AB	0.02/3	CIMIP	14.86				
	2		1	CIRCULAR	0.02/1	RCP	14.63	0.39			
	1.5		1	CIRCULAR	0.08918 RCP	RCP.	9.73				
	1		1		0.10366	Other	0.01				
	1		1		0.10304	Other	5.01	0.3	7.89	0.53	
	1	0	1	CIRCULAR	0.6801	Other	2.81				
	2		1		0.07777	CMP	8.24	0.24	14.56	0.43	
	2		1	CIRCULAR	0.06256	Concrete	0.71				
	1		1	PARABOLIC	0.01685 Other	Other	69.0		1.23	0.05	
			T	CIRCULAR	0.01072	Concrete	11.34	0.16			
	5		1 -	PARABOLIC	0.00397	Concrete	15.43				
	2		T	CIRCULAR	0.0109	Other	15.62	99:0		1.13	
	2		1	CIRCULAR	0.00912 Concrete	Concrete	0.59	0.02		0.05	
	1		1	PARABOLIC	0.03543	Other	0.59	0.02		0.03	
	2		1	CIRCULAR	0.00314	CMP	2.51	0.37		0.57	
	2		1	CIRCULAR	0.03297	CONC	0	0	0	0	
	2 2 5		7 1	CIRCULAR	0.05453	CONC	12.78			0 0	
	5.5		T	CIRCULAR	0.01107	CONC	7.28		12.58	0.53	
	2	0	1	CIRCULAR	0.00682	CONC	2.66	0.14		0.24	
	2		1	CIRCULAR	0.00684	CONC	2.95		4.82	0.26	
	2		1	CIRCULAR	0.00871	CONC	2.58	0.12		0.2	
	2	0	1	CIRCULAR	0.00682	CONC	5.47			0.48	
	1		1		0.00788	CONC	0.93		1.47	0.46	
	2.5		1	CIRCULAR	0.00683	CONC	14.19			0.71	
	1.5		1	CIRCULAR	0.08322	CONC	1.09	0.04			
	2.5		3	CIRCULAR	0.01994	RCP	45.23	0.26	77.41		
	1.5	0	c c	CIRCULAR	0.00648 CONC	CONC	1.61	0.19		0.31	
	6.2		T	CIRCUI AR	0.07643	CONC	1,77	0.03	30.4	0.00	
	2	0	1	CIRCULAR	0.00619	CONC	1.21	0.07			
	2		1	CIRCULAR	0.09982	CONC	28.83	0.4	50.59		
	3.5		1	CIRCULAR	0.00565	CONC	22.15	0.29			
	3.5	0	1	CIRCULAR	0.00683	CONC	47.66	0.57	73.4	0.88	
	7	0	T	CIRCULAR	0.0/78	CONC	13.08	0.21			
	7		T	CINCOLAIN	0.3200		13.1	1.0			

			۵	IIIIEIISIOIIS			6-7	eal	OT	-year	
O	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	2.5	2	1	CIRCULAR	0.03688	CONC	36.12	0.46	71.61	0.91	
	1.5			CIRCULAR	0.49848	CONC	13 61	0			
	7	2		CIRCIII AR	0.11358	RCP	13.51				
	4	0 0		CIRCULAR	0.0126	3CP	52.51				
	5		1	CIRCULAR	0.00215	RCP	54.06	0.45	94.77	0.79	
	.7		1	CIRCULAR	0.23773	CONC	1.63				
	14	2 0	1		0.26307	CONC	0.91				
		3		IRREGULAR	0.49541	Other	0 1 02	0			
	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		1 -	CIRCUIAR	0.28415	RCP	1.0/	0.0	1.83	0.02	
	1.5		1		0.08175	3CP	2.56				
	1.5		1	CIRCULAR	1 2660:0	RCP	2.55				
	1.5	5	1	CIRCULAR	0.03039	RCP	2.51			0.24	
	1.5		, ,	CIRCULAR	0.01047	RCP	3.21				
	J.5			CIRCILIAR	0.01185	RCP	3.46		34.04		
	1.5		1	CIRCULAR	0.02159	3CP	6.4				
	1.5		1	CIRCULAR	0.12254	ACP .	1.26				
	1.5		1	CIRCULAR	0.00459	RCP	5.43				
	1.5		1	CIRCULAR	0.05928	RCP	12.79				
	1.5		4	CIRCULAR	0.00862	RCP	11.88				
	1.5			CIRCULAR	0.02045	RCP	12.92	0.86	15.99		
	1.5			CIRCULAR	0.00852	3CP	0.55				
	1.5		1	CIRCULAR	0.08713	RCP	1.12				
	1.5		1	CIRCULAR	0.01599	RCP	2.3			0.31	
	3.5		1		0.02105	RCP	112.84	0.77	11		
	1.5		1	CIRCULAR	0.01148	RCP	4.64	0.41			
	1.5		1	CIRCULAR	0.08919	RCP	18.4	0.59			
	7			CIRCULAR	0.28995	RCP	20.09	0.17			
	1	1 3	1	PARABOLIC	0.14718	Concrete	1.65	0.03			
	2.5		1	CIRCULAR	0.0249	CONC	23.94	0.37			
	1.5		1	CIRCULAR	0.00374	CONC	1.61				
	1.5		1	CIRCULAR	0.25101	CONC	1.93		3.15	0.00	
	17 (2 0		CIRCULAR	0.07585	CONC	12.79				
	4		1 -	CIRCIII AR	0.01	3CP	1.34				
	2	2 0		CIRCULAR	0.08003	3CP	2.26			90:0	
	2		1	CIRCULAR	0.06722	RCP .	2.27				
	7		1	CIRCULAR	0.50682	RCP	0.27				
	. 1		-	CIRCULAR	0.06722	RCP	2.02				
	7 0	2 2 0		CIRCULAR	0.06/27	RCP	0.53	0.01	1.22	0.02	
	2		1	CIRCULAR	0.05805	3CP	69.0				
	3		1	CIRCULAR	0.01895	RCP	4.9				
	4	4 0	Α,		0.0126	CONC	63.83		۵		
	7	2	T	CIRCILLAR	0.05673	CONC	0.20	71.0	0.41	0.01	
	2			CIRCULAR	0.00813	CONC	0.32				
	2		1	CIRCULAR	0.28118	CONC	0.31		0.5		
	2		1	CIRCULAR	0.0076	CONC	1.77	60:00			
	2	2 0	1	CIRCULAR	0.03135 CONC	CONC	2.04	0.05			
	2	2 0	+	CIRCULAR	0.0303	CONC	2.6	0.07	4.19	0.11	
	7			CIRCULAR	0.00764	CONC	2.19				
	7	2	7	CIRCULAR	0.04885	CONC	6.35				
	2			CIRCULAR	0.0155	3CP	1.12				
	4		1	CIRCULAR	0.05904	CONC	48				
	2	2 0	1	CIRCULAR	0.34511	CONC	10.53	0.08	17.56	0.13	
	2		1	CIRCULAR	0.00922	CONC	9.97				

			5	IIICIINIOIIN			λ-7	מפו	7	-year	
O	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	4		1	CIRCULAR	0.00596 RCP	RCP	120.63	1.09	162.1	1.46	
	0	0	1	IRREGULAR	0.26594	Other	0.04				
			1	PARABOLIC	0.17654	Other	0.1	0			
		m 0		PARABOLIC	0.03167	Other	1.05	0.04	1.67	0.06	
	7			CIRCLILAR	0.01884	CONC	1 49	0.01			
	2		1 (CIRCULAR	0.01155	CONC	1.97	90.0	3.12	0.13	
	2			CIRCUIAR	0.00646	CNO	0.28	0.00			
	4		1	CIRCULAR	0.05241	CONC	43.09	0.13			
	2		1	CIRCULAR	0.06713	CONC	1.39	0.02			
	4	0	1		0.04016	CONC	43.11	0.15	54.1	0.19	
	2		1	CIRCULAR	0.27741	CONC	41.88	0.35			
	2		1	CIRCULAR	0.07911	CONC	1.14	0.02	1.75		
	2		1		0.02972 CONC	CONC	40.11	1.03		1.27	
	2		1	CIRCULAR	0.15393	CONC	0.48				
	2		1	CIRCULAR	0.08633	CONC	0.48				
	7		T	CIRCULAR	0.029/3	CONC	40.15				
	7		1	CIRCULAR	0.01295	CONC	0.32				
	2		1	CIRCIII AR	0.15413	CONC	3.47				
	2		+ +	CIRCULAR	0.02973	CONC	36.19				
	2		1	CIRCULAR	0.02972	CONC	3.7				
	2.5		1	CIRCULAR	0.045	CONC	30.77				
	2.5		1	CIRCULAR	0.03859 CONC	CONC	1.66		2.8	0.03	
	2		1	CIRCULAR	0.00554	CONC	3.91				
	2		1	CIRCULAR	0.00355	CONC	3.9				
	1		1	CIRCULAR	0.00272	CONC	4.03	2.17			
	Τ .		1		0.02845 1	HDPE	1.34	0.22		0.38	
	2		1		0.00117	CONC	4.31	0.56			
	7		I	CIRCULAR	0.00117	CONC	4.56				
	6		1	CIRCUIAR	0.017	CONC	77 71		15.07		
	2.5		1 1	CIRCULAR	0.0017	CONC	21.43	1.53		2.23	
	2.5		1	CIRCULAR	0.22562	CONC	8.79				
	2.5		1	CIRCULAR	0.00514	CONC	9	0.2	10.68		
	2.5		1	CIRCULAR	0.00118	CONC	22.33				
	2.5		1	CIRCULAR	0.00118	CONC	22.48		33.39	2.37	
	2.5		1	CIRCULAR	0.00117 CONC	CONC	23.37				
	1.5		T	CIRCULAR	0.03128	RCP	4.5				
	2.5		1	CIRCULAR	0.00118	CONC	27.31				
	4.5		II I	CIRCULAR	0.00118	CONC	155.04				
	6.5		1 1	CIRCIII AR	0.00111 CONC	CONC	178.42	0.02	0.91	3.82	
	2		1	CIRCULAR	0.01325	CONC	0.66				
	2		1	CIRCULAR	0.16198	CONC	0.81				
	2		1	CIRCULAR	0.0143	CONC	0.48				
	2		1	CIRCULAR	0.00604	CONC	0.52				
	1.5	0 0	1 [CIRCULAR	0.27.246 RCP 0.08137 RCP	3CP	0.05	000	0.1	0 0	
	2.5		1		0.14974	CONC	16.74				
	2		1	CIRCULAR	0.0177	RCP	13.52				
	0		1	IRREGULAR	0.11937	Concrete	3.18	0	5.22	0	
	4		1	CIRCULAR	0.03075	CONC	0	0			
	2	0	1	CIRCULAR	0.04315 R	RCP	11.01			0.41	
	2		1	CIRCULAR	0.11215 RCP	RCP	19.48	0.26	34.82		
	9		1	CIRCULAR	0.00902	RCP	103.69				
	0.5	9 0		TRIANGULAR	0.00689	CONC	0.29			0.13	
	1.			PARABOI IC	0.0100	Concrete	04:00				
	6		T	CIRCUI AR	0.01578	ACP ACP	12.94				
	2 2	0	1	CIRCULAR	0.36589 RCP	RCP	12.95	60.0	22.74	0.17	
	2		1	CIRCULAR	0.31957	ACP 8CP	12.95				

			۵	IIIIEIISIOIIS			Á-7	eal	OT	-year	
ū	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	3	3	1	CIRCULAR	0.01035	CONC	24.74		41.75		
	(3	T .	CIRCULAR	0.03263	RCP	50.65				
	2.5			CIRCULAR	0.14147	RCP	50.7				
	2.3	200		CIRCULAR	0.06107	RCP RCP	48.3				
	1.5		T	CIRCULAR	0.02665	RCP	3.35	0.2		0.34	
	2		1	CIRCULAR	0.00693	RCP	1.58				
	1.5		1	CIRCULAR	0.00944	RCP	9.81				
	4			CIRCULAR	0.033	RCP	2.21				
	1.5			CIRCILIAR	0.04284	RCP.	9.1	0.14	5.45		
	1.5	0 0	1	CIRCULAR	0.0756	RCP	9.82			0.03	
	1.5		1	CIRCULAR	0.01109	RCP	0.75				
	1.5		1	CIRCULAR	0.01744	RCP	5.06				
	1.5		T	CIRCULAR	0.0543	RCP	4.91				
	1.5		,	CIRCULAR	0.05521	RCP	1.63				
	1.5			CIRCULAR	0.03164	RCP	24.03				
	2			CIRCULAR	0.07428	RCP	69.6				
	2.5		1	CIRCULAR	0.03291	RCP	46.6				
	1.5		I	CIRCULAR	0.06934	RCP	1.37				
	1.5		1	CIRCULAR	0.16109	RCP	1.4				
	1.5			CIRCULAR	0.08181	RCP	9.1	0.3	15.85	0.53	
	1.5			CIRCUIAR	1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	RCP	3.1				
	1.5			CIRCULAR	0.08591	RCP	2.24	20:0			
	1.5	0	1	CIRCULAR	0.03075	RCP	2.21				
	2.5		1		0.01501	RCP	37.03	0.74)	1.26	
	2.5		1	CIRCULAR	0.02163	RCP	37.58				
	1.5		1	CIRCULAR	0.0869	RCP	4.98		8.82	0.28	
	1.5				0.01913	RCP BCB	4.93				
	L.5		1	CIRCULAR	0.0049	RCP	2.73				
	7.1			CIRCUIAR	1 923500	RCP	4 18	0.27			
	1.5			CIRCULAR	0.02315	RCP	2.22		3.91	0.24	
	1.5		1	CIRCULAR	0.03348	RCP	2.21	0.11			
	2		1	CIRCULAR	0.05196	RCP	24.63		41.83		
	2		1	CIRCULAR	0.05642	RCP	11.45				
	1.5		1	CIRCULAR	0.47787	RCP	1.18	0.0		0:0	
				IRREGULAR	0.02075	Earthen	25.75				
	0	0	T	IRREGULAR	0.01689	Earthen	24.28	0	31.47	0	
	D		I	IRREGULAR	0.15145	Earthen	0.27				
			1	IRREGULAR	0.17542	Earthen	4.25			0	
			~ (·	IRREGULAR	0.28537	Earthen	3.39				
	0			CIRCLILAR	0.17845	BCP	1 28	200	27 04	0 0	
	2.5	5	1	CIRCULAR	0.02463	RCP	25.76				
	2.5		1		0.00989	RCP	25.79		34.12	0.84	
	2.5		-	CIRCULAR	0.03491	RCP	25.66				
	1.5		-	CIRCULAR	0.01894	RCP	1.97	0.14	3.5	0	
	1.5			CIRCIII AR	0.03062	Concrete	2 42	0 0			
	1.5	0		CIRCULAR	0.24242	RCP	4.25	80.0	7.89		
	1.5		1	CIRCULAR	0.02704	RCP	4.07	0.24			
	1.5		1	CIRCULAR	0.0339	RCP	0.78	0.04			
	1.5		1	CIRCULAR	0.15238	RCP	3.4		6.32	0.15	
	1.5			CIRCULAR	0.01441	RCP	0.0				
	1.5			CIRCULAR	0.01153	RCP	19.33				
	1.5	2 0	1	PARABOLIC	0.06287	Concrete	0.57	0.01	0.47	0.02	
	1.5			CIRCULAR	0.02156	RCP	19.7				

			٥	IIIIEIISIOIIS			6-7	eal	OT	-year	
Q	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	1.5		1	CIRCULAR	0.01689	RCP	20.21	1.48	22	1.61	
	1.5		1	PARABOLIC	0.01841	Concrete	1.06				
		2 0	1	IRREGULAR	-0.17256	Earthen	0	0			
	1.5	0 0		CIRCULAR	0.0145	RCP	15.25		16.99	1.34	
	1			CIRCULAR	0.00792	RCP BCD	T. 66	0.00			
	1.5	0 0	1 6	CIRCULAR	0.0085	PCP PCP	10.05	0.0	11.31		
	L.5		1	CIRCULAR	20000	NCP.	SU.UI	1.04			
	1.5	2		CIRCULAR	0.028	RCP	0.2 A 36	0.10	5.65	0.35	
	1.5			CIRCULAR	0.00488	NCP NCP	4.30	0.44			
	1.5	2 6	1		1034	RCP	1.73	0.09	2 98		
	1.5				0.03202	RCP	1.1	90:0			
	1.5		1	L CIRCULAR	0.02974	RCP	2.8	0.15			
	1.5	5 0	1	CIRCULAR	0.13965	RCP	0.53			0.05	
	1.5		1	CIRCULAR	0.02338	RCP	0.62		1.09		
	1.5		1	CIRCULAR	0.06495	RCP	2.84				
	1.5		,	CIRCULAR	0.11492	RCP	0.7				
	1.5		I	CIRCULAR	0.05558	KCP BCD	21.09				
	TUS		T	CIRCULAR	0.038T/	ACP.	3.29				
		1	1	CIRCULAR	0.00788	RCP	0.99				
	1.5		1	CIRCULAR	0.01289	RCP	13.02				
	1.5		1	CIRCULAR	0.01166	RCP	11.85				
	1.5	5	1	CIRCULAR	0.04832	RCP	1.11		2.16		
	1.5		1	CIRCULAR	0.02709	RCP	3.29				
	1.5		1	CIRCULAR	0.08051	RCP	4.39				
	1.5		1	CIRCULAR	0.22803	RCP	0.56				
	1.5		1		0.00923	RCP	9.24				
	1.5		1	CIRCULAR	0.12857	RCP	0.99				
	1.5		1	CIRCULAR	0.07572	RCP	0.99	0.03			
	1.5			CIRCULAR	0.15911	RCP	1.37	0.03	77.7		
	4.5		1 6	CIRCULAR	0.11242	COINC	3.79	1.03		0.07	
	. T		-	CIRCULAR	0.0122	NCF RCD	14:71	1.0/		010	
	1.5	2		PARABOLIC	0.0001.0	Concrete	4:00	0			
	1.5			PARABOLIC	0.02817	Concrete	0	0			
	1.5		1	PARABOLIC	0.01189	Concrete	0	0			
	1.5		1	PARABOLIC	0.04384	Concrete	0	0		0	
	1.5		1	PARABOLIC	0.02529	Concrete	0	0	0	0	
	1.5	5 3	1	PARABOLIC	0.03361	Concrete	0	0		0	
	1.5		1	PARABOLIC	0.02587	Concrete	0	0		0	
	1.5			PARABOLIC	0.02739	Concrete	0	0	0	0	
	7.5			PARABOLIC	0.31866	Concrete	0				
	1.5	5	1	PARABOLIC	0.09845	Concrete	0.57	0.01	8.0		
	1.5		1	. PARABOLIC	0.10003	Concrete	1.05	0.02			
	1.5		1	PARABOLIC	0.01024	Concrete	1.05	0.06		0.1	
	1.5					Concrete	0.05	0	0.08		
	2.5		1	TRIANGULAR	0.25461	Concrete	20.21	60:0		0.0	
	1.5		1	CIRCULAR	0.37845	RCP	0	0		0	
	2.5		1	CIRCULAR	0.16515	RCP	25.61	0.1		0	
	1.5		1	. CIRCULAR	0.50056	RCP	0.16				
	2.75	5 0	1	CIRCULAR	0.05563	RCP	23.12			0.24	
			1	CIRCULAR	0.09183	RCP	0.8	0.0	2.29		
			1	. IRREGULAR	0.07956	Earthen	1.32				
		0	τ (IRREGULAR	0.16629	Earthen	2.01	0	6.18		
	27.0		1	TRIANGIIIAR	0.15218	Concrete	7.81				
	0.75			TRIANGULAR	0.04742	Concrete	0				
	0.75	3.5	T	TRIANGULAR	0.02011	Concrete	0	0	0		
	0.75		1	TRIANGULAR	0.04443	Concrete	0	0		0	
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Ð	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	2		1	CIRCULAR	0.30285 CMP	CMP	1.36				
	2	2 0	1	CIRCULAR	0.19298	CMP	0.7	0.01			
	2	0	1	CIRCULAR	0.36985	CMP	1.96				
	2	0	1	CIRCULAR	0.19881	CMP	0.19				
	2	0 0	1	CIRCULAR	0.26796	CMP	0.65	0.01	2.11		
	2	0 0	1	CIRCULAR	0.35933	CIVIP	7 1 13				
	7				0.303/8	CIVIP	T. T.		5.40		
	0 75	3.5 0	1	CIRCULAR TRIANGIII AR	0.00414	Concrete	184.62	0.68		1.24	
	0.75				0.03242	Concrete	0.57	0.06		0.26	
	0.75				0.02978	Concrete	0			0	
	2	0 0	1	CIRCULAR	0.29986	CMP	1.51				
	2	2 0	1		0.03612	RCP	33.78		61.45		
	2	0			0.02814	RCP	22.18	0.58		1.05	
	7		₹ ₹	CIRCULAR	0.02642	RCP	32.67				
	1.5	0	П .	CIRCULAR	0.00984	RCP	3.47		6.21		
	6.1.		1	CIRCULAR	0.04388	RCP RCP	4.63				
	2		+ +	CIRCULAR	0.02862	RCP.	7.6				
	1 4	0	1	CIRCULAR	0.00466	RCP	39.15		70.89		
	1.5	0	1	CIRCULAR	0.02792	RCP	0				
	1.5		1	CIRCULAR	0.02613	RCP	3.07				
	2	0	1	CIRCULAR	0.23975 CONC	CONC	21.4	0.19	37.08	0.33	
	7		1	CIRCULAR	0.01058	CONC	3.84				
	6.5		T	CIRCULAR	0.01/39	CONC	25.34				
	2	0 0	T (T		0.0284	CONC	1.24				
	2				0.09169	RCP	8.94	0.13			
	2				0.01802	RCP	1.67	90.0	2.89		
	2.5		1	CIRCULAR	0.03052	RCP	35.41	0.49			
	4				0.00253	RCP	38.75	0.54	67.13		
	0		1	IRREGULAR	0.0394	Earthen	10	0			
	0 0		1	IRREGULAR	0.01044	Earthen	17.15	0	25	0	
			ਜ ਦ	IRREGULAR	0.04285	Earthen	3.34				
			T	IRREGULAR	0.06107	Earthen	2.68				
	0	0	1	IRREGULAR	0.05/29	Farthen	I.I9		1.96		
	0		τ	IRREGULAR	0.00107	Earthen	6.1	0.01		0.03	
	0		1	IRREGULAR	0.13612	Earthen	5.85				
	0		1	IRREGULAR	0.02861	Earthen	14.92	0		0	
	0		1	IRREGULAR	0.01535	Earthen	16.27	0	22.35		
			1	IRREGULAR	0.08393	Earthen	10.89				
	1.5	0	1	CIRCULAR	0.01602	CONC	13.07				
	1.5		1	CIRCULAR	0.004250	CONC	10.89	1.55	21.26	1.0.7 3.03	
	1.5		1	CIRCULAR	0.05136	RCP	4.01				
	2.5		1	CIRCULAR	0.08958	RCP	31.24	0.25			
	2.5		1	CIRCULAR	0.04171	0.04171 RCP	19.12	0.23	35.68		
	1.5		τ .		0.7111	RCP	22.14	0.25			
	1.5	0	1	CIRCULAR	0.02932	RCP	T.3	0.0		0.12	
	1.5		T (CIRCUIAR	0.11704	SCP SCP	3.55	0.00	5.98		
	1.5		1	CIRCULAR	0.0505	RCP	19.62	0.83			
	1.5		1	CIRCULAR	0.03914	RCP	6.25	0.3		1.06	
	2.5		1	CIRCULAR	0.03719	RCP	17.08				
	2.5		1	CIRCULAR	0.07908	RCP	31.3				
	1.75		1	CIRCULAR	0.01023	RCP	10.03	0.63	15.48		
	1.75	0	, 1	CIRCULAR	0.04099	RCP	5.85	0.18			
	4.5		П	CIRCULAR	0.01555	KCP BCD	224.32	0.91	261.46		
	2.25		1	CIRCULAR	0.02797	CONC	22.08	0.05		0.09	
	1.5	0	1	CIRCULAR	0.04374	RCP	13.92	0.63	25.14	1.14	

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O	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	2		1	CIRCULAR	0.01622	RCP	2.42	0.08	3.82	0.13	
	1.5	5	T T	CIRCULAR	0.0333	RCP	5.07	0.26			
				CIRCULAR	0.2531	HDPE	10 0	0		0	
	2.5	0 0		CIRCUIAR	0.023346	3CP	1.25 78.77	0.02	2.32	50.0	
	2	2	1	CIRCULAR	0.15358	4CP	0	0			
	2		1	CIRCULAR	0.07147	RCP	0	0			
	3.5		1	CIRCULAR	0.00541	RCP	92.62	1.25		17'	
	3.5	2	[CIRCULAR	0.00895	RCP	92.62	0.97	110.2	-i	
	0	2 0 0		CIRCULAR	0.02458	3CP	0 54	0 0	96 0		
	2	2 0		CIRCULAR	0.05318	RCP	0.53	0.01		0.02	
	2		1	CIRCULAR	0.00612	RCP	5.93	0.33			
	1.5		1	CIRCULAR	0.0664	RCP	0.76	0.03			
	. 4 ((-	CIRCULAR	0.02	RCP	0	0			
	7	2 0		CIRCULAR	0.0095	KCP 3CB	0	0	0		
	2			CIRCULAR	0.00971	3CP	4.34	0.19			
	2			CIRCULAR	0.08472	SP SP	15.35	0.43			
	2	2 0	1	CIRCULAR	0.00958	3CP	4.33	0.2	7.61	0.34	
	2		1	CIRCULAR	0.02473	RCP	4.33	0.12			
	2		1	CIRCULAR	0.00383	RCP	7.84	0.56	13.88		
	7	2 0	1	CIRCULAR	0.03044	RCP	0	0			
	7		7	CIRCULAR	0.06465	RCP	0	0			
	1.5		T	CIRCULAR	0.04035	RCP	0	0			
	9	0		CIRCULAR	0.00279	3CP	22.51	0.1	106.9	70	
			1		0.08941	RCP	10.29	0.05			
	3		1		0.0074	RCP	10.33	0.18			
	4	4 0	1	CIRCULAR	0.02767	RCP	35.44	0.15			
	4		1		0.02594	RCP	36.23	0.16	53.77	0.23	
	1.5		1	CIRCULAR	0.03249	RCP	7.39				
	7		1	CIRCULAR	0.2143	RCP	1.02		1.65		
	2.5		(1)	CIRCULAR	0.00377	CONC	15.43				
	2.5		c 1		0.00524	CONC	15.39				
	7 7 7			CIRCIII AR	0.00246	RCP	412.83			0.37	
	T			CIRCULAR	0.03745	ABS	0.77				
	1	1	1	CIRCULAR	0.06325	ABS	0.67				
	1	1 0	1	CIRCULAR	0.07322	RCP	3.43				
	1		1	CIRCULAR	0.04763	ABS	2.1				
	1.5		1	CIRCULAR	0.0246	RCP	5.91				
				CIRCULAR	0.0277	ABS	5.66				
	0	0		IRREGULAR	0.01811	Earthen	70:00	0.01	891.94	0.14	
	0		1	IRREGULAR	0.01811	Sarthen	674.18				
	0	0 0	1	IRREGULAR	0.01793	Earthen	665.81	0.2	886.86		
	2		1	CIRCULAR	0.05628	HDPE	3.1				
	6.5	0 0	T (CIRCULAR	0.00964 K	RCP	330.59	0.64	510.01		
				CIRCULAR	0.01271	RCP	50.82	0.68		0.81	
	5.5		1	CIRCULAR	0.00637	RCP	216.48	0.81			
	3	3 0	1	CIRCULAR	0.02425	CONC	80.6	0.09			
	2	2 0	1	CIRCULAR	0.2784	RCP	0.72	0.01	1.27	0.01	
	1.5		1	CIRCULAR	0.03165	RCP	2.15	0.12			
	11.			CIRCULAR	0.14235	KCP.	1.79	0.05			
		0 0		CIRCULAR	0.02113	ABS	0.92	0.18	1.53	0.3	
	1 7			CIRCLILAR	0.08778	5 0	0.36	0.18			
	9			CIRCULAR	0.07526	3CP	0.220	0			
	4	8 8	1	RECT_CLOSED	0.02111 F	RCB	237.43	0.37	270.27	0.42	
	1.5		1	CIRCULAR	0.19522	RCP	6:39	0.14			

			٥	IIITEIISIOIIS			Á-7	eal	OT	-year	
ū	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
		1 0	1	CIRCULAR	0.0057	RCP	0.02	0.02			
	1.1	.5	1	CIRCULAR	0.13779	RCP	5.7				
	3.5	2	1	CIRCULAR	0.03992	RCP	53.15			0.76	
		9	1	CIRCULAR	0.0133	RCP	122.04				
				CIRCULAR	0.00365 F	RCP	118.66	0.75		1.11	
				CIRCUIAR	0.00391	3CP	239.47				
		0	1 (CIRCULAR	0.00341	NCP OCB	240.45				
			1	CIRCULAR	0.01571	ACP.	152.91		270.13		
			1		0.02475	RCP	98.43				
			1		0.00709	RCP	101.98	0.47			
	3.5	5 0	1	CIRCULAR	0.0077	RCP	53.29			1.26	
	3.5	2	1	CIRCULAR	0.03572	RCP	96.18	0.51			
		0 0	-	CIRCULAR	0.01468	RCP	9.3				
	30 1			CIRCULAR	0.06052	KCP	12.71				
	1.25			CIRCULAR	0.0109	HDPE	0.65	0.1	1.06		
	1.2			CIRCUIAR	0.0342	HDPF	2.85				
	1.2			CIRCULAR	0.04641	HDPE	1.06				
	1.25		1	CIRCULAR	0.01048	НОРЕ	1.85				
			1	CIRCULAR	0.03596	RCP	0.17				
	2		1	CIRCULAR	0.01075	RCP	528.97				
	1.5		1	CIRCULAR	0.1456	RCP	2.15	0.05	3.62	0.09	
	1		1	CIRCULAR	0.01633	RCP	2.51				
	1.5			CIRCULAR	0.0151	RCP	2.5	0.19			
	1.5			CIRCULAR	0.02257	HUPE	2.74	0.T/			
			1	IRREGULAR	1 19961 0	Farthen	0.13	0			
	1.25			CIRCUIAR	0.00845	HDPF	3.14	0.53		0.0	
	1.25			CIRCULAR	0.01821	ACP.	3.09				
	3.5		1	CIRCULAR	0.01598	RCP	3.86				
	1.5		1	CIRCULAR	0.05941	RCP	3.43				
	2		1	CIRCULAR	0.06565 RCP	RCP	18.35			0.57	
	11.		1	CIRCULAR	0.09864	RCP	2.15				
			1	CIRCULAR	0.00169	RCP	2.84				
		0 9	T	CIRCULAR	0.00147 F	RCP	22.87	0.14	53.02	0.33	
				CIPCILIAP	0.00369	ACP.	11.7				
	1			CIRCUIAR	0.14,17,1	ACP.	2 41				
	1.5			CIRCULAR	0.02518	RCP	1.57		2.86		
	1.5	5 0	1	CIRCULAR	0.21636	RCP	2.85				
		3 0	1	CIRCULAR	0.00345	RCP	54.43				
		2 0	1	CIRCULAR	0.01003	RCP	5.42				
				CIRCULAR	0.02382	RCP	5.43				
				CIRCULAR	0.0245	SCB SCB	5.39				
	2.5			CIRCULAR	0.02144	ACP ACP	16.45	0.27		0.0	
		3 0	1	CIRCULAR	0.06449	RCP	23.16		39.62		
	3.5		1		0.01678	RCP	2.19			0.05	
	0.67		1	CIRCULAR	0.16213	PVC	0.91				
	2.5		1	CIRCULAR	0.02387	RCP	21.28	0.34			
			1	CIRCULAR	0.0155	RCP	2.56	0.09	5.09	0.18	
				CIRCULAR	0.01653	KCP.	7.56	0.09			
		1		CIRCUIAR	0.07.838	PVC	1.00	0.04	3.00	0.35	
	1.5			CIRCULAR	0.08805	RCP	2.23	0.07			
	1.5		1	CIRCULAR	0.10047	CMP	2.14	0.12			
	2.5	5 0	1	. CIRCULAR	0.00716	RCP	12.17	0.35	2	0.63	
			1	CIRCULAR	0.00716	RCP	5.09				
	-	0 0		CIRCULAR	0.11572	RCP	0.34		0.82		
	3,5	2 0		CIRCUIAR	0.02033	ACP.	75.77	0.43		200	
	5										

			5	mensions			Λ- 7	eal	OT	-year	
a	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	3.5		1	CIRCULAR	0.03355	RCP	63.27	0.34	1	0.59	
	1.5	5 0	1	CIRCULAR	0.02837	RCP	2.37				
		2	H .	CIRCULAR	0.05008	RCP	17.13				
		2	I	CIRCULAR	0.03224	KCP.	21.35				
	2.25	2 2 2		CIRCULAR	0.0059	RCP	5.01		5.45		
	1.25		1	CIRCULAR	0.08432	RCP	6.91	0.37		0.62	
			1	CIRCULAR	0.00453	RCP	96:0				
		2 0	1	CIRCULAR	0.02619	RCP	0.18			0.01	
	1.5		1	CIRCULAR	0.06693	RCP	1.01)		0.00	
		3	1		0.11591 CONC	CONC	0	0	0		
		3	,	PARABOLIC	0.00757	CONC	1.6	0.12			
		3 0		PARABOLIC	0.00303	CONC	0.24	0.12	0.47	0.24	
		1	1	CIRCULAR	0.17878	SMP	0.83		iT		
		5 10	1	RECT CLOSED	0.01659	RCB	308.85				
		0 9	1	CIRCULAR	0.01879	RCP	98.33	0.17	209.46	0.36	
		1 3	1	PARABOLIC	0.04794	CONC	0				
		1 3	1	PARABOLIC	0.09823	CONC	0	0			
		3	1	PARABOLIC	0.07036	CONC	2.03	0.05			
		2	a +	CIRCULAR	0.01/74	KCP SCB	4.94	0.35	8.1		
	, ,	2 12	-	CIRCUILAR	1 878.00	ACP.	3.18	0.53			
	11	2	1 4	CIRCULAR	0.27678	RCP	5.98	0.11		0.18	
	``	1 0	1	CIRCULAR	0.85398	CMP	0.34	0.02			
	7	4 0	1	CIRCULAR	0.02993	RCP	98.33	0.4			
		1 3	1	PARABOLIC	0.56037 CONC	CONC	0	0			
		3	1		0.24209	CONC	0	0			
	1 1		T	PAKABOLIC CIPCIII AP	0.0148	CONC	0 0	0	0 0	0	
			1	CIRCULAR	0.01324	RCP	10.69	0.41			
		2 0	1		0.15634	RCP	12.41		21.96		
		1 3	1	PARABOLIC	0.00303	CONC	0.27	0.03	0.49	90.0	
	8		1	CIRCULAR	0.00422	RCP	189.62				
	1.5		1	CIRCULAR	0.06712	RCP	17.17				
		0 0	1	CIRCULAR	0.02147 0	CMP	29	0.55		0.96	
				CIRCULAR	0.00118	SCP CP	0.08				
	1.5		1	CIRCULAR	1 99600:0	RCP	2.16				
	1		1	PARABOLIC	0.18289	Concrete	2.85				
	1.25		1	CIRCULAR	0.02919	RCP	0.24				
	1.25		T	CIRCULAR	0.01504	HDPE	0.26				
	1.25		T	CIRCULAR	0.04105	CMP	0.26				
			T T	CIRCULAR	0.00323	ACP RCP	13.17				
	1.5		1	CIRCULAR	0.06189	RCP	6.92				
			1	CIRCULAR	0.47947	RCP	3.18				
	2.5	5	1		0.01083	RCP	11.83		20.95		
		3	I	CIRCULAR	0.01081	KCP	21.17	0.31			
	1.5			CIRCULAR	0.15237	RCP	3.37				
	1.5		1	CIRCULAR	0.00506	RCP	5.83	0.78			
	1.5		1	CIRCULAR	0.01534	RCP	3.84				
		7	1	CIRCULAR	0.00263	RCP	167.14		33		
	1.5		1	CIRCULAR	0.01929	RCP	4.35	0.3	7.63		
			T	CIRCULAR	0.00704	KCP.	3.84	0.44			
	1.5	2 2 2	1	CIRCULAR	0.27655	CMP	4.01	on:n	0.0	0.13	
			1	IRREGULAR	0.01478	EAR	9.0	0.2	5:0	0:0	
	1.5		1	CIRCULAR	0.19015	CMP	3.46	0.08			
	2.5	5 0	1	CIRCULAR	0.09578	RCP	19.06	0.15		0.25	
	1.5		1	CIRCULAR	0.03988	RCP	1.33	0.06	2.31	0.11	

			٥	IIIIEIISIOIIS			Á-7	eal	OT	-yeal	
ū	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	1.5		T T	CIRCULAR	0.0106	CMP	5.31	0.49			
	1.5	5	1	. CIRCULAR	0.04587	RCP	68:39	0.28	10.53	0.47	
	7		1	CIRCULAR	0.00784	RCP	8.04	0.4			
	0.5	5 0	1	CIRCULAR	0.87276	PVC	1.17	0.22		0.35	
	(1)		1	RECT_OPEN	0.00915	EAR	1.7	0.02			
	2	5	1	CIRCULAR	0.00576	RCP	50.55		60.13	0.3	
	1.5		Ţ	CIRCULAR	0.04554	RCP	0.94				
		0	1	CIRCULAR	0.01812	RCP	51.36				
		1 3	1	PAPAPOLIC	0.00379	RCF	75.55			T.3b	
		0	1 1		0.02138	RCP	0.89	0.18	L.33		
	416	3 8	1		0.00056	CONC	1.24	90:0			
	ET)	8	1	RECT_OPEN	0.00217	CONC	5.31	0.13			
	(r)	3	1	CIRCULAR	0.03181	RCP	104.34				
	(T)		1	. CIRCULAR	0.0469	RCP	104.24				
	1.5		1	CIRCULAR	0.04287	RCP	2.35				
	1.5		1	CIRCULAR	0.05768	RCP	9.54				
	1.5		τ .	CIRCULAR	0.02149	HDPE	2.01				
	2.5		T .	CIRCULAR	0.00601	RCP	0.37				
	3 0	0 7	1	CIRCULAR	0.00605	RCP BCD	0.33				
	7.1	0 0	1 6	CIRCULAR	1 C0CCO O	RCP	0.19				
				CIRCUIAR	0.09948	CMP	1.33				
	2.5			CIRCULAR	0.21096 RCP	RCP	33.89	0.18	116.32	0.62	
	1		1	PARABOLIC	0.09316	Concrete	0				
	1	1 3	1	. PARABOLIC	0.04	Concrete	0.48	0.02	12.2	0.59	
	7	2 0	1	CIRCULAR	0.1509 CONC	CONC	5.05	0.06			
	41		1	CIRCULAR	0.01522	RCP	94.4	0.29	16		
	1.5			CIRCULAR	0.14643	CMP	2.81	0.13			
	1.5			CIRCULAR	0.009/6	KCP.	1.43	0.14	2.48		
	7		-		0.17017	HDPF	187	0.04			
	2		1 1	CIRCULAR	0.46873	HDPE	2.39	0.02			
	1.5		1	CIRCULAR	0.03969	HDPE	2.56	0.12			
	4		1	CIRCULAR	0.00333	RCP	16.7	0.2			
	4		1	CIRCULAR	0.10334	Earthen	18.95			0.00	
	30		1	RECT_OPEN	0.10318	Earthen	18.85				
	1.5		1	CIRCULAR	0.04903	HDPE	0.86				
	1.5		1	CIRCULAR	0.03154	HDPE	0.89				
	J. L		T	CIRCULAR	0.03585	HDPE	1.72				
	1.1.			CIRCUIAR	0.02882	HDPE	0.5				
	1.5	0	1 4	CIRCULAR	0.01638	HDPE	0.41	0.03	0.63	0.00	
	2		1	CIRCULAR	0.02458	RCP	14.2				
	1.5		1	CIRCULAR	0.04004 RCP	RCP	4.91				
	1.5			CIRCULAR	0.02909	HDPE	4.21	0.23			
	1.5		∃ €	CIRCULAR	0.01514	HDPE	0.I9				
	C.1	0 0	T (CIRCUI AR	0.03/48 HDPF	HDPF	0.34	0.00	7.69	60.0	
	1.5				0.0177	CONC	0.83				
	1.5		1	CIRCULAR	0.01652	HDPE	1.57				
	1.5		1	. CIRCULAR	0.03322	HDPE	2.05	0.11			
	1.5		1	CIRCULAR	0.01452	HDPE	1.03	0.08	1.59		
	1.5	5 0	1	CIRCULAR	0.02852	HDPE	1.28	0.07		0.11	
	1.5		τ .	CIRCULAR	0.04167	HDPE	4.22	0.2	6.7		
	-			CIRCULAR	0.08/83	KCP.	0.66	0.06			
	1.5		T	CIRCULAR	0.00521	KCP.	3 52	0.3	3.89		
	1.5			CIRCUIAR	0.06935	RCP	1 18	0.04			
	7		1	CIRCUIAR	0.10685	RCP BCP	4.79	190.0			
	1.5	2 0		CIRCULAR	0.0196	RCP	7.19	0.49	13.89	0.94	
	2.5		1	CIRCULAR	0.00366	RCP	9.19	0.37	``	0.71	

			5	mensions			λ- 7	Eal	PT	-year	
O	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap	(1)
	1	3	1	PARABOLIC	0.08587	Concrete	1.37	0.05	2.6	0.09	
	1	3	1	PARABOLIC	0.16413	Concrete	0				
			1	PARABOLIC	0.12316	Concrete	0				
	1.5		1	CIRCULAR	0.01258	RCP	7.55	0.64	15.36	1.3	
	3. C.		,	CIRCULAR	0.01599	RCP	51.03				
	0.0 7.0		T .	CIRCULAR	0.03833	RCP BCP	92.01	0.27		0.47	
	3.0		1	PARABOLIC	0.08133	Concrete	0				
	H	8	1	PARABOLIC	0.00505	Concrete	1.81	0.2	3.3		
	1.5	0	1		0.00934	RCP	3.22		5.82	0.57	
	3	3	1		0.00838	RCP	5.51				
	2		1	CIRCULAR	0.06925	RCP	3.88				
	2.3	0 0	1		0.03923	RCP	16.94	0.11			
	, [6	0	1	CIRCULAR	0.06807 RCP	RCP	10.88			0.12	
	1.5		1	CIRCULAR	0.06224	RCP	1.07	0.04			
	4	0 0	1	CIRCULAR	0.01105	RCP	26.68				
	1.5		1	CIRCULAR	0.07414	RCP	0.64				
	4	0	1	CIRCULAR	0.03938	RCP	26.1				
	2.5		7	CIRCULAR	0.02111	RCP	16.97				
	2.5			CIRCULAR	0.06037	RCP	24.28				
	2.7	0	1 4	CIRCULAR	0.04587	RCB	21.01				
	2	0	T	CIRCULAR	0.02502	RCP	12.6	0.35	22.59		
	2	0	1	CIRCULAR	0.02587	RCP	11.2				
	3		1		0.04382	RCP	36.19				
	1.5		1		0.02778	CMP	3.17				
	7 5		I	CIRCULAR	0.01345	HDPE	6.31		11.37		
	4	0	1		0.0162	ABS	72.19	0.39	120		
	2	0	1		0.07062	CMP	0.76				
	4		1		0.01712	RCP	78.79				
	4		1	CIRCULAR	0.03356	RCP	61.5	0.23	101.77		
	4		1	CIRCULAR	0.00678	RCP	61.41				
	4		,	CIRCULAR	0.0181	RCP	59.12				
	1	0	-	CIRCULAR	0.05178	RCP	3.73	0.46	6.69	0.83	
	1.5		1 1	CIRCULAR	0.0509	CMP	5.4				
	3		1	CIRCULAR	0.09784	CMP	10.59				
	9		1	CIRCULAR	0.03933	RCP	118.12		2.		
	1.5		1	CIRCULAR	0.01682	ABS	2.78				
	1.5		1,	CIRCULAR	0.2452	ABS	2.77				
	1.5		1 -	CIRCULAR	0.02226	ABS	5.63				
	2	0	1 1	CIRCULAR	0.00607	RCP	4.87		8.74	0.5	
	9		1	CIRCULAR	0.01527	RCP	119.29		2.		
	3	0	1	CIRCULAR	0.06046	RCP	19.37	0.12			
	8		1	CIRCULAR	0.0082	RCP	19.38		34.44		
	w .	0 0	1 1	CIRCULAR	0.10425	RCP	11.41				
	1:1	o m	1		0.02293	Concrete	0.14	0.01			
	T	8	1		0.0766	Concrete	0.17			0.01	
	2	0 0	1	CIRCULAR	0.01033	RCP	10.85		1		
	1		1	PARABOLIC	0.07132	Concrete	0.16	0.01			
	1.5		1	CIRCULAR	0.02264	RCP	1.34		2.45		
	7	0	1	CIRCULAR	0.00/8/	KCP.	7.67				
	2	0 0	I	CIRCULAR	0.03829	RCP	14.65	0.33	26.03		
	2	0	1	CIRCULAR CIRCIII AR	0.04249	RCP	14.64 8.83				
		o m	1	PARABOLIC	0.02076	Concrete	0.11				
	1	3	1	PARABOLIC	0.00678	Earthen	0.53			0.43	
	1		1	PARABOLIC	0.22115	Concrete	0.09	0	0.15	0	

			2	IIIEIISIOIIS			6-7	eal	OT	-year	
Q	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap	(1)
	2		1	CIRCULAR	0.00435	ABS	7.11		12.66	0.85	
	0.5	0	1	CIRCULAR	0.04295	ABS	0	0			
	0.5		, 1	CIRCULAR	0.01097	ABS	0.03				
			T	PAKABOLIC	0.0408	Concrete	0.06				
	L.3	0 0		CIRCULAR	0.0334 RCF 0.0957 RCP	NCP RCP	1.20	0.07		0.12	
	1.5			CIRCULAR	0.04935	ABS	2.05				
			1 [CIRCULAR	0.01085	CMP	20.55	55:0		26.0	
	1	3	1	PARABOLIC	0.10272	Concrete	0.69				
	1.5	0	1	CIRCULAR	0.0152	RCP	0.83	90:0	1.51	0.12	
	1	1 3	1	PARABOLIC	0.31425	Concrete	0.08				
	1	1 3			0.16378 Concrete	Concrete	0.53				
	1		1	PARABOLIC	0.04039	Concrete	0.23	0.01	0.45		
	1.5		ਜ ਦ	CIRCULAR	0.0219	RCP	4.47			0.52	
	i. C	0 0	1 -	CIRCULAR	0.01514	NCP NCP	5.65				
	C.1			CIRCULAR	0.00456	HDPF	4.05				
	3		1	CIRCULAR	0.03154	CONC	26.6				
	1.5	9	1	CIRCULAR	0.10703	RCP	1.18				
	4	4 0	1	CIRCULAR	0.00646	RCP	39.62				
	4		1	CIRCULAR	0.00902	RCP	54.04				
	4		1	CIRCULAR	0.0122	RCP	55.26				
	4	0	-	CIRCULAR	0.00327 RCP	RCP	27.15	0.33	41.96		
	2:2.2		1 -	CIRCLILAR	75500	ABS	1.34				
	2	0	1 [CIRCULAR	0.01378	ABS	1.3	0.05			
	1.5		1	CIRCULAR	0.15746	CMP	1.36	90:0			
	3.5		1	CIRCULAR	0.06161	CMP	24.11	0.18	33.45		
	1	1 3	1		0.01145	CONC	2.34	0.15			
	1.5		1	CIRCULAR Brott CI OCER	0.00884	RCP	2.34	0.24			
	0.92	7.0	1	CIPCLII AP	0.00802	ACB BCB	10.88		4.03		
	7	1.5	1		0.03101	CONC	10.88				
	1.5		1		1 95220.0	RCP	7.03				
			1	CIRCULAR	0.05399	SP	16.85	0.2			
	1	1 3	1	PARABOLIC	0.02734 CONC	CONC	0.55		66:0	0.04	
	0.33		1	CIRCULAR	0.13726	HDPE	0.87				
	3	3	1	CIRCULAR	0.00492	RCP	20.26				
	m	0 0	1	CIRCULAR	0.01641	RCP	40.31				
	4	0 0	1	CIRCULAR	0.00819	RCP	85.12				
	4	+ 4	1	CIRCUIAR	3 750.0	RCP	93.00				
	1 (60	0 0	1 1	CIRCULAR	0.00403	RCP	23.31	17.0			
	3	3	1	CIRCULAR	0.02132	RCP	4.78				
	m	3 0	1	CIRCULAR	0.05786	RCP	18.07			0.2	
	1.5	2	τ,	CIRCULAR	0.09632	RCP	8.01	0.25			
	-	0 0		CIRCULAR	0.03919	RCP BCB	17.98				
	0 6		1 -	CIRCULAR	0.03188	SCP SCP	17.80	0.23		0.34	
	100		1	CIRCULAR	0.00483	RCP	27.01				
	8	3	1		0.01531	RCP	13.86			0.28	
	3	3 0	1	CIRCULAR	0.07015	RCP	13.13				
	1	5.	1	PARABOLIC	0.01489	ASPHALT	0.21				
	2.5		1		0.01333 F	RCP	28.05		49.39	1.04	
	2.5		1	CIRCULAR	0.05245	CMP	28.19	0.3			
	13 (0 0		CIRCULAR CIRCIII AR	0.02697	KCP.	28.65				
	17)	3	T	CIRCULAR	0.01/12	KCP.	35.09	0.4		0.71	
	a C	0 0	1	CIRCULAR	9,998,000	CMP	3.00				
	1.5	2	1	CIRCULAR	0.01859	RCP	6.59				
	1.5	0	1	CIRCULAR	0.01746	RCP	8	0.58			
	1.5	5	1	CIRCULAR	0.04267	RCP	4.65	0.21	6.18	0.28	
		-									

			2	IIIEIISIOIIS			Á-7	eal	OT	-yeal	
Ð	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap	(1)
	2.5		1	CIRCULAR	0.01937	RCP	13.15	0.23	22.7	0.4	
	2.5	0	1	CIRCULAR	0.01908	HDPE	15.7				
	2.5		7	CIRCULAR	0.02612	RCP	17.68				
		1 0	1	PAPAPOLIC	0.01988	EAK	7.24		6.TT		
		3 3		PARABOLIC	0.02873	Concrete	0.13	0 0	0.22		
	9	0		CIRCULAR	0.00199	RCP	110.08	0.58			
	9	0		CIRCULAR	0.00114	RCP	274.05	1.91	375.58	2.62	
	9			CIRCULAR	0.00155	RCP	254.72	1.53	337.99		
	ę		1	CIRCULAR	0.0177	RCP	270.2				
	9		1		0.02642	RCP	255.97		336.33		
	4.5	0	1		0.013	RCP	75.28			0.59	
			2		0.01661	RCP	58.65	0.34	100.17		
		2 0		CIRCULAR	0.02256	CMP	6.14				
	71		1	CIRCULAR	0.04682	PVC	0.30				
	1.5			CIRCULAR	0.07683	RCP	3.12			0.18	
	<i>u</i> 11		1	CIRCULAR	0.00776	CMP	189.11				
	1.5		1	CIRCULAR	0.3513	RCP	3.41				
	4		1	CIRCULAR	0.01352	RCP	119.1				
	3.5		2	CIRCULAR	0.05692	RCP	150.22				
	3.5		2	CIRCULAR	0.02261	RCB	142.84				
	1.5			CIRCULAR	0.01132	RCP	5.7	0.51	9.58	0.86	
	2 1			CIRCUIAR	0.07844	RCP	0.00				
	1.5			CIRCULAR	0.04342	RCP	11.19	0.51		G	
	2.75	0	1	CIRCULAR	0.01865	RCP	33.79				
	1.5		1		0.10633	RCP	0	0			
	3		1	CIRCULAR	0.00575	RCP	125.48	0.64	18	0.93	
	1.5		1	CIRCULAR	0.01936	RCP	4.71	0.32	7.96		
	1.5				0.06851	CMP	6.44	0.43	10.77	0	
	0.67		H .		0.03324	ABS	27 77	0 0	93 30		
	4.5		1 1	CIRCULAR	0.00/43	ACP.	14.07	0.41			
	F			CIRCULAR	0.01791	RCP	38.86	0.01	62.9		
	2.5		1		0.02058	RCP	7.9				
	6		1	CIRCULAR	0.00752	RCP	29.49		54.3		
	2.5		1	CIRCULAR	0.0369	RCP	17.46				
	2.5		1	CIRCULAR	0.01465	НДРЕ	16.89		32.12	0.65	
	d	1 0	1	CIRCULAR	0.07241	HDPE	0.65				
	. 4] (0 0	T .	CIRCULAR	0.0205	RCP	16.03				
	4 0		7 -	CIRCULAR	0.02143	RCP	9.33				
		1	1 [CIRCULAR	0.0449	ABS	0.74				
	2	2	1	CIRCULAR	0.01632 RCP	RCP	8.67	0.3			
	1.5		1	CIRCULAR	0.00337	RCP	2.69				
	1.5		1	CIRCULAR	0.19239	HDPE	0.62				
	2	0 0	CT C		0.01358	RCP	9.35	0.35			
	1.5		1	CIRCULAR	0.00992	RCP	3.01		4.96	0.47	
	1.5		1	CIRCULAR	0.01926	RCP	3.02		5.01		
	.7	2 0	1	CIRCULAR	0.0127	RCP	12.08		20.89		
	, 7		1	CIRCULAR	0.03828	RCP	9.27				
	2.5		1	CIRCULAR	0.00368	RCP	0.31			0.03	
		9	H .	CIRCULAR	0.00103	RCP	39.88		71.65		
	2			CIRCULAR	0.01924	KCP.	39.37				
	2.5	2	1	CIRCULAR	0.01792	RCP	22.98	0.57	37.5	0	
	2.5		1	CIRCULAR	0.03125	RCP	0	0			
	7		1	CIRCULAR	0.00867	RCP	62.19				
	2.5	2	1	CIRCULAR	0.11215	RCP	0.72	0.01	16.42	0.12	
	1.5	5	1	CIRCULAR	0.03885	RCP	11.03				

a	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	1.5		1	CIRCULAR	0.02304 RCP	CP	0.73				
	1	1 0	1	CIRCULAR	0.03061 P	۸C	0.2				
	1.0	0 0	1	CIRCULAR	0.01932 R	CP	4.02				
	7	7	T	CIRCULAR	0.01945 R	200	12.14				
	1.3			CIRCUIAR	0.00379 Re	CP	13.07	0.56		75.0	
	2		1	CIRCULAR	0.0285 Rt	CB	16.98				
	2		T	CIRCULAR	0.02354 Rt	CP	15.39				
	2	2 0	1	CIRCULAR	0.03063 Rt	CP	17.63		29.94		
	2.5		1	CIRCULAR	0.01699 R	CP	17.03				
	m I		1	CIRCULAR	0.01088 R	CP	28.08	0.4	42.34	0.61	
	4.5			CIRCULAR	0.01269 R	3	113.56)7		
	1.5		1	CIRCULAR	0.05891 Rt	CP	4.23	0.17	7.36	0.29	
	1.5		1	CIRCULAR	0.0115 R	CP	5.1				
	9		1	CIRCULAR	0.00425 Rt	CP	152.69		267.56		
	1.5		1	CIRCULAR	0.05139 R	CP.	1.51				
	2.5		1	CIRCULAR	0.05264 R	CP	3.2				
	9		1	CIRCULAR	0.04159 R	d)	2.14				
	2.5		1	CIRCULAR	0.05905	ONC	13.99				
	3.7		1	CIRCULAR	0.00317	Color	14.55				
	1.5		1	CIRCULAR	0.13892 Rt	CP	8				
	9		1	CIRCULAR	0.00623 RG	RCP	157.37	0.47	277.39	0.83	
	4.5		1	CIRCULAR	0.01699 Rt	CP	162.83	0.64			
	9		1	CIRCULAR	0.00709 R	CB	162.69				
	2.5		1	CIRCULAR	0.06048 R	RCP	19.31				
	2.5		1		0.01602 R	G)	19.84			0.62	
	7		I	CIRCULAR	0.02815 R	3	21.08	0.56			
	2.5		1	CIRCULAR	0.01984 Rt	RCP	40.15	0.7			
	4		1		0.00573 Ri	CP	45.24	0.42			
	3		1	CIRCULAR	0.00814 RG	RCP	41.75			1.09	
	cr)		1	CIRCULAR	0.03267 R	CP	41.76				
	4		1		0.0209 R	Q.	45.55				
	9	0 0	1	CIRCULAR	0.0082 RC	RCP	152.02	0.4	266.75	0.7	
	9			CIRCULAR	0.00995 Rt	2	118				
	9		1	CIRCULAR	0.00569 Rt	8	152.02				
	2		1	CIRCULAR	0.00637 Ci	MP	4.46				
	2.5		1	CIRCULAR	0.02738 R	CP	27.93				
	2		Т	CIRCULAR	0.04327 R	CP	5.63				
	2		1	CIRCULAR	0.02474 R	SCP	10.68				
	2	2 0	T	CIRCULAR	0.01744 H	DPE	14.38			0.81	
	1.5		1	CIRCULAR	0.01806 H	DPE	1.41				
	1.5		1	CIRCULAR	0.03489 H	IDPE	1.4		2.5		
	2	2 0	1		0.00705 H	HDPE	9.18				
			1	CIRCULAR	H 1/1/1 H	IDPE	11.22	0.08			
	1.75			CIRCULAR	0.09901	RCP	10.56	0.21	18.47		
	1.5		1	CIRCULAR	0.01308 RG	RCP	5.75	0.48		0.93	
	1		1	CIRCULAR	0.05481 A.	BS	2.41	0.29			
	1.5		1	CIRCULAR	0.01369 R	CP	3.22	0.26			
	1.5		1	CIRCULAR	0.01785 Cf	CMP	3.2	0.42	5.72		
	2 1		1	CIRCULAR	0.023/3	AIN!	9.56	0.51			
	1.3		1	CIRCULAR	0.02548 Rt		21.75			0.58	
	2.5		1	CIRCULAR	0.03535 Rt	8	21.72				
	2.5		1	CIRCULAR	0.00714 R	CP	21.64				
	2.5	2 0	1	CIRCULAR	0.00711 RG	RCP	45.53	1.32	43.79	1.27	
	(7)	3 0	1	CIRCULAR	0.02089 R	ICP	46.51				

			5	IIIIEIISIOIIS			Á-7	eal	OT	-yeal	
ū	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1
	3.5		1	CIRCULAR	0.0312	SMP	0.00				
	3.5	5 0	1	CIRCULAR	0.03948	RCP	11.45	90.0	20.43	0.1	
	5.5		1	CIRCULAR	0.00689	3CP	42.05				
	5.5	0	_	CIRCULAR	0.00689	3CP	184.26				
	1.5			CIRCULAR	0.03258	(CP	3.39		6.56		
		3 0	1	PARABOLIC	0.07889	Concrete	0.27				
		1 1	1 6	CIRCLILAR	0.03771	ABS	0.00	0 0	1.0	0 0 0	
		1	1	CIRCULAR	0.00402	7BS	3.28				
	1	1 0	1		0.04015 ABS	\BS	5.02		4.75		
	1.5		1		0.00851	(CP	7.64				
	1		1	CIRCULAR	0.0111	НОРЕ	6.62				
	1.5		1	CIRCULAR	0.01417 R	RCP	2.35		4.08		
	1.5		1	CIRCULAR	0.05023	SMP	7.37				
	2.5		1	CIRCULAR	0.01482	3CP	10.29				
	7 6	2	1	RECT OPEN	0.00572 [arthen	1.89	0.13		0.3	
		1		CIRCULAR	0.01031	JOBE	3.3				
		0	1	IRREGIII 4R	0.03569	AB.	4.30				
	3			CIRCUI AR	8 9850.0	CP CP	CT:0				
	1.5	0	1	CIRCULAR	0.08646 RCP	€CP	15.7	0.51	28.2	0.91	
	0		1	IRREGULAR	0.04673 E	AR	8.59				
	9	0 0	1	IRREGULAR	0.05244	AR	8.59	0	15.34	0	
	1		1	. PARABOLIC	0.06452	CONC	0				
	1	1 3	1	. PARABOLIC	0.07107	SONC	0.21	0.01	0.35		
	7	2 0	1	CIRCULAR	0.00692	3CP	10.31	0.55			
	. 7	2 0	1		0.03404 R	RCP	18.53	0.44			
		2 0	ī		0.03487	RCP	21	5.0	37.26		
			1	CIRCULAR	0.07551	ABS	1.58			0.29	
	1.25		1	CIRCULAR	0.23812	CIVIP	0.48	0.00			
			-		8 COLO.O.	RCP	33.52		61 71		
					0.10128	CNO	4 13				
	m		1	CIRCULAR	0.00692	RCP	15.28				
	, m	3	1	CIRCULAR	0.0085	RCP	15.27				
	1.5		1	CIRCULAR	0.05279	RCP	1.59	0.07		0.12	
	m		1	CIRCULAR	0.05562 R	RCP	17.35				
	en	3 0	1	CIRCULAR	0.00673	3CP	21.28				
	60		1	CIRCULAR	0.03092 F	ЗСР	23.53				
	3.5		1	CIRCULAR	0.02696	3CP	23.36				
		0 0		CIRCULAR	0.08306	3CP	28.93				
		0		CIRCULAR	0.02342	RCP	33.3				
	2	2	1 [CIRCULAR	0.01787	C)	9.36				
	1	1 0	1	CIRCULAR	0.3433	RCP	0.28	0.01		0.02	
	9	0 9	1	CIRCULAR	0.00529	3CP	20.64				
	3.5		2		0.01888	3CP	187.16				
	3.5	0 0	7 7		0.01451	RCP	116.96		183.26		
	6.3		7	CIRCULAR	0.03771	RCP	103.63	0.12		0.10	
	3.25			CIRCULAR	0.0385	3CP	29.86				
	8		1	CIRCULAR	0.00408	RCP	158.17			0.53	
	1	1 3	1	PARABOLIC	0.09321	:AR	0	0	0		
	3.5		1	CIRCULAR	0.01089 R	RCP	59.58		10	0.98	
	1.5	5	1	CIRCULAR	0.01124	3CP	3.09				
	. 4			CIRCULAR	0.0107	CMP	9.26				
	1.5	0	d -	CIRCULAR	0.07895	4CF	2.54		4.51	0.15	
	4		-	CIRCULAR CIRCIII AR	0.01978	J.C.	30.31				
				CIRCUIAR	0.04044	4DPF	3.39				
	0	0		IRREGULAR	0.01187 E	Earthen	719.87	0.11	1068.98	0.17	
	4	0 0	1	CIRCULAR	0.01978	{CP	40.47				

							7-y	מסו	0.1	-year	
O	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1
	1.5		1	CIRCULAR	0.04813	1DPE	86:9	0.3			
	2	0	1	CIRCULAR	0.01396	HDPE	10.27	0.38			
	0		1	IRREGULAR	0.01417	Earthen	719.72	0.48	1067.45		
	0	0	1	IRREGULAR	0.01338	Earthen	728.42	0.5			
	0		1	IRREGULAR	0.04713 [Earthen	757.26	0.28	11	0.42	
	I	0	T	CIRCULAR	0.02166	CONC	3.27	0.62	4.63		
	7		1 6	CIRCULAR	0.19098	1DPE	13.91	0.14		0.13	
	1.5	0	1 1	CIRCULAR	0.00387	ABS	7.78	0.42	15.7	0.93	
	1:1	0	1 [CIRCULAR	0.00621	4DPE	1.27	0.45	2.24		
	T	0	1		0.03881	HDPE	3.05	0.43	5.44		
	0		1	IRREGULAR	0.00702	CONC	50.27	0	94.32		
	0		1	IRREGULAR	0.01345	EAR	49.89	0	94.07	0.01	
	8	0	1	CIRCULAR	0.06375	3CP	44.03	1.21			
	H .	m (7	PARABOLIC	0.01421	SONC	0.16	0.01			
		0	H .	CIRCULAR	0.0075 RCP	(CP	0.66	0.21	1.18	0.38	
	7		1 -	TPIANGIIAP	0.00304	SCP.	3.24	0.26			
	7 1 5			CIRCIII AR	75270.0	CONC	11.11	0.01			
	2.5		1 [CIRCULAR	0.05451	SCP SCP	27.04	0.28			
	2.5		1	CIRCULAR	0.03714	RCP	28.19	0.36	43.61	0.55	
	1.5		1	CIRCULAR	0.01976	3CP	1	0.07			
	0		1	IRREGULAR	0.037	arthen	729.88	0.06			
	0		1	IRREGULAR	0.01391	arthen	730.34	0.05			
	2.5		1	CIRCULAR	0.08056	CONC	3.92	0.03	12.38		
	2.5		1	CIRCULAR	0.00486	3CP	28.36	0.99	45.99		
	4		1		0.04831	RCP	43.54	0.14	65.08		
	4		c 1		0.00818	£ 5	28.08	0.22	42.89	0.33	
	0.0		1 -	CIRCULAR	0.11696	RCP	375.28	0.77	75 21		
	7.7	0	1	CIRCUIAR	0.2011.0 0.29333	MP	9.02	0.23	75:57	Ct:O	
	6.5		1	CIRCULAR	0.00849	RCP	219.74	0.45		0.0	
	6.5		1	CIRCULAR	0.01041	RCP	156.46	0.29			
	6.5		1	CIRCULAR	0.01564	RCP	156.67	0.24		0.39	
	6.5		1	CIRCULAR	0.00271	3CP	170.86	0.63			
	8	6	1	RECT_CLOSED	0.03795	RCB	111.94	0.17			
	E 1		← ₹	RECT_CLOSED	0.00141	(CB	80.01	0.64			
	6.0		1 +	CIRCULAR	0.00/16	(CP	100.08	0.37			
	2	0 0	1 -	CIRCULAR	0.16129	SCP.	1.05	0.01	0.30		
	6.5		1	CIRCULAR	0.0284	3CP	219.13	0.25			
	6.5		1	CIRCULAR	0.03687	3CP	368.14	0.37			
	4.5		1	CIRCULAR	0.00167	RCP	10.36	0.13	38.32	0.48	
	4.5		1	CIRCULAR	0.00205	3CP	11.57	0.13			
	m	0	7	CIRCULAR	0.00355	(CP	7.74	0.19			
	2		-	CIRCULAR	0.01304	HDPF	4.53	0.18	7.7	000	
	2		1 4	CIRCULAR	0.04507	HDPE	4.52	0.00			
	6.5		1	CIRCULAR	0.01265	RCP	386.15	0.65	289.57		
	2		1	CIRCULAR	0.00496	RCP	3.14	0.2	8.7	0.55	
	4		1	CIRCULAR	0.0489	RCP	9.34	0.03	11.97		
	1.5	0	1	CIRCULAR	0.01039	RCP	0.56	0.05	2.02	0.19	
	4.5		, 1	CIRCULAR	0.00166	(CP	13.38	0.17			
	4	0		CIRCULAR	0.01482	RCP BCB	63.35	0.36	106.49	0.61	
	-			CIRCIIIAR	0.31213	HDPF	3.46	0.08			
	2.5		τ π	CIRCULAR	0.05257	RCP	29.11	0.31	49.03		
	0	0	1	IRREGULAR	0.02049	Concrete	671.56	0.26	892:63		
	0		1	IRREGULAR	0.01427	Concrete	657.97	0.3			
	0	0	1	IRREGULAR	0.00495	Concrete	642.8	0.5	819.83	0.64	
	0		1	IRREGULAR	0.02722	Concrete	661.4	0.22			
	0		1	IRREGULAR	0.05109	Concrete	362.41	0.09			

								5		,,,,,	
Ð	D' or H' (diameter) or (height)	B' (width)	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap	(1)
	2		2	CIRCULAR	0.01882 RCP	CP	263.28	0.37	496.5	0	
	4	∞ '	1	RECT_OPEN	0.03105 E	arthen	0	0		0	
	4		1	RECT_OPEN	0.03038 E	arthen	0	0		0	
	4 9	0	1	CIRCIII AR	0.01022	artileii	3109	0.26	0 462 45	113	
	1.5		1	CIRCULAR	0.05896 R	CP	13.35	0.52	22.38	0.88	
	1		1	CIRCULAR	A 0.01495	BS	0.78	0.18	1.27	0.29	
	9		1	CIRCULAR	0.00877 R	CP	316.91	0.8	495.78	1.25	
	9	0	1	CIRCULAR	0.01026 R	CP	319.4	0.74	498.37	1.16	
	9		1	CIRCULAR	0.03387 R	CP	310.57	0.4	462.82	0.59	
	2		1	CIRCULAR	0.0095	CMP	2.27	0.19	3.8	0.32	
	1.5		1	CIRCULAR	0.01692 R	C.P.	6.59	0.48	11.43	0.84	
	2.5		1	CIRCULAR	0.00988 R	RCP	5.71	0.14	11.9	0.29	
	1.5		1	CIRCULAR	0.04842	MP	7.52	0.6			
	3	8	1	RECT_OPEN	0.02633 R	CB	77.83	0.12			
	1.5		1	CIRCULAR	0.07663	:MP	21.89	1.39			
	3		1	CIRCULAR	0.00429 R	CP	53.7	1.23			
	2.5		,	CIRCULAR	0.03133 R	CP	20.85	0.29			
	L.3		1	CIRCULAR	0.02019	RCP	11 99	0.15			
	2.5		1	CIRCULAR	0.02222 R	CP	15.4	0.25			
	2		1	CIRCULAR	0.02762 R	CP	19.59	0.52			
	2.5		1	CIRCULAR	0.02196 R	CP	1.28	0.02	2.09		
	1.5		1	CIRCULAR	0.01657 R	CP	4.56	0.34			
	2		1	CIRCULAR	0.01262 R	RCP	15.11	0.59			
	1.5				0.08025	:MP	3.38	0.21	6.24		
	m n		1		0.02419 R	A) (5)	67.79	0.65	91.09		
	0 10		1	CIRCULAR	0.03238	RCP	127.1	1.07	92.00	155	
	1.25		1	CIRCULAR	0.10592 R	CP	1.08	0.05			
	2		1	CIRCULAR	0.01039	CMP	126.26	0.48			
	2.5		1	CIRCULAR	0.00174 R	RCP	59.96	3.51	78.23	4.58	
	2.5		1	CIRCULAR	0.02646 R	RCP	59.95	0.9	78.57		
	3	0	1	CIRCULAR	0.03132 R	СР	67.57	0.57	69'06		
	00	0	1 ,	CIRCULAR	0.04937 R	RCP	8.13	0.05	13.49	0.09	
	5.9			CIRCUIAR	0.00966 R	CP	317.33	7.0	486.52		
	1		1	CIRCULAR	0.03732 H	IDPE	0.63	0.09	1.01		
	3	0	1	CIRCULAR	0.00527 R	CP	9.46	0.2	17.8	0.37	
	5	0	1	CIRCULAR	0.01672 R	CP	112.98	0.34	216.95		
	3.5		1	CIRCULAR	0.55138 R	CP	0.79	0	1.31		
	9			CIRCULAR	0.02255 R	d. C.b	107.16	0.17	207.85		
	2.3		1	CIRCULAR	0.07201 H	HDPE	3.65	0.06	90.9	0.1	
	2.5		1	CIRCULAR	0.00685 R	RCP	6.78	0.2	14.89		
	1		1	PARABOLIC	0.02976	Concrete	0	0		0	
	2.75	0	1		0.02432 C	CMP	15.27	0.34	29.44	0.66	
	1.5		1	CIRCULAR	0.04093 R	KCP	10.27	0.48	18.77	1.0/	
	T. 2		T	CIRCULAR	0.10428 C	RCP	79.78	0.55	174.84	1.21	
	1.5		1	CIRCULAR	0.05426 R	RCP	60.9	0.25	10.25	0.42	
	1.5		1	CIRCULAR	0.05762	CMP	2.8	0.2	4.45	0.33	
	1		1	CIRCULAR	0.0673	Concrete	0.7	0.11	1.2	0.19	
	2.5		1	CIRCULAR	0.03394	CONC	10.28	0.14	23.28	0.31	
	4	0		CIRCULAR PFCT OPEN	0.03621 R	CP	119.53	0.44	165.45	0.61	
	1 2	4 K	7 (7	RECI OPEN	0.10057	CONC	2.11	0.38	4.14	1.14	
	2		1	CIRCULAR	0.06139 R	CP	9.23	0.16	18.73	0.33	
	0.5		1	TRIANGULAR	0.02359	ONC	0.17	0.03	0.27	0.05	
	2	0	1	CIRCULAR	0.1068 R	CP	0.17	0	0.27	0	
	3	0	1	CIRCULAR	0.01235	ONC	8.96	0.12	14.77	0.2	

			2	DIIIIEIISIOIIS			6-7	עמו	OT	-year	
Q	D' or H' (diameter) or (height)	B' (width) Barrels	Barrels	Shape	Slope (ft/ft)	Material	Q _{con} (2-year) (cfs)	Qcon vs Qcap3	Q _{con} (10-year) (cfs)	Qcon vs Qcap3	(1)
	2.5	0		1 CIRCULAR	0.07002 CONC	CONC	23.12	0.21	31.21	0.29	
	0.5		1	PARABOLIC	0.02878	0.02878 Concrete	15.86		19.82		
	2.5	0	1	CIRCULAR	0.04492 CONC	CONC	21.65	0.25	28.73	0.33	
	2.5		1	CIRCULAR	0.02864 RCP	RCP	16.38		29.29		
	1.5		1	CIRCULAR	0.01469 HDPE	HDPE	4.01				
	2.5		1	CIRCULAR	0.02426 RCP	RCP	24.53	0.38	,		
	1	3	1	PARABOLIC	0.04219 Other	Other	0.29			0.08	
	1.5	0	1	CIRCULAR	0.10623 RCP	RCP	4.3		7.73	0.23	
	2.5	0 0	1	CIRCULAR	0.04233 RCP	RCP	24.28	0.29	40.64	0.48	
	1.5	9	1	CIRCULAR	0.08841 RCP	RCP	8.48				
	1.5		1	CIRCULAR	0.08949	RCP	11.01	0.35			
	1.5	9	1	CIRCULAR	0.07287 RCP	RCP	7.19		12.77		
	3	0 0	1	CIRCULAR	0.01118 RCP	RCP	24.09		40.91	0.58	
	3	0	1	CIRCULAR	0.00616 RCP	RCP	23.5	0.45	40.21	0.77	
	3	0	1	CIRCULAR	0.01387 RCP	RCP	31.04			0.56	
	2.5		1	1 CIRCULAR	0.01682 RCP	RCP	19.18	0.36			
	1.5		1	CIRCULAR	0.10761 RCP	RCP	19.02		33.66		
	1.5		1	CIRCULAR	0.01317 RCP	RCP	4.47		7.35		
	2.5	0 0	1	CIRCULAR	0.07204 RCP	RCP	16.04	0.15	26.78		
	1.5	0		CIRCULAR	0.04634 CMP	CMP	2.46	0.2	4.39		
	1			1 PARABOLIC	0.19867	CONC	0.21	0	0.34		
	3		1	CIRCULAR	0.03611 RCP	RCP	42.13		71.86		
	1.5		1	CIRCULAR	0.03346 RCP	RCP	2.18		3.91		
	0		1	IRREGULAR	0.04951 Other	Other	1.05				
	1			1 PARABOLIC	0.17945 Other	Other	1.44	0.02			
	3		1	CIRCULAR	0.00744 RCP	RCP	22.29				
	1		1	PARABOLIC	0.0674 Other	Other	10.58	0.21	20.29		
	0		1	IRREGULAR	0.03539 Other	Other	0		0		
	4		1	CIRCULAR	0.00777 RCP	RCP	26.8		94.47		
	1.5	0		CIRCULAR	0.00648 RCP	RCP	1.85	0.22	2.85	00:3	
	0			1 IKKEGULAK	0.02576 CON	CONC	0 0,		0		
	v .		T	CIRCULAR	0.33922	CIVIP	19.27				
	4		1	CIRCULAR	0.02456 RCP	RCP	78.07				
	m m		1	CIRCULAR	0.04727 RCP	RCP	44.03				
	1.5	0		CIRCULAR	0.10367 RCP	RCP	5.26			0.26	
	0			1 IRREGULAR	0.08468	Other	3.44				
	1.5		1	CIRCULAR	0.07684 RCP	RCP	6.52		11.27		
	1.5	0	1	CIRCULAR	0.02637 RCP	RCP	6.77		11.67	89.0	
	2	0	1	CIRCULAR	0.02899 RCP	RCP	3.5		2.69		
	2		1	CIRCULAR	0.00558 RCP	RCP	7.04		12.13		
	2	0		1 CIRCULAR	0.02137	RCP	7.53		12.1	0.37	
	1		1	CIRCULAR	0.05591 AC	AC	3.7		6.79		
	2	4	1	RECT_OPEN	0.02756 Other	Other	2.09	0.01	4.12	0.02	

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				Propo	sea C	Proposed Condition Junctic	ons Ke	Salits	umm	Junctions Results Summary Table			
imensions	SI				2-year			1	10-year				100-ye
<u>;</u>	2		Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total		,	100 to 10	Z
evation (feet)	Elevation (feet)	Depth (feet)	HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	(10- (10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	(100-year)	Inflow	In (100-)
(leer)	(leer)		(feet)	year) (cfs)	year) (cfs)		(feet)	year) (cfs)	year) (cfs)		(leer)	(TOO-Year) (CIS)	1001
341.403	341.403	0	344.82		243.07	Yes	345.2		286.28	YES	347.76		
346.771	346.771	0	346.77	0	0	No		0	0			0	
347.275	347.275	0	347.27		0 0	ON S	347.28	0	0	YES	347.84		
328.592	328.592	0	331.4	0	657.23		331.88		876.56				
326.449	326.449	0	328.91		657.97	Yes	329.28		875.9				
322.374	322.374	0	444.62	0	10.29	ON :		0	879.17			0	
303.901	303.901	35 387	429.18		10.28	No	307.17	0 0	891.94	YES	307.49		
428.443	433.443	5055	306.79	0	669.07	Yes		0	27.36				
453.153	453.89	0	454.89		0	Yes	454.89	0	0	YES			
402.105	408.105	9	405.52		184.14	ON	7	0	296.33			0	
298.4	332.835	34.435	300.87		130.94	No	302.3	0	299.03	NO	304.38		
442.149	442.149	0	442.29	0	0.59	Yes	7	0	1.47			0	
383	383.487	<null></null>	384.16		223.19	Yes	384.16	0	223.19	YES			
395.27	398.27		395.47		18.95	No			25.64				
406.663	407.059		406.66		0	NO			0				
379.738	379.738	0 07 17	379.89	0	4.81	Yes	379.95		8.3	YES	380.03		
383.6	389.575	5.975			295.61	ON ON	38.	0	400.32				
386.822	386.822	0	387.02	0	7	Yes		0	11.94			0	
354	360.317	<null></null>	354.99		6.55	NO	354.99	0	6.55		354.99		
295.358	301.358 <null></null>	<null></null>	296.01		7.53	ON :			7.53				
368.044	3/1.044	<null></null>	368.04	0	0 2 2	ON ON	368.04	0 0	0 0	OZ Z	368.04		
0	0	0	283.24		726.1	Yes		0	0				
414.412	414.412	0	0		0	No	414.4	0	0		414.4		
303.5	314.067	10.567	414.41		0	No		0	50.94				
372.88	373.335	0 7	304.64	0	26.66	No	374.76	0	191.57	YES	375.73		
352.416	352.556	0	388.73		78.72	ON		2.22				0.16	
355.651	355.651	0	356.19	1.2	99.54	Yes		4.06					
354.446	354.446		360.7	4.06	12.07	Yes	360.58	0	271				
348.963	357.963	6	360.58		271	Yes		0	237.68			0	
339.925	348.925	o c	350.53	0	118.12	ON S	342.94	0	274.27	NO NE	344.02	7	
3/3.3/4	3/3.3/4	0	375.22	11.4	11.45	Yes		0					
374.021	374.021	0	0	0	0	ON	374.21	0	6.18	YES	374.25		
376.37	376.548	0	374.17	0	3.52	Yes	378.43	14.01	16.13		379.51	0.859	
408.997	408.997		377.8	7.4	9.63	Yes			2.74				
407.59	407.59	0	409.14	0	1.44	Yes	408.59	0	4 70 11	YES	408.67	0	
460.336	461.226		443.24	0.6	6.21	Yes	462.88	12.75					

				Propo	sed Co	Proposed Condition Junctic	ons Re	sults S	umm	Junctions Results Summary Table			
imensions	SI				2-year			1	10-year				100-ye
			Max.	Max. Lateral	Max. Total		Мах.	Max. Lateral	Max. Total				
Invert evation	Rim Elevation	Depth (feet)	HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	HGL (10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	May Ir
(теет)	(reet)		(feet)	year)	year)		year) (feet)	year) (cfs)	year)		(теет)	(100-year) (cfs)	(T00-)
482.694	490.694	8	477.76		15.8	No	483.79	0.29	22.72	ON	484	0.011	
433	437.465	4.465			13.16	No		3.77	4.45	ON		0.22	
373.7	375.557	12 625	433.51	2.0	2.69	ON Z	374.28	0	0.09	ON Z			
430	442.833	7.952		0	123.45	ON		0	71.84	ON	432.41	0	
419.743	419.743	0	412.35	0	42.11	ON	422.88	1.58	34.89	YES	423.18	0.076	
443.159	449.159	9		0.9	20.97	Yes		0	15.67	ON	4		
439.995	398 827	103	443.89	0	9.41	ON ON	394 18	0	20.29	OZ Z	396.84	0	
388.355	397.355	6	391.96	0	153.52	ON		0	287.96	ON		0	
387.716	394.716	7	391.25		162.23	No	393.57	0	286.45	ON	395.73	0	
390	397.709	7.70	(1)		162.79	No	39.	2.69	267.74	ON		0.14	
412.208	417.208	Ω C	394.6	1.6	152.74	ON Z	414	0	52.31	NO	417.47		
430.704	433.734	37.734		0	0.16	Yes		0	46.49	NO		0	
442.39	442.475	0	404.13		46.51	N		13.49	13.68	YES		0.849	
409.806	416.806	7	443.93	7.4	7.59	Yes	413.4	20.44	62.56	ON	413.89	1.44	
332.276	332.691	0	412.23		34.03	No		33.54	33.54	YES			
329.327	329.327	0	334.21	19.28	19.28	Yes	333.59	32.14	275	YES	335.16	2.4	
378.33	382.41				179.71	NON		9.27	69.85	VES		0.413	
384.013	391.513	7.5		5.2	45.79	ON		0	311.21	ON			
376.5	386.892	10.392			180.48	N		0	340.12	ON			
374.327	375.504				185.48	No		4.27	96.59	YES		0.218	
406.689	412.189	ις		2.3	51.69	Yes		0	47.74	ON :		0	
389 922	396 922	7	407.72	0 8 0 2	29.22	ON ON	392.82	13.42	55.3	OZ Z	393 15	0.869	
390.701	397.701	7	391.17		43.61	ON N		0	56.01	ON		0	
383	395.741	12.741	391.79		36.33	NO			330.54	ON	387.65	0	
385.83	395.864	10.03	386.08		219.89	No			585.88	ON		0	
397.87	397.87	0	390.13		375.3	ON S	398.2	4.63	4.63	YES	398.3	0.246	
0 0	0	0 0	398.19	7.83	7.83	NO NO	0	0 0	0 0	ON CN			
0	0		0		0	ON		0	0	ON		0	
404.786	405.75	0	0		0	N	404.8	0	5.41	ON	404	0	
0	0		404.85		2.98	No		0	0	ON		0	
374.2	380.26	9.0	0 1	0	0 [ON .		0	39.57	ON :			
389.45	397.45		3/7.51		13.67	ON Z		0	517.42	ON ON			
390.224	397.974	۲./۷	393.24	0	330.64	ON ON	395.93		489.97		396.52		
393,464	401.214	7.75	397.95		0.78	ON ON		0	488.67	O N			
409.6	416.359	9	397.52		316.96	No		0	183.98	ON		0	
425.117	425.117		413.16		126.64	NO		6.77	13.52	YES		0.372	
333.493	333.493	0	425.59	4.06	8.15	Yes	336.95	0.17	85.44	YES	337.31	0.005	

Max.					Propo	sed C	Proposed Condition Junctic	ons Re	sults 5	nmm	Junctions Results Summary Table			
Hotelation Hot	imensior	SI				2-year			1	0-year				100-ye
	Invert	Rim	:	Max.	Max. Lateral	Max. Total	-	Max. HGL	Max. Lateral	Max. Total	-	Max. HGL	Max. Lateral	Mag
CFS CFS	evation (feet)	Elevation (feet)	(feet)	(2-year)	(2- year)	(2- year)	Surcharging (2-year)	(10- year)	(10- year)	(10- year)	Surcharging (10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	lr (100-)
455.826 8.27.2 65.12.9 0 2.1.2 NO 43.56 O 2.5.4 NO 43.56 O 2.5.4 NO 43.64 NO 44.25 O 3.9.4 NO 44.25 NO 44.25 O 3.9.4 NO 44.25 NO 44.25 NO 44.25 NO 45.24 NO 44.25 NO 45.24 NO 44.25 NO 45.24 NO 44.25 NO 45.24 NO 44.25 NO 44.25 NO 45.24 NO 44.25 NO 45.24 NO 44.25 NO 45.24 NO 44.25 NO 45.24 NO 44.25 NO <th< th=""><th>7000</th><th>101 014</th><th>117.0</th><th></th><th>(cfs)</th><th>(cfs)</th><th></th><th></th><th></th><th>(cfs</th><th></th><th></th><th></th><th></th></th<>	7000	101 014	117.0		(cfs)	(cfs)				(cfs				
442716 64776 44277 6 4776 44277 0 2.22 NO 435.66 0 5.45 NO 447.818 442.78 42.24 0 43.24 NO 443.26 0 8.25 NO 447.818 0.186 443.24 0 2.24 NO 440.28 0 1.580 NO 442.186 6.16 443.34 0 2.24 NO 440.2 0 2.89 NO 442.186 0.16 443.34 0 0 2.24 NO 440.2 0 0.89 NO 442.187 0.16 443.34 0 0 2.24 NO 440.2 0 0.89 NO 442.187 0.16 443.34 0 0.22 NO 440.2 0 0.89 NO 442.187 0.16 4.24 0 0.22 NO 440.2 0 0.89 NO 4.24 0.16 4.24	450.91	459.585	8,072			5.12			0		OZ CZ	529.36		
447 281 7.56 445.56 0 43.1 No 435.46 0 15.89 NO 448 282 10.686 445.34 0 43.79 0 15.89 NO 448 282 10.686 445.34 45.79 0 9.13 NO 440.28 0 15.89 NO 467 186 10.686 46.71 40.72 40.72 0 3.34 NO 467 186 11.06 46.71 40.72 0 3.24 NO 467 186 11.07 40.01 0 2.21 NO 440.2 0 1.58 NO 443 286 11.06 4.01 1 2.21 NO 440.2 0 1.58 NO 440 28 11.06 4.01 1 2.21 NO 440.2 0 1.58 NO 440 28 11.06 4.01 4.02 0 4.02 0 1.00 NO 440 28 11.06	436.24	442.716	6.476			2.22			0		ON			
448.202 8.4462 4.93 4.93 No 44756 D 3.39 NO 448.202 8.4426 4.945 4.945 4.945 4.945 0 3.39 NO 448.202 4.945 4.945 4.945 4.945 4.945 0 3.39 NO 449.386 4.041 4.043 0 2.24 NO 4.935 0 3.39 NO 449.386 0 4.040 0 2.24 NO 4.035 0 3.39 NO 449.386 0 4.040 0 2.24 NO 4.042 0 2.24 NO 4.053 NO 441.396 0 3.24 0 2.24 NO 4.023 NO 4.053 441.307 0 3.24 NO 4.042 0 3.44 NO 4.043 NO 4.053 NO 441.302 0 3.243 NO 4.043 NO 4.043 <td>434.82</td> <td>442.08</td> <td></td> <td></td> <td></td> <td>3.1</td> <td></td> <td></td> <td>0</td> <td></td> <td>ON</td> <td></td> <td></td> <td></td>	434.82	442.08				3.1			0		ON			
462,196 6,566 440,16 0 2,21 NO 453,57 0 3,39 NO 442,1356 6,146 45,435 0 2,21 NO 443,5 0 0 3,3 NO 442,1357 6,146 45,145 0 2,21 NO 440,0 0 0 0 442,1357 6,146 45,145 0 2,24 NO 440,0 0 0 0 442,1377 4,143 0 2,24 NO 440,0 0	436.92	447.818	10.898			4.93			0		ON C	513.45	0	
449.186 6.446 6.456 6.442 6.456 7.556 <	453.1	462.786	9.686			2.21			0	(1)	ON			
421.927 11.927 443.39 0 2.21 NO 440.00 0 59.9 VVS 343.36 0 4410.16 0 2.34 NVS 342.96 0 55.3 VVS 341.386 0 440.01 0 2.34 NVS 345.04 NVS YVS 350.32 0 316.04 0 2.34 NVS 345.03 N YVS 350.32 0 345.44 0 2.34 NVS 345.03 N A11 NVS 350.32 0 346.42 0 2.31 N 46.44 N 46.44<	443.04	449.186	6.146			2.24			0		ON			
343.896 0 440.11 0 0.62 NO 440.06 0 5.55 VES 341.396 0 342.48 0 362.49 0 5.53 VES 316.022 0 342.48 0 342.99 0 1.2 VES 350.32 0 350.34 0 2.0 0	410	421.927		443.39	0	2.21			0		ON	461.2		
316.024 0 34.41 VES 74.52 0 76.54 76.54 0 76.54 0 76.54 76.54 76.54 76.54 76.54 76.54 76.54	439.709	439.896				0.62	ON >		0		YES	440.1	0	
443.94 0 316.04 0 7.5 7.6 4.45.2 0 4.15 7.65 360.32 0 444.44 0 2.11 Ne 446.29 0 10 0<	341.390	341.390				29.41			0 0		YES	, cr		
350.392 0 454.44 0 2.11 Nes 350.39 0 0 0 0 0 0 456.49 0 0 0 0 0 456.49 0 0 0 0 0 0 456.49 0 0 0 456.49 0 0 456.20 0 350.39 0 450.20 0 450.20 0 158.60 <t< td=""><td>454.343</td><td>454.343</td><td></td><td>316.04</td><td></td><td>0.7</td><td></td><td>,</td><td>0</td><td></td><td>YES</td><td></td><td></td><td></td></t<>	454.343	454.343		316.04		0.7		,	0		YES			
445.597 0 350.39 0 46.49 0 45.49 VES 445.626 0 380.57 Yes 422.24 0 423.4 YES 431.602 0 290.66 0 380.57 Yes 422.24 0 423.4 YES 286.635 0 243.60 0 743.9 Yes 731.9 Yes 733.9 Yes 138.9 Yes 141.6 Yes 733.9 Yes 742.9 Yes 141.6 Yes 141.6 Yes 141.6 Yes 141.6 Yes 141.6 Yes 141.6 Yes 142.6 Yes	350.392	350.392	0	454.44		2.11			0		ON	350.39		
431,602 0 435,788 0 445,4 0 475 475 431,602 0 290,66 0 380,37 Yes 226,238 0 1439,67 YES 276,635 0 431,602 0 15,86 0 1139,67 YES 285,233 0 28,873 0 15,86 0 1139,67 YES 429,47 0 28,873 0 0.31 YES YES YES 429,407 0 31,887 0 0.34 YES YES YES 429,407 0 31,867 0 0.34 YES 311,90 YES 429,407 0 31,867 0 0.34 YES 316,27 YES 429,407 0 43,87 0 680,38 YES 310,01 YES 316 YES 421,887 0 43,27 0 43,27 0 73,41 YES 435,27	445.997	445.997		350.39		0			0		YES		0	
431 563 0 280,540 0 380,57 Ves 422,54 0 127,93 VES 276,533 0 228,33 0 278,38 0 754,79 Yes 288,63 0 120,41 Yes 285,233 0 278,38 0 754,79 Yes 318,67 0 71,27 Yes 429,631 0 238,67 0 1.94 Yes 319,01 0 412 Yes 429,471 0 432,61 0 429,6 0 429,6 Yes 429,6 0 412 Yes 429,401 0 432,6 0 439,6 Yes 435,6 0 422 Yes Yes 429,6 Yes Yes 429,6 Yes Yes 429,6 Yes Yes 429,6 Yes Yes A29,6 Yes Yes A29,6 Yes Yes A29,6 Yes A29,4 Yes A29,4 Yes	285.632	285.768	0	446.42		9.5			0		YES			
285.233 0 742.03 0 742.04 Ves 331.9 0 133.04 Ves 331.9 0 133.04 Ves 331.9 0 132.04 Ves 331.9 0 143.04 Ves 331.9 0 143.04 Ves 425.04 0 143.04 Ves 331.9 0 143.04 Ves 425.04 0 143.04 Ves 431.04 0 143.04 Ves 432.04 0 143.04 Ves 432.04 0 432.04 Ves	431.602	431.602	0	290.66		380.57			0	-	YES			
319.932 0 288.07 0 731.01 Yes 311.9 0 1.52 NO 429.407 0 331.89 0 0.91 No 429.6 0 4.12 YES 316.031 0 331.89 0 680.38 Yes 425.6 0 680.38 YES 425.80 0 431.80 0 680.38 Yes 425.6 0 662.3 YES 435.70 0 434.27 0 45.74 Yes 425.6 0 79.41 YES 435.80 0 434.27 0 45.74 Yes 425.6 0 79.41 YES 437.80 0 437.9 0 45.74 Yes 425.6 0 75.41 YES 437.80 0 437.9 0 43.09 Yes 435.8 0 433.4 NC 437.90 0 0 433.76 0 436.8 Yes	285,233	276.633		452.09		754.79					YES	279.27		
429.407 0 311.89 0 0.91 No 429.6 0 4.12 VES 415.31 0 316.631 0 680.38 Yes 425.6 0 680.38 Yes 425.6 0 680.38 Yes 425.6 0 79.41 YES 435.7 0 78.4 Yes 435.6 0 79.41 YES 435.7 0 78.4 Yes 435.6 0 79.41 YES 435.7 0 78.4 Yes 435.6 0 79.41 YES 435.6 0<	303	319.993		288.07		731.01			0		ON			
316.031 0 429.51 0 1.94 Yes 319.01 0 884.89 YES 425.583 0 318.67 0 6.62 YES 425.64 0 6.62 YES 425.583 0 435.64 0 4.1 Yes 435.66 0 6.62 YES 425.701 0 437.64 0 4.1 Yes 435.66 0 5.41 YES 392.825 0 425.75 0 4.35.72 0 7.41 YES 392.825 0 425.75 0 5.41 YES 435.83 0 5.43 YES 407.93 0 433.76 0 1.784 YES YES YES 409.934 0 433.76 0 8.68 Yes 436.31 YES YES 409.934 5.18 429.68 Yes 429.63 0 15.42 YES 409.934 5.18 40.7	429.345	429.407	0	311.89		0.91			0		YES	429.78		
425.583 0 431.67 0 680.38 Yees 425.66 0 66.2 YeS 425.701 0 434.27 0 45.74 0 45.74 Yes 425.66 0 79.41 YeS 425.701 0 434.27 0 45.74 Yes 425.76 0 79.41 YeS 425.701 0 437.93 0 43.75 0 73.41 YeS 425.76 0 79.41 YeS 437.93 0 43.76 0 1.97 YeS 425.76 0 75.41 YeS 409.934 5.18 429.56 0 8.68 YeS YeS 429.63 0 15.44 YeS 409.934 5.18 429.56 0 8.68 YeS 429.63 0 15.42 YeS 409.934 5.18 429.56 0 8.68 YeS 408.51 0 15.42 YeS 40.934	316.031	316.031	0	429.51		1.94			0		YES		0	
431.831 0 442.544 0 443.74 Yes 433.24 0 7.941 YES 392.825 0 442.57 0 43.74 Yes 435.76 0 3.12 YES 392.825 0 435.75 0 1.97 Yes 435.76 0 5.43 NO 437.943 4.535 393.01 0 43.09 Yes 435.76 0 54.31 YES 429.226 0 433.76 0 1.78.42 NO 312.2 NO YES 429.226 0 433.76 0 1.78.42 NO 312.2 NE YES 429.226 0 433.76 0 89.79 Yes 40.81 NE YES 429.236 0 434.82 0 43.64 NE YES YES 439.837 0 43.69 Yes 40.83 0 43.54 YES 434.838 0 4	425.583	425.583	0	318.67		680.38			0		YES			
32.829 0 45.575 0 1.97 Yes 393.04 0 54.1 YES 437.943 4.535 393.01 0 43.09 Yes 433.83 0 543.4 NO 437.943 0 433.76 0 17.842 NO 75.2 YES 402.926 0 433.76 0 89.79 Yes 429.63 0 15.72 YES 402.926 0 86.8 Yes 429.63 0 15.44 YES 408.93 0 434.92 0 86.8 Yes 429.63 0 15.44 YES 408.93 0 434.92 0 8.68 Yes 429.63 0 15.44 YES 408.93 0 434.92 0 2.54 Yes 429.63 0 NO 41.03 0 0 0 0 0 0 0 0 NO 41.03 0	431.881	431.881	0 0	425.64		4.1			0 0		YES	436.83		
437.943 4.536 39.01 0 43.09 Yes 433.83 0 243.4 NO 307.49 0 437.94 No 312.2 0 157.22 YES 307.49 0 178.42 No 312.2 0 157.22 YES 409.324 5.18 429.55 0 88.79 Yes 429.63 0 15.44 YES 409.334 5.18 429.55 0 8.68 Yes 408.51 0 15.44 YES 434.825 0 434.92 0 2.54 Yes 408.51 0 68.29 NO 414.937 0 434.92 0 0 0 0 0 0 NO NO 414.937 5 40.03 0 0 0 0 0 0 NO NO 0 0 0 NO NO NO 0 0 0 0 0 0	392.829	392.829	0	425.75		1.97			0		YES			
307.49 0 433.76 0 178.42 No 312.2 0 157.22 YES 429.256 0 311.56 0 89.79 Yes 429.63 0 15.44 YES 429.256 0 311.56 0 86.79 Yes 429.63 0 15.44 YES 449.825 0 311.56 0 37.09 NO 435 0 68.29 NO 434.825 0 440.29 0 37.09 NO 435 0 68.29 NO 434.825 0 430.29 0 37.09 NO 0 <	433.408	437.943	4.535			43.09			0		ON		0	
429.256 0 31.56 0 89.79 Yes 429.63 0 15.44 YES 409.934 5.18 429.56 0 8.68 Yes 408.51 0 68.29 NO 434.825 0 437.29 0 37.09 NO 435 0 68.29 NO 0 434.825 0 0 2.54 Yes 408.51 0 NO 0 0 0 2.54 Yes 0 0 NO NO 414.937 5 0 0 0 0 NO	307.49	307.49		433.76		178.42			0	`	YES			
404.934 5.18 442.50 0 8.08 Yes 408.51 0 08.29 NO 434.825 0 434.825 0 437.99 0 37.09 NO 435 0 0 0 0 0 NO	429.226	429.226	0 1			89.79			0		YES			
414.937 6 434.92 0 2.54 Yes 0 0 0 0 NO 414.937 5 0 0 0 0 NO NO <t< td=""><td>434 677</td><td>409.934</td><td>9.T8</td><td></td><td></td><td>37.09</td><td></td><td></td><td>0 0</td><td></td><td>NO</td><td>410.03</td><td></td><td></td></t<>	434 677	409.934	9.T8			37.09			0 0		NO	410.03		
0 0 0 No No 410.05 0 NO 414.937 5 0 0 0 410.05 0 0 0 NO 422.682 7 410.03 0 0 0 0 0 0 0 NO 422.682 7 416.03 0 0 0 0 0 NO	0	0	0	434.92		2.54			0		ON			
414.937 5 0 0 0 410.03 0 <t< td=""><td>0</td><td>0</td><td>0</td><td>0</td><td></td><td>0</td><td>ON</td><td></td><td>0</td><td></td><td>ON</td><td>0</td><td></td><td></td></t<>	0	0	0	0		0	ON		0		ON	0		
422.682 7 410.03 0.17 No 415.77 0 0.27 NO 0 0 415.75 0 0.17 No 0 0 0 NO	409.937	414.937	5	0		0			0		ON		0	
0 415.75 0 0.17 No 0 0 0 NO 290.419 3.219 0 0 0 0 0 0 NO 292.517 4.5 290.57 0 23.56 NO 393.22 0 40.99 YES 392.025 1 290.74 0 19.02 NO 46.99 YES 9 0 392.92 0 46.99 YES 9 0 392.92 0 46.99 YES 9 0 0 0 0 NO NO 441.07 0 0 0 0 0 NO NO	415.682	422.682	7	410.03		0.17			0		ON	415.7		
290.419 3.219 0 0 0 No 290.82 0 40.99 VES 292.517 4.5 290.57 0 23.56 No 290.82 0 40.99 VES 392.025 1 290.74 0 19.02 No No 393.22 0 46.99 VES 0 392.92 0 29.88 Ves 0 46.99 VES 0 0 0 0 0 0 0 NO 441.073 1.073 0 0 0 440.77 0 4.63 NO	0	0		415.75		0.17			0		ON C	0		
292.517 4.5 290.57 0 23.56 Yes 290.95 0 33.66 NO 392.025 1 290.74 0 19.02 No 393.22 0 46.99 YES 0 0 392.92 0 29.8 Yes 0 NO NO 441.073 1.073 0 0 0 0 440.7 0 4.63 NO	287.2	290.419				0			0		YES	291.5		
392.025 1 290.74 0 19.02 No 393.22 0 46.99 YES 0 0 392.92 0 29.8 Yes 0 0 0 NO 0 0 0 0 0 0 0 NO 441.073 1.073 0 0 0 440.7 0 4.63 NO	288.017	292.517				23.56			0	33.66	ON			
0 392.92 0 29.8 Yes 0 0 NO 441.073 1.073 0 0 0 0 0 0 0 NO 444.073 1.073 0 0 0 0 4.63 NO NO	391.025			290.74		19.02			0	46.99	YES			
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0	0	0	392.92		29.8			0	0	ON			
441.0/3 1.0/3 U U U U 440.7 U 440.7 NU	0	0	0			0			0	0	ON 2		0	
315 57 57 NO 313 41 0 4 20 67 NO	311 506	316 506		440 6		7 5 7		('	0 0	,	ON CN	314.76	100	

								0.11.0		1404			
				Propo	sea C	Proposed Condition Junctic	JUS KE	Salits	umm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
			Max	Max.	Max. Total		Мах.	Max.	Max. Total				
Invert	Rim Elevation	Depth (feet)	HGL (2-vear)	Inflow (2-	Inflow (2-	Surcharging (2-vear)	HGL (10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	May
(feet)	(feet)		(feet)	year)	year)		year) (feet)	year)	year)		(feet)	(100-year) (cfs)	(100-)
354	354.566	0.566	303.21		2.95	No	354.01		0.14	ON	354.02		
414.035	414.192		354.01	0	0.04	No	414.08	0	1.14	ON	414.1		
0	0	0	414.07	0	0.72	ON	0	0	0	ON			
0 0	0	0	0	0	0	ON N	0	0	0	OZ Z	0		
395.666	395.666	0	0	0	0	NO	396.09	0	86.86		396.0		
438.347	438.347	0	396.09	0	86.86	Yes	438.38	0	0.55			0	
448.444	448.444	0	438.37	0	0.32	Yes	448.68	0	1.26				
443.333	443.333	0	449.02	0	0.69	Key Yes	443.03	0	27.82	YES	445.09		
413	414.259	1.259		0	15.79	Yes	415.21	0	29.92				
427.746	439.246	11.5	415.03	0	17.04	Yes	429.65	0	27.42	ON	435.1		
431.077	437.077	9 1	429.09	0	15.39	ON :	431.08	0	0	ON			
431.6/6	436.676	۷ (431.08	0	0 0	ON ON	431.68	0	0 97	NO	434.69		
0	0		437.85		0.58	Yes	0	0	0	ON			
432.413	433.275	0	0		0	ON	432.56	0	15.51	ON	432.5		
469.206	476.123	6.917	432.53	0	10.95	No	470.28	0	90.6	ON			
462.42	469.992	7.572	469.96	0	5.49	No	473.46	0	80.11				
465.861	470.861	5	464.33	0	47.07	ON Z	467.08	0	25.55				
485.912	782.586	9.6/4	466.48	0 0	13.1	ON N	486.51		45.55		486.76		
277.2	282.045	4.845		0	51.7	ON ON	280.05	0	92.91				
306.849	306.849	0		0	52.51	No	310.11	0	887.3				
459.186	459.937	0.751	309.73		666.03	Yes	459.24	0	3.15			0	
439.108	494.57	55.462	459.22		1.93	ON Z	439.43	0	3.57	ON G	43		
479	480.009	7.084	439.36	0 0	0 0		479		0 6.67	OZ CZ	479		
449.195	483.482	(1)	426.62	0	4.12	No	449.53	0	3.59	ON			
415.533	421.533		449.47	0	2.28	No	415.63	0	0.5	ON			
393.28	406.28		415.61		0.32	No	393.9	0	10.54	ON		0	
348.925	348.925	0	393.76	0	6.39	ON No	349.83	0	.,	YES	350.24		
450.200	449.407	15.141	737 07	C	27.33	Sept N	444.49	0.92	5.1.5 5.70				
443.382	430.382	11.001	445.85	0	3.42	ON ON	436.09	0	49.68	O N			
442.07	447.07	5	434.56		40.15	ON	442.22	0	0.75	ON			
478.344	479.047	0.547	442.19		0.48	No	478.34	0	0	ON		0	
413.957	420.957		478.34		0	ON	415.13	0	54.12	ON			
404.53	411.53		415	0	43.16	ON	405.84	0	54.1	ON	405.9	0	
0	0	0	405.7		43.11	ON :	0	0	0 1	ON			
336 145	336 409	4 0	0 0	0	76 7	ON Sec	443.49	0 0	35.57	YES	446.83		
492.567	492.567	0	337.89	0	17.68	Yes	498.06	0	4.32	YES		0	
354	363.998	9.998	492.74	0	0.5	Yes	354.56	0	22.72	ON		0	

				Propo	Sed Co	Proposed Condition Junctions Results	ns Re	Sults S	umm	Summary Table			
imensions	S				2-year			1	10-year				100-ye
Invert evation (feet)	Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	May Ir (100-)
489.972	490.419	0	311.58		12.9	No	490.01		0.99	ON	490.03		
319.955	324.955	S		0	0.55	ON :	321.34	0	22.73			0	
406.116	406.116	0		0	12.95	ON	406.19	0	2.39				
375.226	375.226	7 153	406.1/ 375.69	0	1.34	Yes	375.82	0	17.64	YES	3/5.99		
423.02	416.522	14.322			9.81	ON	404.49	0	79.14				
421.8	437.233	15.433			46.61	No	423.55	0	41.83			0	
429.626	438.126	8.5		0	24.63	NO	430.88	0	21.7	ON			
443.331	447.831	4.5		0	12.93	ON :	443.83	0	4.46	ON			
462.385	469.885	7.5	443.71	0	2.55	ON Z	462.76	0	4.48	NO	462.87	0	
419.204	453.734	4.5		0	12.79	ON ON	450.15	0	62.05				
415.8	422.621	6.821		0	35.09	ON No	421.05	0	15.99			0	
403.376	419.876	16.5	416.91	0	12.92	No	414.27	0	31.38	ON	418.97		
407.033	411.533	4.5		0	22.17	No	415.95	0	3.92	YES			
413.4	433.957	20.557			1.86	NO	425.63	0	63.15	ON			
407.93	422.158	14.228			36.89	ON Z	410.16	0 71	64.08	ON Z	461.16		
353.793	357.793	0.0 A 5	372 16	2 54	37.0		353.87	6.75	6.15	ON CN		0.274	
326.427	329.427				3.44	NO N	326.8	1.22	1.22	ON			
440.891	441.85	0	326.71	0.71	0.71	ON	441.92	1.23	1.23	YES	441.93	0.057	
451.819	451.819	0		0.72		Yes	451.84	0.87	0.87	YES	45	0.03	
504	506.222	2.222	45	0.5	0	Yes	504	0	0	ON			
418.673	418.869	0 17	504	0 18	0 018	ON SON	419.05	0.27	0.27	YES	419.09	0.012	
419.441	426.441	7.		2.83		ON	419.44	0	0	ON			
418	426.009	8.009		0	0	No	418	0	0	ON			
310.585	314.085	3.5			0	NO	311.18	5.48	5.48	ON			
370.137	375.637	5.5		(1)	3.39	ON Z	371.05	2.98	31.21	ON 2			
372.14	374.524	0	370.92	1.8	1 60	02 2	375 16	7.8	78.87	NO	375 71	0.159	
300.311	304.811	4.5		2.71	21.66	Yes	301.57	1.49	33.82	ON			
497	499.014	2.014			19.08	NO	498.67	0	3.91	ON			
309.358	313.858	4.5	497.57	0	2.18	No	310.09	14.99	14.99	ON	313.41	0.989	
309.882	314.382	4.5		8.48	8.48	No	310.37	7.74	7.74		310.72		
306.317	310.817	4.5		4.3	4.3	No	307.17	4.61	19.59				
306.218	310.718	4.5		2.55	11.02	ON :	306.92	5.07	12.8	ON	(1)		
286.7	291.386	4.686		2.92	7.21	ON :	290.9	0.75	40.94	ON :			
287.521	291.021	3.5		0.46	23.95	ON 2	290.91	7.35	7.35	ON Six			
286.604	290.104	3.5		4.46	4.46	ON No	290.85	3.45	73.7	YES		0.216	
323.608	332.608	0	330.55		13.49	CN CN	0	79.67	79.67		332.22		
303.682	306.682	3	0		0	No	304.33	13.43	15.09		304.5	0.90	
454.567	454.91	0	304.16	7.68	8.5	No	454.67	0	11.93	ON		0	

				Propo	sed Co	Proposed Condition Junctic	ons Re	sults S	nmm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
				Max.	Max.		Max.	Max.	Max.				
Invert	Rim Elevation	Depth (feet)	Max. HGL	Lateral Inflow (2-	Total Inflow	Surcharging (2-vear)	HGL (10-	Lateral Inflow	Total Inflow	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	May
(feet)	(feet)	(leer)	(feet)	year)	year)	(Z-)cai	year) (feet)	year)	year)	(10-4-64)	(feet)	(100-year) (cfs)	(100-)
0	0	0	297.1		7.57	ON	0	0	0	ON	0	0	
296.45	301.45		0		0	No	297.	1.1	12.13	ON	298.0	0.04	
433.306	435.306				7.04	ON :		15.57	19.87	ON :			
432.339	437.339	5.5	434.16	8.92	11.29	ON ON	433.88	1.13	27.02	ON ON	434.51	0.056	
470.205	475.205	5			15.24	ON	4	4.41	4.41	ON			
429	441.503	12.503	470.72	2.6	2.66	No	429.7	0	7.69	ON	429.9	0	
0 269 727	0 475 588	5 861	429.57	0	4.54	ON N	470 5	0 0 47	0 4 86	ON CN	0 0	0 0 0 1	
470.747	475.747	5	470.28	O	2.95	ON NO	4	12.56	12.56				
469.845	474.845	5	471.51	7.27	7.27	No	470.5	4.29	4.29	ON	473.95	0.243	
468.335	474.763	6.428		7	2.58	No		0.63	24.04	ON			
469.45	476.339	6.889			14.38	ON Z		0.67	13.23	ON Z		0.028	
469.037	475.988	4.5	470.23	0.97	17.7	ON	470.02	1.7	1.7	OZ OZ	471.79		
465.742	472.234	6.492			1.09	ON		4.01	31.47	ON			
466.243	470.243	4	467.03	2.45	18.88	No	468.67	2.68	2.68	ON	470.92	0.13	
463.5	470.898	7.398		1.67	1.67	No	467.63	1	35.08	ON	470.23	0.045	
460.402	479.884	0 1	464.89	9.0	21.86	ON		0	0.22	ON S			
468.745	4/3./45	ر 1	460.42	1 72	0.I3	ON V	469.03	2.69	2.69		470.29	0.121	
470.033	474.533	4.5			1.35	ON ON		50.65	50.65	ON ON		1.63	
459.574	467.932	8.358			28.88	No		3.44	101.95	ON		0.17	
488.671	493.671	5			62.02	No	489.84	0.51	25.54			0.02	
457.564	466.564				13.1	No		3.08	88.88			0.138	
285.795	290.795	5	459.69		65.53	ON Z		15.31	21.86	ON		0	
293.131	293.037	D 14	280.3	8.97	12.51		12.562	8.82	32.82		293.24	0.52	
391.386	391.386	2	281.42		13.61	ON ON		H: 0	375.58				
318.429	323.429	5	392.75		274.05	Yes		2.8	2.8		(1)	0.20	
351.075	356.075	5	318.6		1.63	No		1.53	1.53	ON			
362.871	367.871	5	351.2		0.92	No	(1)	1.84	1.84	ON			
465.19	469.69	4.5			1.08	ON :		2.33	2.33	ON		0.144	
464.556	470.056	5.5	465.5	1.31	1.31	ON Z	464.95	2.15	4.47	ON Z	465.07	0.132	
433.983	440.483	7.4			3.3	ON ON		0.00	11.23		7		
434.879	439.379	4.5			6.49	No		5.91	5.91	ON		0.30	
460.503	465.003	4.5		3.4	3.45	No		2.14	2.14	ON			
430.532	435.032	4.5	460.69	1.27	1.27	ON	432.17	8.95	8.95	ON	437.93	0.434	
421.073	421.073	0		5.4	5.47	No		0	25.73	YES	7		
417.1	423.222	6.122	421.93		15.3	Yes		2.13	17.29	ON			
407.471	411.971	4.5	418.18	1.3 0.51	12.91	ON CN	419.31	1.81	7.41	YES	421.21	0.036	
405.459	408.959		408.6		1.12	No		5.58	9.03	YES		0.258	

				1			1			: 1			
				Propo	sed Cc	Proposed Condition Junctic	ons Re	sults S	nmm	Junctions Results Summary Table			
imensions	SI				2-year			1	10-year				100-ye
				Max.	Max.		Max.	Max.	Max.				
Invert	Rim	Depth	Max. HGL	Lateral Inflow	Total Inflow	Surcharging	HGL	Lateral Inflow	Total Inflow	Surcharging	Max. HGL	Max. Lateral	Max
evation (feet)	Elevation (feet)	(feet)	(2-year) (feet)	(2- year)	(2- year)	(2-year)	(10- year) (feet)	(10- year)	(10- year)	(10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	(100-)
77	C + C + C + C + C + C + C + C + C + C +	L	00.00	(cfs)	(cfs)			(cfs)	(cfs)	2			
470.312	4/4.812	V.4	470.93	1.52	1.52	ON Z	470.50	00.03	3.32		7		
497.003	474.674	U L	470.51		12.83	ON	469.87	1.22	1.22	ON ON	459.2	0.055	
422.797	422.797	0	469.84		0.78	No	422.93	0	10.77	YES			
465.8	475.718	9.918			6.44	Yes		0.93	3.23	ON			
476.55	481.55	2	466.05	9.0	2.05	ON NO		0.26	1.11	ON		0.012	
480.055	485.055	2	476.71		0.7	ON		0.86	0.86	ON S		0.043	
403.29	466.29	U I	400.2	0.53	0.55	NO NO	405.57	3.26	3.76	ON CN	403.30		
458.884	465.884	7	427.37		1.96	No		3.63	91.7	ON			
437.476	442.476	5	460.72		63.63	No	7	4.09	4.5	ON			
441.629	446.629	5	438		2.77	No	441.75	0.41	0.41	ON			
416.141	421.141	2	441.73	0.26	0.26	No	416.38	0.51	0.51	ON		0.024	
395.467	400.467	S C	416.33	0.32	0.32	ON Z	395.99	2.4	2.89	ON		0.122	
429.017 204 704	429.017	0 (993.00		1.79	ON SON	205 17	0 0	00.02	CIA	429.97	0 0	
202 015	400.704	15		C	2.00	S CN		0.45	57.6				
395.713	408.313	7			2.6	ON ON		7.22	10.75	ON ON			
396.209	401.209	2	396.62		6.54	OZ		3.62	3.62	ON	(1)		
389.999	404.999	15	396.71		2.21	No		4.64	85.49	ON			
388.18	393.18			()	48.01	ON		14.06	14.06	ON			
386.2	395.214				8.3	ON		96.0	17.57	ON			
387.3	392.925	5.625			10.53	ON		2.82	16.81	ON			
443.519	448.019	4.5			9.99	ON :		0.52	0.52	ON			
432.4	435.599	3.199	443.62	0.33	0.33	ON N	435.36	1.64 O	1.64	ON ON	436.83	0.096	
432	434.959	2.959			0	No		84.26	85.9	YES		4.02	
425.903	430.903	5	435.22	46.96	47.92	Yes		0.78	3.13	ON		0.037	
412.188	412.188	0	426.29		1.98	No	7	0.43	4.2	YES	•		
412.883	415.883	w r	412.81		2.67	Yes		0.45	0.45	ON			
428.438	433.438	v c	413.06	0.29	0.29	NO NO	428.64	0.64	1.69	NO	428.68	0.03	
427.83	434.83	7	413.53		1.07	Yes		1.73	2.37	ON			
501.677	501.677	0	428.09		1.5	ON		18.66	18.66	YES			
440.074	445.074	5	503.24	10	10.24	Yes		0.54	4.24	ON		0	
434.433	439.433	5	440.23	0.35	0.35	ON	434.7	2.29	2.29	ON	434.77	0.115	
0	0	0	434.65	1.42	1.42	ON	0	0	0	ON		0	
430.779	435.779	5	0		0	ON		1.49	52.15	ON		0.067	
433	435.855	2.855	431.6	0.95	41.88	ON		1.03	1.76	ON	433.28	0.044	
438.972	444.456	5.484			1.15	No	7	0.49	59.03	YES		0.021	
446.577	451.577	2	440.5		36.29	ON 2	447.1	5.78	5.78	ON S		0.378	
440.952	445.952	ν _π	446.98	3.41	3.41	ON S	445.22	6.3	6.3	ON S	446.14	0.415	
442.996	450.342	7.346			1.69	No	446.21	3.56	50.48	ON N			

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				Propo	sed Co	Proposed Condition Junctic	ons Re	sallts S	nmme	Junctions Results Summary Table			
imensions	SI				2-year			1	10-year				100-ye
				Max.	Max.		N N	Max.	Max.				
Invert	Rim	4	Max.	Lateral	Total	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	HGL	Lateral	Total	,	Max. HGL	Max. Lateral	Max
evation (feet)	Elevation (feet)	(feet)	(2-year)	(2-	(2-	Surcharging (2-year)	(10- year)	(10-	(10-	Surcharging (10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	lr (100-)
			(теет)	year) (cfs)	year) (cfs)		(feet)	year) (cfs)	year) (cfs)				
436.287	436.287	0	438.8	Ш	131.77	No	439.57	0	71.65	YES	439.63	0	
433.785	442.226	8.441			39.88	Yes		3.6	36.05	ON		0	
434.215	448.695	14.48			25.05	ON		0.67	34.06			0.03	
434.297	453.455	19.158	439.49	0.17	22.48	NO NO	442.58	15.66	15.66	YES	448.61	0.943	
434.639	442.218	7.579			9.28	Yes		0.62	16.29	YES			
434.421	445.129	10.708			12.77	NO			33.09	ON			
434.494	446.578	12.084	439.99		22.33	ON S	443.55	2.01	31.32	ON	450.76	0.091	
434.773	436.092	7 931	440.10	0.44	4 56	ON SAV		0.07	6.73	VES			
434.999	437.499	2.5	446.96	0.48	4.31	Yes	44	3.66	7.64	YES			
0	0	0			4.03	Yes		0	0	ON		0	
437.985	441.985	4			0	No	443.21	2.31	9.95	YES		0.109	
472.587	478.087	5.5			5.36	No		5.01	15.68	ON		O	
472.786	478.286	5.5			8.81	ON :		10.71	10.71	ON			
452.047	457.047	2	473.55	6.02	6.02	ON :		0.17	1.08	ON	7		
451.19	456.19	5	452.28	0.11	0.67	ON Z	451.36	0.26	1.32	ON S		0.012	
432.0	430.132	3.332	431.32		0.01			0.00	77.0		433.13	0.00	
453.183	458.183	U V	453.82		0.48	ON		0.07	0.84	ON ON			
427.572	433.072	5.5			0.52	ON		30.38	30.38	YES			
495.501	495.501	0	431.62	16.74	16.74	ON	495.66	0.86	0.94	YES	495.78	0.032	
424.5	432.562	8.062	495.65	0.53	0.82	Yes	427.76	0	212.93	ON	428.32	0	
450.604	450.604	0	426.64		110.08	No		0	5.35	YES			
370.654	376.654	9 7			3.15	Yes		41.87	41.87	ON			
331.0	398 826	12.37	397.91	1.86		ON ON	387.72	3.11	85.52 85.5	ON CX	393 07	0.165	
372.6	378.941	6.341			50.7	ON		0.19	102.09	ON		0.008	
435.55	441.67	6.12	374.41	0.12	60.57	No	436.39	8.83	8.83	ON	506.42	0.65	
441.27	449.524	8.254	436.15	4.92	4.92	No	441.82	8.83	8.83	ON	514.47	0.615	
430.42	437.457	7:037	441.68		4.98	No		8.89	17.64	ON		0.634	
433.55	441.867	8.317	431.6	5.01	9.9	ON N	433.89	1.23	1.23	ON	521.91	0.069	
744	454.010	7 280			0.70			1.11	7.17	ON CA		0.20	
444.34	432.229	4.233			4.19	ON ON		t C	72.55	OZ CZ			
435.68	443.849	8.169			13.01	ON		1.88	1.88	ON		0.08	
426.07	440.735	14.665		1.1	1.18	N		1.22	19.62	ON			
425.46	437.154	11.694	426.7	0.78	11.47	ON	426.42	13.85	22.14	ON	505.42	0.881	
454.8	470.709	15.909	426.17	8.23	13.01	ON	455.16	3.93	3.93	ON	535.01	0.232	
412.9	421.039	8.139			2.24	No		0.98	0.98	ON			
439.21	447.819	8.609	1		0.62	ON :		1.67	5.45	ON			
429.98	442.532	12.552	439.6	76.0	3.1	ON S	430.31	0.42	2.61	ON S	504.97	0.021	
400.3	454.93	8.13			1.59	ON ON		2.00	5.93	ON ON		21.0	

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				ropo	sea cc	Proposed Condition Junctio	ons Ke	Salits 5	nmm	Junctions Results Summary Table			
imensions	S				2-year			1(10-year				100-ye
			Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total			,	
Invert evation (foot)	Rim Elevation	Depth (feet)	HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	(10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	(100-year)	Max. Lateral Inflow	May I
انوورا	(lear)		(feet)	year) (cfs)	year) (cfs)		(feet)	year) (cfs)	year) (cfs)		(leer)	(TOO-Year) (CIS)	(-001)
425.9	434.028	8.128	440.8	1.41	1.41	No	426.51	4.19	21.76	NO	491.87	0.227	
432.62	443.875	11.255	426.35	2.54	12.3	No	432.91	0.32	2.2	ON		0.016	
405.99	414.128	8.138	432.85	0.2	1.38	ON Z	406.69	13.78	16.4	ON		0.796	
3/3	391./9/	18.797	406.53	8.15	9.71	ON ON	37.575	2.05	20.7	ON ON	3/3.2/	0.098	
368	387.892	19.892	367.56		25.76	ON N	369.17	0.38	33.95	ON		0.013	
405.627	405.627	0	369	0.24	25.66	No	405.79	0	22	YES		0	
386.848	386.848	0		0	20.21	Yes	386.85	0	0	YES			
361.75	401.214	4.214	386.85	0 0	0 80 80	Yes	399.42	0 23	42.34	ON ON	399.55	0	
418.4	426.734	8.334	362.69	0.15	25.79	ON ON	419.14	1.46	7.62	ON ON		70:0	
427.13	429.198	2.068	418.93	0.77	4.08	No	427.59	2.18	2.18	ON		0.142	
419.38	429.337	9.957	427.45	1.07	1.07	No	420.19	0	4.26	ON		0	
423.3	432.756	9.456	419.97	0	2.42	No	423.85	0.28	4.29	NO		0.013	
425.45	434.69	9.24		0.18	2.44	ON	425.97	0.22	4.04	ON	7	0.01	
427.56	436.554	8.994		0.14	2.28	OZ		0.31	3.86	ON		0.015	
430	438.444	8.444	427.91	1.07	2.17	ON Z		3.55	3.55	ON Z		0.251	
413.76	423.213	9.435	450.30	1.97	1.97			00.00	70.7		410.30		
417.00	423.183	3.086	417.27	0.03	0.78	ON ON	437.19	6.75	23.37	YES			
415.53	423.837	8.307	436.03	3.96	13.24	No	415.97	5.14	6.32	NO		0.313	
404.327	404.327	0	415.85	2.64	3.4	ON		0	6.32	YES			
381.44	381.44	0	404.49	0	3.4	Yes		0	7.89	YES		0	
423.62	425.75	2.13	381.73	0	4.25	Yes		0.08	0.08	ON		0.004	
423.07	425.202	2.132	423.72	0.05	0.05	ON N	423.13	0 0	0.08	ON	423.15	0	
427.47	435.598		424.12	0.58	0.58	ON NO	436.6	1.41	25.16	YES		0.063	
427.06	435.532		435.9		21.93	Yes	434.95	0.91	0.91	NO		0.04	
422.786	422.786	0	434.38	9.0	9.0	No	424.07	0	22	YES	424.43	0	
419.982	419.982	0	424.03	0	20.21	Yes	420	0	0.47	YES			
448.398	448.668	0 0 0	419.99	0 0	0.3	Yes	448.4	0 20	0 0	ON ON	448.4	0 0	
378.818	378.818	0.50	417.05	0.1	0.16	OZ OZ		0	0	YES		0	
454.41	461.531	7.121	378.82		0	Yes		1.71	1.71	ON		0.097	
459.72	465.839	6.119	454.58	0.99	0.99	OZ	482.02	4.43	4.65	YES		0.241	
458.887	465.476	6.589	460.13	2.6	2.6	No	480.85	3.32	8.93	YES	475.82	0.201	
462.2	469.35	7.15	459.58		4.51	ON	468.41	5.32	5.32	ON		0.311	
461.25	469.366	8.116	462.63	3.07	3.07	ON	467.89	3.01	8.31	ON			
454.3	461.807	7.507	461.72	1.74	4.81	ON	463.32	0.39	2.66	YES	7		
454	461.576	7.576	457.83	0.22	0.89	OZ	463.24	6.95	19.43	YES		0.413	
455.285	466.09	10.805	457.78	3.92	11.63	ON 2	465.03	0	16.96	ON		0	
451.007	451.007	0 7 504	458.23	0	9.1	ON X	451.01	0 2	0 2 2	YES	451.01	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
450	462.577	12.577	455.74	3.2	3.29	ON	461.69	0	15.33	ON		0	

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				Propo	sed Co	Proposed Condition Junction	ons Ke	Salits 5	umm	Junctions Results Summary Table			
imensions	SL				2-year			1	10-year				100-ye
				Max.	Max.		Z	Max.	Мах.				
Invert	Rim	Depth	Max. HGL	Lateral Inflow	Total Inflow	Surcharging	HGL	Lateral Inflow	Total Inflow	Surcharging	Max. HGL	Max. Lateral	Max
evation (feet)	Elevation (feet)	(feet)	(2-year) (feet)	(2- year)	(2- year)	(2-year)	(10- year)	(10- year)	(10- year)	(10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	lr (100-)
			,	(cfs)	(cfs)		(teet)	(cfs)	(cfs)				
455.84	462.968	7.128	456.52	1.11	1.11	No	457.15	2.98	2.98	NO	468.01	0.167	
451.63		8.131			1.73	No		0.87	1.98	ON			
446.59		8.134			0.53	oN :		3.77	4.74	ON			
447.52	455.647	8.127	446.92	2.24	7.85	ON CN	451.12	1.05 1.5	1.37	ON ON	456.44	0.054	
433.086	436.086	3			0.7	ON		3.37	38.29	YES			
455.02		8.129	436.44	1.89	22.33	Yes		0	4.87	NO			
454.84	462.956	8.116		0	2.83	No		0	8	NO			
451.2	461.323	10.123	455.23		4.4	ON A		2.26	2.26	ON 2	7	0.10	
448.145	461.115	12.97	452.92	L:3	12.27	ON N	459.72	0	14.9				
442.293					22.51			0 0	27.31	YES	430.12		
450.383					20.24	ON ON		0	11.4	ON			
453.29	461.411	8.121			10.57	N		0	1.95	ON			
448.479	461.429	12.95	453.48		0.99	No	460.1	0	14.93	NO	462.19		
445.945	459.331	13.386		0	12.99	ON		0	19.42	ON			
407.161		0		0	15.69	ON		0	3.35	ON			
447.26		8.129	,		1.86	ON No		8.26	8.26	NO		0.4	
454.914	458.048	3.134	447.6	4.8	4.87	ON S	454.91	0	0	ON	454.91		
452.03		3.02			0 0				0 0	ON ON			
446.342		3.62		0	0	ON		0	0	ON			
443.954		3.62	446.34		0	ON		0	0	ON			
440.498	444.118	3.62	443.95	0	0	ON	440.5	0	0	NO	440.5		
437.81	441.43	3.62	440.5		0	No		0	0	ON		0	
434.691	7	3.62	437.81		0	No		0	0	ON			
433.39		3.62	434.69		0	ON :		0	0	ON	7		
455.323	455.323	0 ,	433.39	0	0 0	ON		0	4.51	YES			
424.863	427.013	2.13	457.47		1.05	CN CN	423.19	0	2.15	ON C	425.29		
448.899	460.179	11.28			1.06	O Z		0	6.34	ON			
399.535	405.165	5.63	7		3.32	ON		0	7.89	ON	7		
423.75	430.339	6.589	399.83	0	4.25	NO	423.92	0.48	0.48	NO		0.024	
423.5	427.792	4.292	423.89	0.3	0.3	ON	425.99	2.54	22	ON	431.39	0.108	
458.121	460.241	2.12	425.66	1.53	20.21	NO	458.12	0	0	NO			
423.004	425.134	2.13			0	ON	423.2	0	0.89	ON		0	
372.025		0	423.17		0.57	ON		5.77	33.91	YES			
392.179	392.179	0			25.61	Yes		5.84	33.98	YES		0.48	
422.52	433.735	11.215		1.7	24.59	Yes	425.94	0	203.71	ON	426.7		
0	0	0	424.84		103.69	No		0	0	ON			
378.247	378.247	0	0 020		0 "	No	(1)	0	30.17	YES			
3/3.582	373.582	0	378.85	0	23.12	Yes	377.07	0	37.18	YES	377.56		
756 759	456.759	0	377	0	25.32	Yes		2.27	2.27	YES		0.27	

100-ye

Ma) Ir (100-)

					-		1			:			
				Propo	sed Co	Proposed Condition Junctic	ons Ke	Sults 5	nmm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
				Мах.	Мах.		M	Мах.	Max.				
Invert	Rim :	Depth	Max. HGL	Lateral Inflow	Total Inflow	Surcharging	HGL	Lateral Inflow	Total Inflow	Surcharging	Max. HGL	Max. Lateral	May
evation (feet)	(feet)	(feet)	(2-year) (feet)	(2- year)	(2- year)	(2-year)	(10- year)	(10- year)	(10- year)	(10-year)	(100-year) (feet)	(100-year) (cfs)	(100-)
				(cfs)	(cfs)		(teet)	(cfs)	(cfs)				
443.669	443.669	0	293.62	0.07	25.25	ON	444.29	0	14.15	YES	444.37	0	
431.82	439.226	7.406			7.82	Yes	432.33	1.52	6.01	ON		0.07	
335.08	357.698	7 335	337 07	0.94	3.57	ON ON	349.78	4 46	35.66	ON C	347.69	0 0	
412.22	420.404	8.184		2.5	22.14	ON No	412.55	0.96	0.96	ON			
407.928	407.928	0	412.47	0.0	9.0	No	408	0	5.98	YES			
342.317	342.317	0			3.55	Yes		0.71	23.19	YES			
360.341	360.341	0	344.35	0.46	17.2	Yes	362.48	19.67	21.41	YES	362.49	0.031	
432.82	440.412	7.592			13.12	Yes	433.27	4.51	4.51	ON			
387.525	387.525	0			2.64	No	389.06	12.99	14.77	YES			
0	0	0	388.6	7.5	8.65	Yes	0	0	0	ON			
411.92	418.789	698.9			0 7	ON N	412.35	1.18	2.13	ON		0:0	
373.477	373.477	0 0	383.77	0.72	4.01	Ves	373.67	0 0	15.48	YES	373.7		
355.51	355.51	0			10.03	Yes	356.7	0	11.91	YES	(1)	0	
406.459	406.459	0	355.75		5.85	Yes	406.49	0	2.11	YES	406.51	0	
337.12	357.484	20.364	406.48		1.3	Yes	338.24	0	49.03	ON		0	
350.45	356.52	6.07	337.99		31.22	No	353.45	31.33	31.33	ON		1.3	
345.995	345.995	0		19	19.6	NO :	346.59	0	23.12	YES		0	
365.027	365.027	0			17.16	Yes	367.16	14.4	18.33	YES	m	0.58	
350.448	350.448	0		, o	E 2E	Yes	352.47	75 20	26.12	YES			
354.155	354.155	0 0	351.62	15.53	0.45	YP YP	357.36	77.07	38.20	YES	350.5	L.33	
350.949	350.949	0			10.89	Yes	357.36	2.25	21.57	YES		0.09	
350.105	350.105	0	354.15	1.48	11.13	Yes	356.7	0	38.68	YES			
348.91	348.91	0	353.64	0	13.07	Yes	356.7	12.58	24.2	YES		0.503	
388.104	390.234	2.13		7.8	17.27	Yes	388.33	0	5.7	ON		0	
349.134	349.134	0		0	3.34	ON No	356.7	0	49.51	YES	,	0	
348.967	346.967	6 399	379 77		32 44	Yes Ves	373.78	0 0	76.00	CN ON	321.9	0.37	
373.61	378.66	5.05		2.3	16.24	ON	375.36	25.13	25.13	ON		1.86	
412.19	426.462	14.272	374.48		13.9	ON	413.4	0	24.86	ON		0	
414.5	421.106	909'9	413.05	0	13.85	NO	416.04	24.86	24.86	ON	423.6	1.87	
408.751	408.751	0	415.54	13.82	13.82	ON	408.83	0	24.83	YES	408.86	0	
336.02	341.742	5.722			13.85	Yes	m	0.42	0.42	ON	(1)	0.01	
309.391	309.391	0		0.5	0.25	ON	309.4	0	0.41	YES		0	
329.402	329.402	0			0.25	Yes	329.96	0	49.18	YES	m		
380.182	380.182	0	.1,		31.3	Yes	380.7	0	124.98	YES			
303.185	303.185	0	380.7		124.98	Yes	312.19	0 0	1/8.06	YES	313.0		
0	0	0			0 0	ON	0	0	0	ON	0	0	
439.754	442.524	0.524			0	NO	442.39	0	16.81	ON	442.4		
399.04	405.421	6.381	442.31	0	8.6	No	404.13	0	110.25	ON	404.95		

Proposed Condition Junctions Results Summary Table

				200	3		- 1):≥5. k			
imensions	S				2-year			,	10-year			` '	100-yea
			Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total		707	700	
evation	u	Depth		Inflow	Inflow	Surcharging	(10-	Inflow	Inflow	Surcharging	(100-year)	Inflow	Na.
(feet)	(feet)	(reet)	(2-year) (feet)	(2- year) (cfs)	(2- year) (cfs)	(Z-year)	year) (feet)	(10- year) (cfs)	(10- year) (cfs)	(10-year)	(feet)	(100-year) (cfs)	(100-)
284.72	287.162	0	288.88			No	284.72	0		ON	284.72	0	
290.031	290.3	0						2.99	2.9		290.07	0.18	
284.023	289.023	5		1.69	1.69			0			284.02		
286.259	291.259	5		0				0			286.26	0	
390.636	390.636	0		0				0			390.64	0	
456.901	456.901	0 1	390.64	0	0 4 5 8	Yes	456.95	0	4.62	YES	456.95	0	
432.83	434.83	2		0							424:12	0	
432	439.133	7.133		0				0			432	0	
427.5	438.767	11.267	432	0	0		428.28	0	7.69	ON	428.51	0	
444.596	450.096	5.5	428.1	0	4.53		446.69	51.89	53.83	ON	477.68	3.62	
279.406	284.406	2		28.54	29.5			0				0	
278.841	289.841	11		0				0				0	
276.159	288.337	II	278.84			ON ON	276.34		0 0	ON C	277.34		
396.068	396.068	0		0	0.5			29.15	(1)			1.71	
272.269	277.269	5	397.83	15.9	20.75	Yes	274.64	0	5.16	ON	276.28	0	
279.665	284.665	5	274.23	0		NO		0	0.96	ON	279.91	0	
282.607	287.607	5		0	0.5			0			282.61	0	
273.809	278.309	4.5		0		ON		0			278.9	0	
285	287	2	7			ON 2		0			286.09		
284.5	788.1	3.0	285.6		4.34	ON ON	285.31		7.61	OZ Z	285.6	0	
282.5	288.17	5.6	.,	0		OZ Z		6.8			284.84	0.375	
		<null></null>		3.7			<null></null>	<null></null>	<null></null>	#VAL		<null></null>	<null></null>
429.307	429.307		<null></null>	<null></null>	<null></null>	Yes		0	0.35	YES	429.41		
335.956	335.956	0			0.2			0			335.96		
302.981	307.481	4.5	335.96	0		Yes	302.98		0 0	OZ Z	302.98	0	
297.613	302.613	5.5						0			297.61	0	
289.103	294.103	5	297.61	0	0		289.1	0		ON	289.1	0	
307.266	307.392	0		0				0	0		307.27	0	
283.742	283.742	0						0			284.83	0	
279.146		0		0		ON	280.18	0	_	ON	281.71	0	11
200 67	341.7	<iiin></iiin>	2/9.96	/IIII	/9/		<iiiii></iiiii>	<nul></nul>	<null></null>	#VALUE!	<null></null>	< nN >	<iiin></iiin>
308.57	314.57	٥ ٥	309 48	< Inni>		Yes							
473.859	473.859	0 0										D C	
422.03	422.03	0					422.46		C.		422.51		
408.713	417.122	8.409						0			413.65	0	
329.574	330.639	0	411.13	0	33.6	ON	333.82	0	(4	YES	335.13	0	
338	340.918	2.			` '			0	9		339.99		
391.511	396.011	4.5	339.46	0	33.3				4.51		392.35	0	
399.3/4	399.3/4	O		0		INO	399.37	0	0	NO	399.37	0	

				Proposed Cond	sed Co	ondition Junctions Results Summary Table	ons Re	esults S	umm	ary Table			
imensions	S			-	2-vear			1	10-vear				-
Invert evation (feet)	Rim :levation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year) (cfs)	Surcharging (2-year)	5 ± 0 % €	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. F (100-yv (fee	Max. Lateral Inflow (100-year) (cfs)	1
402.294	402.294	0	0		0	No		0	1.06	YES			0
376	378.889	2.889	402.33		0.64	Yes			339.53	YES			0
374.214	375.214	0	379.12	0	194.65	Yes	s 375.64	0	399.03	YES	376.26		0
367.076	367.076	0	374.6		221.45	Yes			464.01	YES			0
358.082	358.082	0	371.12		285.64	Yes	s 363.39		440.04	YES			0
391.492	394.492	3	361.92		285.15	Yes			10.24	ON			0
38b 428 66	390.022	4.022	392.94	0 0	3.05	ON ON	478.66		87.02	AES ON	395.57		5 C
431.296	431.296	0	428.66		0	ON			1.93	YES			0
419.927	419.927	0	431.33		1.11	Yes	s 421.04		41.47	YES	421.36		0
0	0	0	420.77	0	21.18	Yes		0	0	ON			0
373 791	0 273 791	0 0	0		0	ON	0 0		0 0	NO	378 8		0 0
373.41	373.41	0	377.49	0	147.12	Yes		0	15.53	YES	(1)		0
343.804	343.804	0	377.5		7.74	Yes	s 350.07	15.4	471.73	YES	350.12	1.04	C +
364.917	364.917	0	349.27	0.6	265.31	Yes			5.23	YES			0
334.377	339.877	5.5	365.24		3.18	Yes			898.32	NO			0
335.843	335.843	0	338.1	0	570.16	No	342.06	6.52	489.22	YES	342.45	0.321	-
314.352	314.352	0	0	3	0	ON	314.8		15.82	YES	315.2		0
422.077	433.577	11.5	314.74	0	11.81	Yes		0	201.71	ON			0
444.1	451.752	7.652	423.94		103.3	No			5.52	ON			0
377.895	378.238	0	444.61		3.14	No			1.53	ON	37.		0
383.758	388.008	4.25	377.91	0 0	0.92	ON ON	383.96		165.45	ON ON	384		0 0
396.2	400.698	4.498	404.44		119.53	ON N		0	201.6	ON			0
436.531	441.031	4.5	398.08		142.84	ON	4		70.52	ON			0
441.489	446.989	5.5	439.59		39.37	No	7		0	ON			0
392.364	397.864	5.5	441.49	13 23	0 0	ON	393.6	21.96	28.46	ON Z	394.06		N 0
379 57	334 52	ש ת	393.29		119.4	ON S			421.85	VES		0.212	V (C
381.627	386.127	4.5	333.49		227.72	ON N			22.54	ON			_
380.896	385.896	5	382.48		12.57	No			37.52	ON		0.012	~
452.01	459.236	7.226	381.95	0.18	21	No		0	155.15	NO			0
280.66	280.66	0	453.9		104.34	No	283.4		1092.99	YES	284.8		0
0	0	0	0		0	ON :			0	ON			0
0 0	00 000	00 0	0 42E 4E	0 0	0 202	ON	0 0	77 77	77 77	ON Z	73 364		يا د
454.3	455.264	3.00	453.45		5.65	ON ON	7		12.47	ON			0 00
451.855	456.355	4.5	452.41		4.48	ON N			8.14	ON	45		
398.477	403.977	5.5	399.39		24.32	ON			40.68	ON			0
388.508	394.008	5.5	389.58		24.51	No			41.18	ON			_
368.507	373.007	4.5	369.38	6.52	7.56	No	369.96	12.48	14.84	NO	373.35	0.762	~

100-ye

Ma

(100-)

				(-		6	-		-			
				Propo	sea co	Proposed Condition Junctic	ons Ke	Salits 5	umm	Junctions Results Summary Table			
imensions	SL				2-year			1	10-year				100-ye
			Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total				
Invert evation (feet)	Rim Elevation (feet)	Depth (feet)	HGL (2-year) (feet)	Inflow (2- year)	Inflow (2- year)	Surcharging (2-year)	HGL (10- year) (feet)		Inflow (10- year)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	Ma)
418 758	473 258	A 7	418 94	(cfs)	(cfs)	Z		(cfs)	(cfs)	Z	419 03	0.028	~
331 454	331 454	î C			653 14	Service Servic		t C	884 54				
432.528	437.028	4.5		4.7	4.71	ON N		7.95	7.95			0.63	10
430.902	435.402	4.5			6.1	ON		2:32	10.26				~
430.835	437.335	6.5			1.17	No		1.97	1.97				8
368.519	373.019	4.5			5.7	ON		0.87	10.37				
430.99	430.99	0 7 7	431.32	1.54	2.88	Yes	431.42	2.56	4.85	YES	431.53	0.132	
445.979	451.979	9			16.91	ON		1.93	30.12				
449.7	455.7	9			5.21	NO		1.72	8.27				
0	0	0			0	No		0	0		0		0
0	0	0		0	0	No		0	0			0	0
367.455	367.455	0	367.46	7	0.13	Yes	367.46	0 2 3	0.21	YES	367.46	FC 0	
0	0	0			0	ON	1.17	0	0			73:0	
0	0	0		0	0	No		0	0				0
0	0	0			0	No		0	0	ON)
0	0	0			0	No		0	0				0
0	0	0	0	0	0	ON CA	0	0	0		0		
		0 0			0 0	ON ON			0 0	ON C			
0	0	0			0	N		0	0				
0	0	0			0	No		0	0)
440.598	441.439	0	440.8		3.09	No	440.9	0	5.46		441.0		0
0	0	0	0	0	0 0	O Z	0	0	0 0	ON C	0	0	
0	0	0			0	ON		0	0				
0	0	0			0	NO		0	0				0
0	0	0	0	0	0	No		0	0		0	0	0
900 202	900 000	0 2	1 705	71	1 03	ON ON	207 17	1 65	1 65	ON ON	207	20 0	0
398.346					0.78	ON		1.27	1.27				
401.57					2.12	ON		3.46	3.46				7
0	0	0			0	No		0	0				0
333.579	339.079	5.5	336.0		660.04	ON	336.6	0	994.41		336.8		0
0	0	0	0	0	0	ON Z	0	0	0	ON S	0	0	
403.07	407.07	0 4	403.2	0.6	0.67	ON	403.	1.07	1.07		403.3	0.04	
0	0	0			0	No		0	0				0
0	0	0	0	0	0	No		0	0			0	0
0	0	0			0	No		0	0				0
0	0	0 "	0	0	0	ON Z	0	0 77	0 70 07	ON		0	0
477.000	337.274	0.5				Yes			27.96		537.120		

				•	-		•						
				Propo	sed Co	Proposed Condition Junctic	ons Re	sults 5	nmm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
				Max.	Max.		Max.	Max.	Max.				
Invert	Rim	Depth	Max. HGL	Lateral Inflow	Total	Surcharging	HGL (10-	Lateral Inflow	Total	Surcharging	Max. HGL	Max. Lateral	May
(feet)	(feet)	(feet)	(2-year) (feet)	(2- year)	(2- year)	(2-year)	year)	(10- year)	(10- year)	(10-year)	(feet)	(100-year) (cfs)	(100-)
				(cts)	(cfs)		(leer)	(cfs)	(cfs)				
443.026	448.526	5.5		8.29	8.29	No	443.87	15.07	15.07	ON			
437	442.916	5.916		1	4.14	ON		2.4	6.82	ON S	7		
321.137	731 387	4.25	321.83	7.56	19.51	NO NO	322.09	7.30	34.87	ON CN	322.8	0.500	
407.347	411.017	3.67			0	ON N		o i	0	ON			
411.927	415.597	3.67	411.93		0	No	411.93	0	0	ON			
399.296	399.296	0	401.05	0	3.43	Yes	401.08	0 ,	6.12	YES			
430.397	433.397	2 254	430.63	1.06	1.06	ON ON	430.7	1.8	1.8		432.08	0.119	
430.72	434.594	3.874			1.87	ON		2.07	3.12	ON		0.127	
0	0	0			0	No		0	0	ON			
379.112	383.112	4	379.45	0.92	0.92	No		1.54	1.54	ON	379.68	0.078	
337.71	337.71	0		26.34	45.8	Yes		46.63	83.99	YES			
446.857	451.107	4.25	7		3.18	ON :		5.62	5.62	ON			
360.343	388.343	78			32.24	ON 2		19.17	47.78	ON S			
409.786	414.286	4.5			3.45	ON TO	7	6.16	6.16	ON S			
398 477	436.912	4.5	432.63	1.81	11.81	NO SAY	432.7	3.19	3.19	NO	432./8	0.159	
410.045	413.045	0 ~	413	3,4	3.48		413.05	6 47	6.47	YFS		0 338	
440.398	444.898	4.5	440.66		2.16	ON	440.73	3.6	3.6	ON			
433.958	436.958	3	437.41	0.57	2.72	Yes	437.45	0.0	4.48	YES	437.49	0.042	
387.672	387.672	0	387.82	4.84	4.84	Yes	387.85	8.33	8.33	YES	387.88	0.49	
449.983	449.983	0		0	0	ON	449.98	0	0	ON		0	
298.493	301.993	3.5			2.87	ON		4.94	61.13	ON)	
298.901	302.901	4 4		H	11.37	ON 2		20.47	98.58	YES			
320 989	375 489	4.203	321 31	1.57	1 57	ON ON	321.42	2.19	7.86	ON C	321 54	0.111	
320.264	324.764	4.5			2.41	No		1.49	4.34	ON			
369.07	369.494	0.424	372.31	0	208.33	Yes	372.7	0	308.51	YES	372.85	0	
313.437	317.937	4.5			2.85	ON	313.76	5.02	5.02	ON			
338.278	338.278	0	338.68		6.95	Yes		9.63	13.3	YES			
330.32	330.32	0	330.6	2.55	3.81	Yes	330.77	4.59	9.89	YES	330.98	0.244	
362 830	362 620	0 0	311.44		0.90	Sea Les		3.07	1005 03	CIT			
433.124	438.124	0 14	433.8		740.30	S NO		9.55	1093.03	CN			
426.3	430.8	4	7		11.18			19	20.05	ON			
444.322	444.322				0.91	Yes		0	1.53	YES			
462.187	465.857	3.67	462.43	0.91	0.91	ON	462.51	1.54	1.54	ON		0.07	
424.931	430.431	5.5	425.83		16.38	ON	426.17	0	29.29	ON	426.64		
0	0	0	0		0	No	0	0	0	ON		0	
431.617	434.617	m	432.73		5.99	OZ Z	432.73	2.55	5.99	ON		0.082	
432.276	434.276	7	432.97	3.46	3.46	ON No.	432.97	3.46	3.46	NO	432.97	0.10	
470.135	470.135	0	470.13		0	NO	470.13	0	0	NO		0	

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				rropo	פמ כנ	Proposed Condition Junction	אווא אוונ	salls 3		Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
			Max.	Max. Lateral	Max. Total		Max.	Max. Lateral	Max. Total			,	
Invert evation	Rim Elevation	Depth (feet)	HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	HGL (10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	May Ir
(reet)	(reet)		(feet)	year)	year)		year) (feet)	year) (cfs)	year)		(reet)	(100-year) (cfs)	(-00T)
449.513	449.513	0	449.82	5.82	5.82	Yes	449.89	10.29	10.29	YES	449.98	0.612	
396.521	400.521	4	397.84	` '	15.66	No	398.49	22.82	29.66				
437.614	442.114	4.5	437.91	2.23	2.23	ON 2	438	4 (4 11	ON	7	0.19	
798 292	798 292	5.991	410.47	0 0	45.24	NO X	411.06	0	17.77	NO	302.08		
427.435	430.435	· κ	427.8	2.2	2.21	ON	427.92	3.82	3.82			0.20	
361.942	366.442	4.5			7.36	No	362.95	12.97	12.98				
358.777	363.777			01	22.43	ON	360.6	16.68	39.65				
359.051	363.551	4.5	360.12	5.1	5.1	NO N	360.65	8.96	8.96	OZ CZ	351./4	0.50	
351.671	351.671	0	351.71	0	0.33	Yes	351.72	0	0.54		351.7	0	
352.442	355.442	3	352.58	0.17	0.17	No	352.65	0.28	0.28	ON	352.7	0.01	
356.717	356.717		356.74		0.33	Yes	356.75	0	0.61	YES			
357.838	359.838	7	358.1	0.45	0.45	ON ON	358.2	0.79	112.2	OZ Z	358.36	0.032	
293.532	293.532	0	297.17		722.72	Yes	297.77	0	1076.17	YES			
357.021	363.021	9	358.44	6.3	63.4		358.96	10.68	109.87	ON		0.49	
324.518	329.518	2	325.99	1	47.34	ON	326.75	24.04	79.76				
0	0	0	0	0	0	ON	0	0	0	ON	0	0	
323.25	329.25	9			112.74	ON	326.27	3.21	193.47				
307.735	314.235	6.5			128.11	No	310.67	13.2	219.58				
317.905	324.405	6.5		` '	124.16	ON :	320.54	24.21	212.96				
343.742	343.742	0			36.07	Yes	344.27	3.42	64.67				
388.1/8	392.678	4.5	388.55	7.37	7.37	ON Z	388.68	4.28	4.28		388.85	0.255	
323.814	323.814	0.4			6.39	Yes	323.97	0	11.52				
311.843	311.843	0	314.18		666.85	Yes	314.51	0	884.75				
286.491	290.991	4.5			21.26	No	288.04	7.31	38.1				
289.44	293.94	4.5		12	17.13	ON :	290.55	22.12	30.18				
2/2.351	276.60I	4.25	2/4.12	1.6	4.55	ON ON	281.48	2.69	5.6	YES	280.99	0.152	
282.8	286.59	3.79	283.56	0.5	1.38	ON ON	283.98	0.89	2.44	ON		0.03	
288.332	288.552	0	288.33		0	N		0	0	ON			
283.664	286.664	3	283.76	0.18	0.18	NO	283.97	0.29	0.29	ON	284.84	0.01	
287.793	292.293	4.5	287.99	1.01	1.01	ON	288.05	1.73	1.73	ON		0.074	
381.253	381.253	0	381.25		0	ON	381.25	0	0	ON			
342.789	342.789	0	343.21	1.6	1.61	Yes	343.34	3.02	3.02			0.1	
299.021	CTT 116	0	302.40		1 63	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	202.00		50.60	YES	303.12		
364.772	364.496	0	364.58	0	0.24	Yes	364.6	0	3.07	YES			
364.832	367.832	e e	365.08	0.3	0.36	ON	365.17	0.65	0.65	ON		0.02	
0	0	0	0		0	N	0		0	ON			
390.481	390.481	0	390.48		0	No	390.48		0	ON			
365.526	368.517	0	366.54	0.98	0.98	No	366.55	1.82	1.82	NO	366.56	0.084	

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				Propo	sed Co	Proposed Condition Junctic	ons Ke	Sults 5	umm	Junctions Results Summary Table			
imensions	SI				2-year			1	10-year				100-ye
				Max.	Max.		N N	Max.	Max.				
Invert	Rim	Depth	Max. HGL	Lateral Inflow	Total	Surcharging	HGL	Lateral Inflow	Total Inflow	Surcharging	Max. HGL	Max. Lateral	Max
evation (feet)	Elevation (feet)	(feet)	(2-year) (feet)	(2- year)	(2- vear)	(2-year)	(10- year)		(10- year)	(10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	Ir (100-)
				(cfs)	(cfs)		(feet)	(cfs)	(cfs)				
339.343	339.343	0	339.34		0	N		0	0	ON	339.34	0	
289.196	289.196		292.02	0	724.61	Yes	292.53	0 6	1079.64	YES	293.41	0	
330.673	339.000	4 C	330.7		0.07			I.39	1.53			0.00	
361.332	361.332	0	361.33		0	ON		0	0	ON			
369.974	370.069	0	369.97		0	No	369.97	0	0	ON	369.97	0	
325.299	325.299	0	325.35		2.03	Yes		0	3.6	YES		0	
335.384	335.384	0 7	335.67	2.04	2.04	Yes	335.76	3.61	3.61	YES	335.86	0.176	
306.435	310.685	4.25			6.93	ON ON		3.38	11.74	OZ OZ		0.218	
310.145	313.645	3.5			2.41	No		1.19	3.73	ON		0.074	
322.381	326.631	4.25			14.69	No		24.55	26.44	ON			
344.652	344.652	0			1.21	Yes		2	2	YES			
338.439	339.368	0		0.1	0.19	ON ;		0.31	0.31	ON		0.0	
325.41/	325.417	0	325.42		0 0	Yes		0	0	YES			
360.875	360.875	0 2			0 00	Yes		0 6	0 05 00	YES			
356 573	361.564	6.564	355.90	11.01	11.02	ON ON	356.37	19 37	19 37	OZ CZ	357.36	121	
414,171	414.837	0	414.17						0	CZ			
355.647	355.797	0	355.65		0	ON		0	0	ON		0	
385.759	389.259	3.5	386.65	10.08	10.78	No	387.02	17.65	19.03	ON		1.16	
385.226	389.726	4.5		1.78	12.42	ON		3.09	21.99	ON		0.172	
417.533	417.701	0	418.06		23.16	Yes		0	39.62	YES		0	
409.422	409.422	0	409.62		0.31	Yes	7	0.54	0.54	YES		0.021	
326	328.439	2.439	326.31	1.44	1.44	ON S	326.4	2.37	2.37	ON Z	330.04	0.113	
330.039	353.339	4.5	347 13		7 57			0.65	4.77	OZ CZ		7000	
0	0		0		0	ON N		0	0	ON		0	
369.362	373.862	4.5	369.6	0	2.16	No	369.67	0	3.64	ON	369.75	0	
369.679	374.179	4.5	370.14	2.17	2.17	No	370.29	3.64	3.64	ON	370.48	0.161	
432	432.923	0.923	432.32		1.35	No		2.3	2.3	ON		0.119	
385	401.047	16.047			0.27	ON A	385.21	0.05	0.43	ON Z	385.26	0.002	
300.133	350.403	67.4	300.20	0.24	00.24	ON		0.59	0.39 A7 E6	NO		0.014	
412.288	389 31	6.31	383.37	1,6	1 89	S ON		2 96	3.38	CN		0.15	
376.6	377.153	0	376.64		2.44	ON.		0.0	4.26	ON		0.034	
342.615	347.115	4.5	343.14		96.9	N		10.39	12.34	ON		0.519	
329.839	335.339	5.5	330.98	0.99	21.11	No	331.44	1.57	37.81	ON		90.0	
330.274	335.024	4.75	331.26	8.63	11.81	No	331.7	15.11	20.92	ON		0.963	
334.501	334.501	0	335.12	3.1	3.18	Yes	335.35	5.78	5.8	YES		0.295	
332.061	337.061	S.	337.13		0 !	Yes	337.13	0	0.01	YES		0	
438.01	442.01	4	438.51		4.5	ON CA	438.67	1.69	7.38	ON Z		0.076	
440.645	444.645	4 L	441.20	3.33	3.33	ON ON	442.23	8.06	T.0		445.20	0.304	
	0												

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				Propo	sed Co	Proposed Condition Junctic	ons Ke	Sults >	umm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
				Max.	Max.		M	Max.	Мах.				
Invert	Rim	Oonth h	Max.	Lateral	Total		HGL	Lateral	Total	Surcharaina	Max. HGL	Max. Lateral	May
evation (feet)	Elevation (feet)	(feet)	(2-year) (feet)	(2- vear)	(2- vear)	(2-year)	(10- year)	(10- year)	(10- year)	(10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	1r (100-)
				(cfs)	(cfs)		(feet)	(cfs)	(cfs)				
425.421	425.421	0	426.25	5.46	5.46	Yes	426.29	89.6	89.6	YES	426.33	0.701	
437.822	442.322	4.5	7		3.83	ON :		6.79	6.79	ON			
437.238	441./38	4.5			4.37	ON Z		0.85	7.66	OZ Z			
432.714	430.30	4.5	434.05	0.75	9.00	ON ON	434.22	1.19	7.16	ON ON	437.21	0.028	
433.052	437.552	4.5			3.84	No		9.9	9.9	ON			
437.381	441.881	4.5		0.62	0.62	No		96.0	96.0	ON		0.041	
429.747	441.747	12		0	4.01	ON :		0	6.87	ON		0	
288 888	431.438 304 308	0.438	431.12		5.80	ON N	390.12	1 52	71 57		431.12 390.42	90 0	
437.691	438.013	0.0	438.09		0.61	Yes		0.98	0.98	YES			
438.048	438.048	0	438.66		3	Yes		5.25	5.25	YES			
428.178	433.178	5	428.93	9.51	9.51	ON	429.21	16.66	16.66	ON	430.55	1.1	
423.422	428.422	5			10.97	ON		2.74	19.2	ON			
406.705	411.205	4.5		3.4	3.46	ON		5.7	5.7	ON		0.22	
429.445	433.695	4.25			2.9	OZ :		0	4.87	ON			
427.77	432.02	4.25	428.19		2.86	ON N	428.32	0	4.77	ON ON	428.44	0	
309 875	390 965	0 0	399 95		0 17		300		0 26 0		300		
0	0	0	0		0	ON ON		0	0	ON			
439.853	439.853	0	439.97		5.6	Yes	440.0	0	10	YES	440.0	0	
401.708	401.708	0	402.49		0.17	Yes	402.5	0	0.26	YES	402.5		
395.871	395.871	0	396.35	0	5.17	Yes	396.37	0	8.53	YES		0	
396.816	396.816	0	397.05		5.23	Yes	(17	8.61	8.61	YES			
404.367	404.367	0	404.4		0.18	Yes		0.27	0.27	YES			
400.667	401.923	4.5	400.71	2.23	5.23	NO NO	400.72	3.85	5.83	ON C	400.74	0.181	
403.025	407.695	4.67	403.57	1	6.47	ON		1.93	10.64	ON			
387.769	392.439	4.67	388.65	1.8	8.16	NO	388.96	2.96	13.43	NO	389.5	0.146	
432.733	435.733	3		` '	1.17	ON		1.83	1.83	ON			
404.7	411.909	7.209		0.	51.9	ON		0.98	63.1	ON		0.052	
377.086	380.221	3.135	377.38		15.27	ON N	377.51	0 [29.44	ON 2		0	
407.174	411.0/4	C.4	407.38	7 20	0.94			1.5.1 1.5.7	7C.T		707.32		
403.174	0	0	0.004		02.41	ON ON		17.21	02:22	ON ON		400.0 C	
392.013	397.013	5	392.4	1:3	1.31	ON	392	2.14	2.14	ON	392.6	0.10	
387.39	387.39	0	387.78		1.24	Yes	(1)	0	2.29	YES			
439	447.55	8.55	440.45	7.24	9:59	NO	443.89	12.56	16.38	ON	446.78	0.835	
440	448.482	8.482	440.43		2.35	ON	443.9	3.95	3.95	ON	447.81	0.195	
457	466.873	9.873	459.2	3.8	104.15	No	465.22	6.42	160.08	ON	467.	0.37	
0	402 105	0	0 000		0 0	ON Z	0 000	0	0 2 25	ON Z	0 000		
398.605	403.105	v. 4	399.05	70.7	2.02	NO SHA	399.18	3.35	12 92	NO	399.35	0.208	
415.002	415.325	0	415.04	1	2.27	NO	415.05	2.93	3.57	NO		0.12	

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				Propo	sea cc	Proposed Condition Junction	ONS RE	Salts 3	umm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
				Max.	Max.		Max.	Max.	Max.				
Invert	Rim	Donth	Max.	Lateral	lotal	Surrharaina	HGL	Lateral	lotal	Surcharaina	Max. HGL	Max. Lateral	Max
evation (feet)	Elevation (feet)	(feet)	(2-year)	(2-	(2-	(2-year)	(10- vear)	(10-	(10-	(10-year)	(100-year) (feet)	Inflow (100-vear) (cfs)	1r (100-v
(1001)	(1551)		(feet)	year)	year)		(feet)	year)	year)		(122)	(513) (153) (504)	001
487.091	492.591	5.5	487.32	1.19	1.5	NO	487.4		2.66	ON		0.096	
503.89	506.89	3	503.89		0	No	503.89	0	0	ON	503.89		
392.33	395.33	æ			5.05	ON		0	7.95	ON		0	
407	410.832	3.832		5.1	5.12	ON Z		8.07	8.07	ON		0.375	
409.773	409.773	O (M	409.77	0	0	NO	409.77	0	0	ON	409.77	0	
426.025	429.025	· K	426.05		2.21	ON No		0	3.82	ON			
408.179	411.179	3	408.18		0	No	408.18	0	0	ON			
421.791	426.291	4.5	422.17		1.44	ON :	422.29	1.6	2.48	ON	7		
428.617	433.117	4.5	428.73	0.51	0.51	ON ON	428.77	0.88	0.88	ON ON	428.8	0.039	
404.310	407.310	n m	404.3	2.0	2.01		404.33	1.28	1.28	ON C		90.0	
451.575	456.575	2	451.75		2.39	ON N	451.8	0.91	4.34	ON			
456.446	461.446	5	456.73	1.87	1.87	No	456.83	3.44	3.44	ON	456.94	0.187	
399	400.5				15.62	ON NO		0	26.7	YES			
419.641	424.141	4.5		0.5	0.51	No		0.8	0.8	ON		0.03	
357.827	357.827	0			23.2	Yes	358.26	0	7				
428.125	431.625	3.5	7		0.86			1.38					
428.177	431.077	3.5	4.65.4	 	6.0 C	ON C	0 479.40	1.44 0	1.44 O	ON CX	428.53	0.0	
477	482.094	5.094	477.	0.	0.54	NO	477.	0.54	0.83	ON	477.2	0.023	
477.527	482.027	4.5	477.65	0.19	0.19	No	477.68	0.29	0.29	ON	477.71	0.012	
463.593	467.093	3.5	463.88	1.03	1.03	ON		1.6	1.6	ON	464.05	0.071	
463.371	466.871	3.5			1.28	No		2	2	ON	7		
474.541	478.041	3.5	474.89	1.57	1.57	ON Z		2.56	2.56	ON		0.121	
435.393	445.347	j T			4.8	ON S	435.83	0.16		ON CA	435.94		
284.149	284.96	0	286.83		469.24	Yes	287.05	0	542.84	YES			
436.204	440.704	4.5	436.68	0.41	3.52	No	436.81	0.67	5.61	ON	436.98	0.034	
437.662	441.662	4	437.83		99.0	ON No		1.05	1.05	ON			
436.434	440.934	4.5	436.99		2.46	ON :	7	3.91	3.91	ON			
398.07	401.57	3.5	398.86	1 07	7.17	ON N	399.4	9.23	13.89		401.28	0.556	
363.766	373 786	786			9.12		368 89	3.03	19 24				
382.69	382.763	0.2500			0.00	ON CN	382.69	0.5	0	ON ON		0.0	
394.661	400.271		394.67	0.4	0.41	ON		1.09	1.09	ON		0.05	
399.676	402.676		400.02		1.51	N		0.24	2.84	ON			
414.174	414.415	0	414.21	0	1.34	No	414.23	0	2.69	ON	414.25	0	
271.9	274.05	2.15	273.7	0	25.85	ON	274.39	0	199.81	YES	275.16		
419.295	419.451	0	419.3		0	NO	419.3	0	0	ON			
445.039	448.039		445.04		0	ON ;	445.04	0	0	ON	7		
461.001	461.001	0	461.24	2.03	2.03	Yes	461.32	3.61	3.61	YES	461.4	0.181	
414.249	417.249	n m	414.25		00.1	ON ON	414.25	0	0 0	ON			

					-		(
				Propo	sed Co	Proposed Condition Junctic	ons Re	sults S	nmm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
				Max.	Мах.		Z	Max.	Max.				
Invert	Rim :	Depth	Max. HGL	Lateral Inflow	Total Inflow	Surcharging	HGL	Lateral Inflow	Total Inflow	Surcharging	Max. HGL	Max. Lateral	Ma
evation (feet)	Elevation (feet)	(feet)	(2-year) (feet)	(2- year)	(2- year)	(2-year)	(10- year) (feet)	(10- year)	(10- year)	(10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	(100-)
392.392	392.392	0	392.44	(CTS)	(CTS)	Yes	392.46	(CTS)	(CTS) 3.38	YES	392.49	0	
317.992	322.492	4.5		3.2	3.23	ON	318.81	5.83	5.83			0.37	
271.632	271.852				466.33	Yes	274.36	0	894.77				
316.715	324.715				5.5	No	317.53	4.06	9.84	ON			10
312.366	317.366	5			3.89	ON N	312.83	7.17	7.17	ON S	312.97	0.355	10
305 000	513.903	0.0	309.02		10.90		303.22	117	20.04			0.77	
303.308	311.323	7		0.71	26.08	ON ON	305.58	1.14 0.4	49.68	ON ON			
306.598	311.098	4.5			0.65	ON	306.8	1.15	1.15		(1)		10
0	0	0	0	0	0	No	0	0	0	ON	0	0	
312.789	312.789	0			1.18	Yes	313.44	2.16	2.16				10
306.501	311.501	20 1			2.65	ON Z	307.68	4.1	4.1	ON			10
369.199	373.699	C. 4	369.82	5.18	5.18 4.51	NO	370.09	8.05	9.51	VES	370.65	0.588	2
382.15	386.65	4.5			11.18	ON	383.28	20.03	20.03	ON			
381.595	386.095	4.5			3.17	ON	382.88	5.1	8.25				
422	424.458	2.458	422.72	5.31	6.3	NO	422.96	9.28	11.35	NO	423.27	0.562	6:
400.34	403.34	3		2.79	3.13	Yes		4.81	5.59	YES		0.274	
403.582	403.582	0			5.91	Yes		9.79	9.79				~
387.699	392.199	4.5			4.19	ON :	388.19	7.66	8.5	ON			~
384.087	392.087	∞ п	385.95	9.42	94.54	ON ON	386.6	16.22	161.33	ON ON	387.62	1.23	~
309.034	706 916	0 1			78.72			11 92	121 88	ON ON			1
365.901	366.056	\ O			0 0	ON ON		0	00.151	ON CO			
403.591	409.591	9	7	11.9	72.09	ON	405.97	21.11	120.79	ON	7	1.3	10
412.155	419.155	7		2	59.15	ON	414.17	4.8	97.54	ON			8
410.751	417.751	7	412.07		61.52	ON	412.48	4.91	101.79	ON	41.	0.318	~
428.97	432.97	4	429.4	3.7	3.75	No	429.66	6.72	6.72	ON	43	0.37	
716 917	0 0 21/	0	0 418 7E	0 27.5	0 2 2	ON No.	77 017	0 0	0 6 5 7	NO	0 0 010	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
372.202	378.202	9			10.63	ON	372.82	9.78	19.25	ON			2 00
374.636	379.136	4.5			5.4	No		4.53	10.37	ON			_
351.326	357.326	9	352.22	13.7	25.17	ON	352.55	23.44	44.5	ON	353.15	1.79	
378.866	383.366	4.5	379.33	2.78	2.78	ON	379.48	4.76	4.76	ON	379.69	0.21	
412.747	417.747	5			15.35	ON	414.08	0	27.4	NO			
294.138	294.138	0			425.2	Yes	299.11	0	599.59	YES			
346.543	351.043	4.5	347.18		5.65	ON N	347.42	5.04	9.76	ON Z			
254 506	414.043	4 "	410.33	5.04	5.54		41U.41	11 30	2.0		410.32	0.401	
369 959	375 959	4.5			19.37		371.58	13.9	37.50	ON ON			
0	0	0			0		0	0	0	ON		0	
375.7	376.7	1	375		0	NO	375.7	0	0	NO			
432.412	435.412	3	432.52	0.3	0.32	No	432.54	0.51	0.51	ON		0.02	61
421.326	421.653	0	421.34	0	0.17	No	421.35	0	0.27	NO	421.35	0	0

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				Propo	sed Co	Proposed Condition Junctic	ons Re	salts S	nmm	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
			200	Max.	Max.		Max.	Max.	Max.				
Invert evation	Rim Elevation	Depth (feet)	Max. HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	HGL (10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	Max. HGL (100-year)	Max. Lateral Inflow	May
(reet)	(reet)		(feet)	year)	year)		year) (feet)	year) (cfs)	year)	•	(teet)	(100-year) (cfs)	(100-)
357.604	362.104	4.5	357.95		1.38	NO	358.07	2.5	2.5	ON	358.21	0.121	
350.929	350.929	0	(,,		1.34	Yes	351.07	0	2.45				
342.593	347.593	5 5	343.8		8.82	ON Z	344.44	15.37	16.19	ON Z			
383.778	385.14	3	385.93	0.22	14.66	NO	385.93	13.33	26.06	ON	385.94	0.018	
379.692	382.692	3	379.79		0.11	ON	379.82	0.2	0.2	ON			
377.031	380.031	3	377.84	0.75	0.86	No	378.54	1.6	1.79	ON		0.092	
403.981	403.981	0 .			0.26	Yes	404.12	0 (0.46		7		
306.046	41I.U63	v.4	406.76	0.27	570 34	NO SAY	406.83	0.47	839 16	NO	314 71	0.019	
442.346	445.346	o m	442.68		6.00	ON	442.79	5.43	5.43			0.32	
417.134	420.134	က	417.24	0.1	0.18	No	417.27	0.31	0.31	ON			
436.584	439.584		436.65	0.1	0.1	N	436.67	0.16	0.16	ON	436.68	0.006	
411.917	418.498	3	411.92		0.28	No	411.93	0	0.47	ON			
423.965	429.465	5.5			10.87	ON :	424.95	8.9	19.38	ON			
457	458.054	1.054			0.1	ON	457.1	0.16	0.16	ON	7		
453.778	457.699	3.5		0.2	0.27	ON S	453.8	0.35	0.45	NO		0.01	
452.392	452.592	0	452.5I	0	0.07	Tes	10.264		0.44	YES	452.02		
421.298	425.798	4.5	421.61	1.2	1.29	ON	421.71	2.34	2.34	ON		0.1	
337.321	337.321	0	337.56		0.35	Yes	337.63	0.55	0.55	YES		0	
416.801	416.855	0	416.86	0	1.28	Yes	416.89	0	2.32	YES	416.92	0	
403.919	403.919	0	404.29		2.29	Yes	404.31	0	3.87	YES			
439.355	439.355		439.82		1.38	Yes	440.07	2.58	2.58	YES			
448.232	451.232	2000	448.39	0.72	0.72	ON ON	448.44	1.25	1.25 1.55		448.49	0.056	
404.499	404.499	0			0.83	Yes	404.64	0	1.51	YES			
421.723	424.723	3	421.77	0.0	0.08	No	421.78	0.12	0.12	ON		0.00	
401.157	401.157	0			0.54	Yes	401.37	0.63	1.08				
408.234	408.234	0	408.35	0.2	0.24	Yes	408.4	0.46	0.46			0.02	
377.262	377.262	0 0	377.29		0.53	Yes	377.3	0	1.06				
322.549	328.027	4.027	322.7	0	0 .4	ON N	12.525		0.19		324.3		
459.715	459.715	0	459.71		0	OZ Z	459.71	0	0	ON	45		
458.209	458.407	0	458.21		0	No	458.21	0	0	ON			
465.837	466.298		465.84		0	ON	465.84	0	0	ON		0	
420.677	425.177	4	420.87	0.27	1.18	No	421.02	0.46	4.02	ON	422.3	0.02	
416.881	424.881	∞	418.53		39.43	ON	419.17	0.78	69.7	ON			
415.701	427.701	12	417.45	` '	54.1	ON	418.09	26.91	91.21	ON			
415	427.361	12.361	416.67		55.15	No	417.3	2.03	92.44	ON			
413.6	420.6	7	415.48		56.9	ON Z	416.18	3.31	94.5	ON		0	
217 120	429.948	4 0	427.08	17.63	17.63	ON 30X	430.09	31.21	17.18	YES	430.25	3.47	
420.074	425.324	5.25		1.7	3.16	ON	420.55	3.08	6.03			0.17	

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				Propo	sed Co	Proposed Condition Junction	ons Re	Sults S	nmm	Junctions Results Summary Table			
imensions	SI				2-year			1	10-year				100-ye
				Max.	Мах.		No.	Max.	Мах.				
Invert	Rim	:	Max.	Lateral	Total		HGL	Lateral	Total		Max. HGL	Max. Lateral	Ma
evation	Elevation	Depth (feet)	HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	(10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	(100-year)	Inflow	Ir (100)
(near)	(leer)		(feet)	year)	year)		year) (feet)	year)	year)		(leer)	(TOO-Year) (CIS)	(-00T)
434.401	434.401	0	434.81		0.03	Yes	434.83	0	0.05	YES	434.85	0	
437.078	437.458	0				Yes		8.95	9.64	YES		0.54	
437.244	437.244	0			2.4	Yes		4.16	4.16	YES			
440.5	443.025	2.525			2.59	ON		0.45	4.62	ON			
441.912	446.412	6.4	442.44	6.55	11.37		442.62	0.76	4.2	YES	442.88	0.033	
404.183	406.01	0			0	ON	7	0	0	ON			
436.995	440.495			10.8	10.89	No		19.29	19.29	ON		1.9	
479.458	482.128	2.6	479.46		0	ON		0	0	ON			
478.195	482.195	4 0	4/8./4	3.4	3./1	NO	479.02	6.11	6.82	ON	482.27	0.384	
491.857	491.857	0	492.02	0.5		Yes		о н	0.79	YES		0.04	
430.381	433.881	3.5	431.16			ON		0	10.43	YES			
435.311	438.641	3.33	438.71	0		Yes		0	7.7	YES			
448.005	448.005		448.1			Yes		1.71	18.03	YES			
449.534	449.927	0	449.86	15.4	15.51	No		77.72	77.72	YES		2.6	
424.212	424.212	0	424.21		0	ON		0	0	ON			
408.446	408.446	0	408.45		0 10	Yes		0 20	0 6	YES			
407.032	411.032	4.59	408.32	3.53	23.32	ON ON	410.31	6.41	38.19	ON ON	411.51	2.04	
405.8	411.162	5.362	408.01		25.8	ON		4.72	55.32	ON			
405.55	411.55	9	407.91	1.14	85.36	No	409.24	2.02	154.02	ON	411.37	0.109	
407.387	413.387	9	409.88	3.07	40.47	No	413.87	5.36	65.72	YES			
397.156	403.656	6.5	399.79		93.55	No		8.07	168.78	ON	1		
396.863	403.863	7	399.55		98.68	ON A		0.43	180.35	ON Z			
424.217	430.217	0 9	424.9	0.22	4 77	N N	425.15 475.58	0.33	22.45	ON C	423.40	0.016	
411.435	414.935	3.5	414.13		0	. N		0	0	ON			
344.859	344.892	0	345.69	0	66.47	Yes	346.03	0	103.79	YES	346.46	0	
418.362	424.362	9	420.01		27.03	No		13.14	49.45	ON			
418.22	424.22		419.21		27.85	ON		1.59	55.6	ON	7	0	
430.026	436.026	9 1	430.86	9.17	13.81	ON	431.11	16.37	22.79	ON	431.5	1.38	
420.332	434.032	J. J.	429.34		13.15			23.59	73.59			1 96	
440.024	443.024	e co	442.17		0.29	ON ON		0.44	0.44	ON		0	
439.703	439.703	0	439.82		0.22	Yes		0.35	0.35	YES			
437.637	437.637	0	437.68		0.24	Yes		0	0.36	YES		0	
460.531	470.031	9.5	461.58	0.16	30.04	NO	461.96	0.27	54.14	ON	462.42	0.011	
448.857	452.357	3.5	450.47	1.62	35.21	No	451.07	3	62.56	ON	452.44	0.186	
385.539	387.235	0	385.58		2.85	No		0	4.81	ON			
449.3	453.3	4	450.51		5.86	No		10.5	10.5	ON			
464.836	469.336	4.5	465.78		28.19	ON Z		0.27	49.61	ON 2	466.95		
461.021	465.321	C.4	462.8	11 21	28.30	ON ON	403.33	00.32	19.67			0.014	
400:00+	47.00.307	5	CT: /0+	I	20.00			50:03	47.70	ON THE REAL PROPERTY.			

Proposed Condition Junctions Results Summary Table

				Propo	sea co	Proposed Condition Junctions Results Summary	ons Ke	saurs 3	TIED I	ary lable			
imensions	SI				2-year			1	10-year				100-ye
Invert evation (feet)	Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year) (cfs)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	May Ir (100-)
486.593	486.593	0	486.59	0	0	OZ	486.59	ı	0	ON	486.66	0	
501.847	506.347	4.5		2.1	2.17	No	502.31	3.8	3.88	ON	502.46	0.22	
0	0	0		0	0	No	0	0	0	ON			
0	0	0		0	0	NO	0	0	0	ON			
373.308	373.308	0 !		0	1.97	Yes	373.7	0	3.28	YES			
493.811	498.311 493 173	4.5	494.63	1.59	9.56	02 2	495.03	3.17	15.84	OZ CZ	498.69	0.184	
484.251	488.751	4.5		3.73	13.01		485.67	6.75	22.49				
473.845	478.345				17.71	ON NO	475.04	4.1	30.9				
0	0				0	ON	0	0	0	ON			
434.677	436.677	2	434.68	0	0	No	434.68	0	0	ON	434.68		
0	0	0			0	ON	0		0	ON			
509.211	512.211	C I			0.13	ON :	509.3		0.23	ON :			
415.315	420.315	ر 1047			6.42	0 2	415.96		11.3/	ON ON	7		
407.02	411.667	4.047 O	408.31	1.40 O	12.87	ON CN	408.53	2.23	0	OZ CZ	408.8	0.092	
411.2	415.402	4.202	411.6	4.8	4.94	0 2	411.81	8.12	8.42	ON	412.1	0.55	
399.39	403.352	3.962	400.6	8.67	58.92	OZ	401.12	14.35	100.06	ON	403.57	0.863	
401.63	405.352	3.722	7	2.49	15.39	No	402.39	4.18	26.75	ON	403.29	0.211	
396.45	401.54	5.09			75.2	No	399.39	15.35	129.39	ON			
393.384	399.884	6.5			224.27	ON.	398.29	0.65	335.2	ON			
392.191	398.691	6.5			258	ON Z	397.98	4.73	339.19	ON 2			
392	402.342	10.342	396.56	0.51	255.09	02 2	397.66	0.81	338.66	OZ Z	398.04	0.04 0.04	
442.511	447.011	4.5			3.12	ON NO	442.96		5.19	ON			
442.608	447.108	4.5		0.63	0.63	No	443.03	1.06	1.06	ON		0.043	
0	0	0		0		No	0		0	ON			
440.846	445.346	4.5		0.28		OZ	441.15		5.67	ON S			
397.02	399 763	6.0	434.84	ر 73 /	138 61	02	436.13	8.31	102.1		436.98	0.388	
397.528	401.028			5.61	5.73	0 2	399.68		9:26				
411.5	418.354	.9		16.22	33.73	ON	413.42	2	56.4				
410.5	418.136	7.636	412.06	4.06	45.25	No	412.77	99'9	77.66	ON	7	0.351	
421.226	425.726		,		0.02	No	421.97	0		ON			
426.976	431.476	4		0.3	6.44	ON NO	428.11	0.5	10.7	ON		0.02	
440.164	440.164	0	440.1	0	0	ON Z	440.16		0	ON Z	440.1	0	
	0	0 0		0	0 0	ON Z	0		0 0				
0	0	0	0	0	0 0	ON Z	0	0	0	OZ Z			
438.335	438.335	0	438.3		0 0		438.33		0		438.3		
431.235	443.493	3.67		0.8	0.81	No	434.92	1.2	1.29	ON		0.05	
450.532	450.532	0		0	0	No	450.53		0	ON			
0	0	0	0	0	0	No	0	0	0	ON	0	0	
0	0	0			0	No	0	0	0	NO			

				Propo	sed Co	Proposed Condition Junctic	ons Re	sallts S	nmme	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
				Max.	Max.		No.	Max.	Max.				
Invert	Rim	:	Max.	Lateral	Total		HGL	Lateral	Total		Max. HGL	Max. Lateral	Ma
evation (feet)	Elevation (feet)	Depth (feet)	HGL (2-year)	Inflow (2-	Inflow (2-	Surcharging (2-year)	(10-	Inflow (10-	Inflow (10-	Surcharging (10-year)	(100-year)	Inflow (100-year) (cfs)	Ir (100-)
(leer)	(leer)		(feet)	year) (cfs)	year)		(feet)	year)	year)		(leer)	(100-year) (113)	
469.653	469.653	0	469.65		0	No	469.65	0	0	ON	469.65	0	
413.253	419.159				98.9	No	415.8	9.93	11.57	ON			
464.829	469.329				15.77	ON	465.96	28.34	28.34	ON			
437.454	441.954	4.5	437.96	9.69	9.99	ON Z	438.13	16.95	17.58	ON Z	438.37	1.08	
439.602	444.602	5			12.63	ON N	442.08	0.92	21.78	ON		0.039	
444.673	448.673	4	444.88		0.74	No	444.94	1.2	1.2	ON		0.065	
444	449.117	5.117			3.03	No	444.88	0.56	4.97	ON	7		
444.271	448.771	4.5			2.69	ON	445.19	4.44	4.44	ON			
442.117	446.617	4.5	442.58	0.05	3.05	ON S	442.74	0.0	5.03	OZ Z	445.44	0.003	
445.077	449.077	4 r.			16.91	ON ON	447.15	1.1	32.27				
434.447	434.447	0	,		1.36	Yes	434.54	0	2.33	YES			
454.769	459.769	5	455.76	7.3	16.05	No	456.35	12.62	30.7	ON		0.80	
456.383	461.383		457	0.13	9.33	No	457.32	0.19	18.92	ON	460.61	0.008	
437.936	441.606	3.67	441.81	.,	22.8	Yes	441.81	20.39	22.8	YES	7		
436.406	440.906	4.5	439.64		0.17	ON	439.97	0.26	0.26	ON			
437	440.918	3.918			38.59	ON	440.09	16.61	69.29	ON			
429.206	434.706	5.5	429.34	11.06	11.06	ON Z	431.09	1.14	9.52	OZ Z	431.12	0.05	
425.87	434.373	8.503	7		61.45	ON ON	431.5	14.47	166.88	ON		0.973	
425.5	434.527	9.027			79.41	No	430.45	12.71	214.85	ON	7		
433.344	437.344	4	435.75	1	11.84	No	437.36	20.35	20.35	YES		1.97	
387.049	387.809	0.76	387.86	0	8.04	Yes	388.12	0	13.26	YES	388.47	0	
432.747	436.747	4	435.7	4.4	36.16	No	437.16	7.58	75.85	YES		0.59	
448.232	450.062	1.83	448.23		0	ON No	448.23	0	0	ON		0 0	
447.610	500 373	ט כ	447.62	1 02	1 02	NO	447.02 107.58	7 6 7	1 67	CN CN	79.7 67	0 083	
0	0	0	0		0	ON ON	0	0	0	ON		0	
0	0	0	0		0	No	0	0	0	ON		0	
451.96	452.96		453.02	6.14	6.14	Yes	453.1	10.77	10.77	YES	453.19	0.824	
430.296	434.796	4.5	430.51		0.73	No	430.6	0.98	1.42	ON			
433.591	438.091	4.5	434.13		4.07	No	434.31	6.85	6.85	ON		0	
428.569	431.569	က	429.31	7.5	7.52	ON ;	429.63	13	13	ON		1.04	
404.1/9	404.179	ο,	404.79		58.08	Yes	404.88	0	73.96	YES			
433.62	437.62	4 r	433.74		0.7	ON NO	433.8	0.46	0.46	OZ Z			
427.256	429.756	1 049	428.4	0.89	13.25	NO	478.74	1.58 0 31	7.2 96	NO	429.18	0.093	
414.454	418.454	4		Ì	16.95		415.95	29.79	29.79	CN			
397.703	400.203	2.5			28.15	Yes	401.16	4.92	42.92	YES		0	
394.557	401.557	7			113.94	No	398.95	4	206.38	ON		0.258	
393.891	401.391	7.5	396.1		117.96	N	398.41	9.61	213.68	ON			
437.133	441.633	4.5	437.68		2.06	No	437.86	3.58	3.58	ON			
436.654	440.904	4.25	437.07	2.23	4.25	No	437.21	3.88	7.4	NO	437.38	0.209	

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				Fropo	sea CC	Proposed Condition Junctic	ONS RE	Salits 5	mum	Junctions Results Summary Table			
imensions	S				2-year			1	10-year				100-ye
Invert evation (feet)	Rim Elevation (feet)	Depth (feet)	Max. HGL (2-year) (feet)	Max. Lateral Inflow (2- year) (cfs)	Max. Total Inflow (2- year) (cfs)	Surcharging (2-year)	Max. HGL (10- year) (feet)	Max. Lateral Inflow (10- year) (cfs)	Max. Total Inflow (10- year) (cfs)	Surcharging (10-year)	Max. HGL (100-year) (feet)	Max. Lateral Inflow (100-year) (cfs)	Max Ir (100-)
389.992	398.992	6	391.96	1.8	1.82	ON	m	2.93	13.83	ON		0.157	
389.5	398.261	8.761	394.49		152.71	ON R		0 5	267.66	ON Z			
393.458	398.958	ر.ر 7.7	393.77	3.06	1.51	ON ON	393.99	5.31	3.11	OZ CZ	397.78	0.443	
390.146	394.646				8	ON		17	14.18	ON		0.95	
387.21	394.71	7.5	389.82	0.41	162.8	No	393.26	0.64	286.33	ON		0.028	
384.5	390.957	6.457				No		1.2	311.2	ON		0.063	
387.103	391.603	4.5		15.8		ON W		28.28	30.73	YES		2.68	
394	396.967	7.24	395.27	4.31	45.56	ON ON	397.86	7.23	71.27	YES	399.02	0.403	
390.415	396.915				152.21	ON No			274.42	YES		0.321	
398.776	403.776		400.31		40.17	No		15.58	66.17	ON		0.797	
395.816	399.816		397.66		41.81	No		3.17	66.15	ON		0.149	
412.26	417.26	5	413.51		4.47	ON		7.14	7.14	ON		0.355	
440.437	440.437		440.9	3.00	3.00	Yes	441.05	9.77	9.77	YES	441.31	0.732	
431.118	436.618				19.84	CZ			32.38	ON		0.062	
430.498	436.498				21.09	ON			34.31	ON	,	0.132	
431.753	436.253	4	432.56		19.3	No		1	31.54	ON		0.829	
0	0	0	0	0	0	No	0	0	0	ON	0	0	
465.037	465.525	0	465.04			No			0	ON			
419.201	424.201	5	420.32	7.1	27.9	No	420.7	12.3	45.89	ON	422.8	0.95	
0 0	0	0	0 0	0	0 0	ON A	0 777	0	0	ON S			
451.132	451.132	0 7	451.13	0.22	14.61			0.37	24.94	OZ OZ	451.13	0.016	
445.493	449.493	4	445.96			ON		7.32	7.32	ON		0.464	
447.618	452.118	4.5	447.95	1.42	1.42	No	448.06	2.52	2.52	ON	448.18	0.127	
442.611	445.611	3	443.61		9.5	No		14.04	16.5	ON	7	1.18	
448.672	448.672	0 1			1.23	Yes		2.13	2.13	YES		0.098	
436.799	440.299	3.5	440.93	2.91	9.54	Yes	441.01	5.23	17.71	YES	441.1	0.317	
395.898	395.898	n	395.92		2.01	Nex Yes			3.34	YFS		044:0	
422.292	426.292	4	422.64	1.8	1.87	ON		3.3	3.36	ON		0.192	
398.03	403.53	5.5	404.5	1	7	Yes	405.09	30.67	65.42	YES	405.37	2.19	
397.69	403.69	9	404.48	0.18	49.88	Yes	404.99	0.28	65.42	YES	405.34	0.012	
415.29	420.79			(1)	21.73	ON		6.24	38.67	ON			
437.586	442.086	4.5				No	4	10.6	10.6	ON :		0.608	
436.72	441.72				ZI	ON Z			32.98	ON C		0.0/3	
440.396	444.896	4.5	440.79		2.6	ON	441.06	4.5/	4.57	ON S		0.227	
439.3 AAF 06A	0.444 0.70 050	U L	440.33	0.21	0.68				17.31	ON CA	441.42	0.016	
446.5	450.799	4.299			3.21	ON			5.78	ON		0.394	
401.528	401.528	0			8.44	Yes		1	14.12	YES		0.76	
454.786	458.286	3.5	455.81	0.73	2.21	No	456.52	1.27	3.87	NO	457.89	0.068	

	100	l (1)	0.493	0.438	0	0.398	0	0 0	0.02	0.14	0.285	0.05	0.387	0.813	0.03	0.205	0.085	0 7	0.271	0	0.244	0.85	0.015	0.033	0 455	0.19	0.035	1.53	1.73	0.149	0.23	0	0.393	0 !	0.516	0.161	0.04	0.32	0.464	0.572	0.000
		Max. Lateral Inflow (100-year) (cfs)	0								0																														
		Max. HGL (100-year) (feet)	454.45	439.64	0	444.41	438.02	495.85	455.12	461.35	451.06	450.98	449.81	449.9	449.39	445.98	448.61	500.66	747.42	432.41	416.68	459.9	450.34	464.65	460.52	468.81	445.9	435.13	435.69	429.47	431.77	433.27	410.52	433.52	372.76	393.17	391.67	392.08	343.21	358.23	404.63
ry Table		Surcharging (10-year)	YES	O C	OZ	YES	YES	YES	YES	YES	ON	YES	YES	YES	YES	ON !	YES	YES	VES	ON	ON	YES	YES	YES	CN	YES	ON	ON	ON	ON	ON	ON	ON	YES	ON	ON :	ON	ON :	ON Z	OZ Z	0 0
umma	10-year	Max. Total Inflow (10- year) (cfs)	13	6.73	0	8.01	6.71	0.56	0.40	2.86	4.95	0.99	66.6	12.54	9.82	24.07	12.32	14.56	4.03	0	4.81	10.74	0.36	0.74	20.02	120.14	0.82	33.36	18.37	2.83	37.29	0	68.19	0	39.25	2.84	0.92	31.43	60.29	52.96	0.19
sults S	1		7.23	6.73	0	7.91	0	0 46	0	2.86	4.83	0.99	6.55	12.54	0.63	2.91	1.67	0 0	4.09	0	4.81	10.74	0.36	0.74	0 8 28	3.88	0.82	14.7	17.56	2.83	4.24	0	7.21	0	7.18	2.84	0.92	6.16	8.01	11.29	0.19
ons Re		Max. HGL (10- year) (feet)	454.39	439.58	0	443.57	437.96	495.71	455.11	461.32	450.94	450.93	449.73	449.83	449.38	445.73	448.6	495./I	447.24	432.41	416.63	459.87	450.32	464.63	400.52	468.36	445.86	430.79	431.44	429.32	428.18	433.27	408.81	433.52	371.91	393.06	391.67	391.79	342.35	357.85	404.61
Proposed Condition Junctions Results Summary Table		Surcharging (2-year)	Yes	ON S	ON	Yes	Yes	Yes	Yes	Yes	No	ON	Yes	Yes	Yes	ON :	Yes	Yes	ON	ON	ON	Yes	Yes	Yes	CAN CAN		N _O	No	ON	ON	ON	No	No	Yes	ON 2	ON :	ON :	ON :	ON	ON ON	ON ON
sed Co	2-year	Max. Total Inflow (2- year) (cfs)	6.62	3.71	0	4.36	3.48	0.32	0.20	1.52	3.28	0.58	7.82	7.09	7.91	10.29	7.44	I./8	2.37	0	2.85	5.95	0.22	0.4	0.01	36,31	0.49	18.54	10.34	1.58	20.97	0	37.07	0	21.32	1.59	0.61	17.35	33.32	28.96	0.12
Propo		Max. Lateral Inflow (2- year) (cfs)	4.02	3.71	0	4.32	0	0 00 0	0.20	1.52	2.72	0.58	3.71	7.09	0.38	1.67	0.94	0 10	7.37	0	2.85	5.95	0.22	0.4	U 4 89	2.42	0.49	8.25	98.6	1.58	2.48	0	3.99	0	4	1.59	0.61	3.38	4.79	6.25	0.12
		Max. HGL (2-year) (feet)	454.33	439.48	0	443.03	437.91	495.63	455.1	461.3	450.07	450.08	449.6	449.77	449.36	445.27	448.43	491.57	447.07	432.41	416.59	459.84	450.3	464.62	460.32	464.04	445.83	430.38	430.94	429.2	427.64	433.27	407.85	433.52	371.32	392.98	391.66	391.55	341.87	357.56	404.59
		Depth (feet)	3	2.5	0	0	0	0	0	0	2.872	2.501	3.5	m ·	4	3.823	0	0 1	0.0	3.5	c	0	0	0	ט גי	5.5	4.25	5	5	4	2	0	7.139	0	8.5	4.5	0	9 .	4.5	7. C	J. 4
	S	Rim Elevation (feet)	454.253	439.824	0	442.035	437.61	495.41	454.901	461.249	451.022	450.801	448.928	449.507	449.043	448.323	447.601	491.421	450.128	435.906	419.473	457.826	450.207	464.582	400.440	468.354	449.976	434.445	434.883	432.871	431.5	433.27	413.699	433.517	378.526	397.215	393.886	396.88	345.191	362.275	408.524
	imensions		451.253	437.324	0	442.035	437.61	495.41	454.901	461.249	448.15	448.3	445.428	446.507	445.043	444.5	446.74	491.421	446.628	432.406	416.473	457.826	450.207	464.582	460.446	462.854	445.726	429.445	429.883	428.871	426.5	433.27	406.56	433.517	370.026	392.715	391.65	390.88	340.691	356.775	404.524

100-ye

May Ir (100-)

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				Propo	sed Co	Proposed Condition Junction	ons Re	salts S	nmme	Junctions Results Summary Table			
imensions	SL				2-year			1	10-year				100-ye
Invert	Rim	:	Max.	Max. Lateral	Max. Total		Max. HGL		Max. Total	-	Max. HGL	Max. Lateral	Ma
evation (feet)	Elevation (feet)	Depth (feet)	HGL (2-year) (feet)	(2- year)	(2- year)	Surcharging (2-year)	(10- year) (feet)	(10- year)	(10- year)	Surcharging (10-year)	(100-year) (feet)	Inflow (100-year) (cfs)	lr (100-)
329.345	335.345	9	330.93			ON	331.67	0.72	50.58	OZ	335.54	0.035	
330.774	335.274	4				ON		16.01	16.46	ON	335.86		
0	0			0	0	ON		0	0	ON	0		
324.393	333.393	6.25	328.96	0.89	29.88	O Z	330.85	1.45	52.32	0 0	334.65	0.079	
324.895	333.895					ON		2.36	51.05	ON	335.46		
330.3		1.				Yes		16.21	30.49	YES	335.19		
326.975	331.475	4.	331.72	10.28	82.94	Yes	333.6	17.29	291.11	YES	335.31	0.883	
325.466	333		32	3.0	441.0	ON	33.	5.19	654.36	ON :	334.98	0.248	
399	370 882	0 0	399	0 0	0	OZ Z	370 88	0 0	0 0	ON CN	399	0	
362.899	366.899			6.2	6	OZ Z		11.14	16.54	ON ON	368.13	0.75	
363.316	367.816	4				N		5.51	5.51	ON	368.12		
418.836	418.836		419.24	2.83	2.83	Yes	419.35	4.49	4.49	YES	419.5		
376.3					۵,	No		8.79	87.7	ON	382.36		
399.731	404.231	4.5	400.03	2.55	2.55	ON	400.13	4.52	4.52	NO	400.25	0.244	
399,593	404.68	5.08						9.05	75.86	CN CN	401.89		
0	0							0	0	ON	0		
420.768	423.768		420.95	9.0	9.0	No	42	1.07	1.07	ON	421.07	0.05	
388.848	392.348	3.5	388.85	0	0	ON	388.85	0	0	ON	392.37	0	
377.131	386.131				18	No		10.97	316.72	ON	383.96		
381.03	386.03	20 1	381.25	1.19	1.19	ON Z	381.32	2.04	2.04	ON S	382.24	0.127	
374.123	376.023					N N N N N N N N N N N N N N N N N N N		00:	1 27	VES	17.72		
375.234	377.234			3.2		ON		5.5	5.5	YES	378.16	0.27	
372.628	377.128	4				ON		7.81	12.54	ON	377.55		
371.628	376.628	5		3.43	10.4	ON	375.79	5.99	18.46	ON	377.13	0.421	
359.277						Yes		4.72	7.44	YES	363.71	0.206	
393.3		1.86				ON :		2.26	2.26	ON	395.62		
392.971	395.971		393.46		3.05	ON Z	393.83	3.22	5.46	ON Z	395.3		
382.40I	385.401	. C	χ.					14.48	94.29	OZ Z	383.7	0.8/1	
376.515	432.672	2.8	429.84	0.17	49.98			0.32	94.24	ON ON	378.51	0.014	
0	0					ON		0	0	ON	0	0	
0	0					No		0	0	ON	0	0	
426.564	429.564	ε.	429.62	0.67	0.67	Yes	429.64	1.15	1.15	YES	429.67	0.056	
427.595						ON	42	0	0.02	ON	429.67	0	
427.3		2.93				No		1.18	1.18	ON	428.34		
427.093	430.093			2.5		ON		4.61	5.78	ON	428.25	0.31	
426.71	427.304	0.55	426.81			ON	426.85		5.78	NO	426.89		
438.316	438.31b 434.372	0 7 7		3.62	11.1	Yes N		1.94	13.01	SIL ON	438.87	0.034	
4423.012						ON			10.01	2	40.LC4	,,,,	

408.42

0 N

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408.08

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1.01

1.01

407.74

4.5

411.97

407.47

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				Propo	sed Co	Proposed Condition Junctic	ons Ke	Sults 5	nmm	Junctions Results Summary Table			
imensions	S				2-year			10	10-year				100-ye
				Max.	Max.		Max.	Max.	Max.				
Invert	Rim Elevation	Depth	Max. HGL	Lateral Inflow	Total Inflow	Surcharging	HGL (10-	- >	Total Inflow	Surcharging	Max. HGL (100-year)	Max. Lateral Inflow	May
(feet)	(feet)	(reet)	(2-year) (feet)	(2- year) (cfs)	(2- year) (cfs)	(2-year)	year) (feet)	(10- year) (cfs)	(10- year) (cfs)	(10-year)	(feet)	(100-year) (cfs)	(100-)
400	402.104	2.104	401.79		1.14	N _O	401.8	1.84	1.84	ON	401.81	0.087	
392.193	396.693	4.5			7.39	ON		9.14	12.25	ON	m		
389.915	394.415	4.5	390.62	8.42	9.02	ON ON	392.57	14.05	15.46	ON Z	396.7	0.838	
391.401	396.401	9.012	391.47			ON		0.25	0.25	ON			
391.814	396.814	5	391.96			NO		1.05	1.6	ON			
375.706	385.206	9.5	(II)		m	No		3.83	595.89	NO			
377.7	395.716	18.016	381.2	9.64	163.9	ON Z	382.35	16.3	266	ON	384.62	1.05	
384.852	390.852		385.32		48.34	ON ON	385.3	0.63	86.39	ON ON	385.4	0.02	
0	0		0		0	ON		0	0	ON			
380.165	384.165	4			1.24	NO		1.24	1.24	ON			
374.5	379.668	5.168	(1)		27.92	No		6.4	39.35	ON			
375	378.011	3.011	377.6			ON Z		1.99	11.68	YES	379.31		
374.808	377.358	7 052	377 52	10.42	18.46	NO NO	378 57	17.1	T.05	YES YES		0.043	
772 272	579.41	4.930	,		C	ON X		1./1	60.50	NO			
371.507	380.507	0	373.22			ON		5.37	106.53	NO	(1)		
358.75	367.496	8.746			153.55	N		4.89	270.82	ON			
361.887	369.887	∞			106.38	ON		9.33	155.11	ON			
363.095	363.095	0	363.78		3.18	Yes		0	5.22	YES			
416.707	421.707	2	417.58		15.22	ON		0	27.74	ON			
351.038	356.038	5	351.43	0.4	3.48	ON :		0.64	6.01	ON			
346.053	352.053	9 1	349.57	2.96	12.71	ON N		4.87	23.34	ON			
347.115	352.115	4 189	349.58	2.88	8.08	ON CN	350.46	13.87	37.7	ON CX	352.55	1 02	
366.766	372.266	5.5			.,	ON		4.47	49.27	ON			
352.16	359.345	7.				No		7.11	112.85	ON			
351.67	359.394	7.72			105.74	ON		3.98	163.98	ON			
369.755	375.755				26.5	ON N	m	2.95	44.68	ON	(1)		
358 056	371.112	4.012	3507.04	3.2	2.2	ON ON	359 31	5.25	37 97	ON CN	350.74	0.273	
420.284	425.284	5	421.17			No		25.52	25.52	ON			
336.3	341.436	5.136			(1	ON		3.03	578.47	ON			
337.2	342.84	5.64	339.69	10.26		No	341.38	17.05	573.2	NO			
357.328	357.328		357.48		0.22	Yes		0	1.4	YES			
351.106	351.106	0	351.11		0 0	Yes		0	0 4	YES			
419.952	443.952	7	420.55		9.19	No		0.37	15.14	ON			
414.319	417.319	n c	417.96	0.24	y. c	Yes	41/.99	0.36	15.3/	YES	418.03	O.U.D.D	
0	0	0	0		0	ON ON		0	0	ON			
399.285	404.285		400.04	0.2	10.78	N		0.35	18.82	ON		0.01	
451.16	451.91					ON		0	90.6	NO			
417.67	422.42	4.75	418.22	10.59	10.59	No	418.41	18.53	18.53	NO	418.68	1.43	

Proposed Condition Junctions Results Summary Table

imensions	S				2-year			1	10-year			1	100-ye
				Max.	Мах.		Max	Max.	Max.				
+10,0	O.		Max.	Lateral	Total		. מאַ	Lateral	Total		No.	Icro+c I vcM	Z
וועפור		Depth	HGL	Inflow	Inflow	Surcharging	101	Inflow	Inflow	Surcharging	(100 ::eer)	Iviax. Lateral	ואומ
(foot)	(foot)	(feet)	(2-year)	(2-	(2-	(2-year)	-01)		(10-	(10-year)	(100-year)	(100 (100 kg)	1100,
(1991)	(lear)		(feet)	year) (cfs)	year) (cfs)		(feet)	year) (cfs)	year) (cfs)		(1991)	(T00-)ear) (CI3)	-001)
394.708	402.658	7.95	398.69			ON	400.68	0.49	463.12	ON	401.65	0.026	
398.472	403.472	5	400.9	2.31	2.31	ON	402.18	3.85	3.85	ON	403.27	0.227	
412.093	416.593	4.5	413.17	3.55	23.04	No	415.21	6.18	38.62	ON	417.34	0.365	
413.654	418.154	4.5	414.39	6:59	6:29	No	415.56	11.43	11.45	ON	418.43	0.7	
402.25	406.25	4	403.91	0.94	0.94	No	405.59	1.5	1.5	ON	406.46	0.076	
400.607	405.607	2	403.91	8.43	9.4	No	405.57	14.25	15.8	NO	406.44	0.88	
0	0	0	0	0	0	No	0	0	0	NO	0	0	
400.821	405.821	2	403.89	5.84	5.84	No	405.52	69.6	11.78	NO	406.53	0.566	
403.359	407.859	4.5	408.53	22.64	22.64	Yes	408.65	39.86	39.86	YES	408.75	5.03	
403.209	407.709	4.5	404.2	7.58	7.58	No	407.57	12.81	13.12	NO	407.83	0.814	
414.978	420.478	5.5	415.66	9.24	12	No	415.92	16.62	21.97	NO	416.32	1.13	
412.957	418.457	5.5	413.81	2.99	15.52	No	414.16	5.38	28.51	ON	414.87	0.372	
406.412	411.412	2	407.33	5.5	20.81	No	408.03	9.26	36.48	NO	410.14	0.55	
405.405	409.905	4.5	406.05	1.47	1.47	No	407.53	2.4	2.4	NO	410.93	0.129	
410.082	414.582	4.5	410.63	1.33	1.33	No	411.41	2.21	2.21	NO	415.2	0.118	
415.434	419.934	4.5	416.03	4.58	4.59	No	416.26	7.89	7.93	NO	419.62	0.5	
413.722	417.722	4	414.83	14.86	15.12	No	415.49	26.35	26.89	NO	417.95	2.43	
0	0	0	0	0	0	No	0	0	0	NO	0	0	
405.18	409.214	4.034	407.57	3.34	193.73	No	408.78	5.58	297.8	ON	409.41	0.314	
404.78	410.315	5.535	406.6	0.95	54.34	No	408.16	1.54	61.79	NO	408.9	0.077	
406.82	411.683	4.863	410.43	4.15	191.95	No	411.63	7.02	280.59	NO	411.76	0.407	
410	415.479	5.479	413.31	0.78	125.87	No	415.59	1.25	183.52	YES	416.73	0.058	
410.867	416.867	9	413.24	1.23	68.82	No	415.68	2.04	92.61	NO	416.74	0.112	
412.032	416.282	4.25	413.16	0.57	0.88	No	415.41	0.94	0.94	NO	416.49	0.054	

G. Costs and Prioritization

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\$185,704	\$93,124	\$92,580	3.00	36	\$39,831	\$18,731	\$21,100	3.00	36	\$94,538	533
\$171,775	\$86,075	\$85,700	2.00	24	\$36,660	\$17,160	\$19,500	2.00	24	\$87,326	100
\$143,519	\$64,849	\$78,670	1.00	12	\$29,360	\$12,810	\$16,550	1.00	12	\$72,162	317
\$136,850	\$58,982	\$77,868	0.92	11	\$27,994	\$11,652	\$16,342	0.92	11	\$68,808	394
\$130,181	\$53,114	\$77,067	0.83	10	\$26,626	\$10,493	\$16,133	0.83	10	\$65,453	470
\$123,512	\$47,247	\$76,265	0.75	6	\$25,260	\$9,335	\$15,925	0.75	6	\$62,100	547
\$116,843	\$41,380	\$75,463	29.0	æ	\$23,894	\$8,177	\$15,717	0.67	8	\$58,746	524
\$110,174	\$35,512	\$74,662	0.58	7	\$22,527	\$7,019	\$15,508	0.58	7	\$55,391	200
\$103,505	\$29,645	\$73,860	0.50	9	\$21,161	\$5,861	\$15,300	0.50	9	\$52,037	777
\$90,496	\$27,996	\$62,500	0.42	5	\$18,254	\$5,474	\$12,780	0.42	5	\$45,339	914
\$76,707	\$14,337	\$62,370	0.33	4	\$15,654	\$2,924	\$12,730	0.33	4	\$38,552	20
\$58,448	\$9,828	\$48,620	0.25	3	\$11,790	\$1,970	\$9,820	0.25	3	\$29,287	17
\$53,564	\$6,344	\$47,220	0.17	2	\$10,889	\$1,269	\$9,620	0.17	2	\$26,892	72
\$53,454	\$6,344	\$47,110	0.08	1	\$10,819	\$1,269	\$9,550	0.08	_	\$26,807	72

\$\text{Small} | \text{\$10,881} \text{\$1,088} \text{\$1,088} \text{\$1,790} \text{\$2,527} \text{\$23,894} \text{\$25,260} \text{\$25,260} \text{\$25,790} \text{\$25

 Average
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cash value loss.

note. The \$/sqft is based on the square foot assigned

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		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
8 Storm Drain Pipe	\$ 336,563.91 \$	\$ 161,550.68 \$		498,114.58 \$ 1,173,106.71 \$		563,091.22 \$ 1,736,197.93	788266.8063
Storm Drain Pipe	\$ 39,452.18 \$	\$ 18,937.04 \$	\$ 58,389.22 \$	\$ 1,173,106.71 \$		563,091.22 \$ 1,736,197.93	788266.8063
Storm Drain Pipe	\$ 7,139.19	\$ 3,426.81 \$		10,566.00 \$ 1,173,106.71 \$		563,091.22 \$ 1,736,197.93	788266.8063

		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
torm Drain Pipe	\$ 336,563.91	\$ 161,550.68	\$ 498,114.58 \$		1,173,106.71 \$ 563,091.22 \$ 1,736,197.93	\$ 1,736,197.93	788266.806
torm Drain Pipe	\$ 39,452.18 \$	\$ 18,937.04 \$	\$ 58,389.22 \$		1,173,106.71 \$ 563,091.22 \$ 1,736,197.93	\$ 1,736,197.93	788266.806
torm Drain Pipe	\$ 7,139.19 \$	\$ 3,426.81 \$	\$ 10,566.00 \$		1,173,106.71 \$ 563,091.22 \$ 1,736,197.93	\$ 1,736,197.93	788266.806

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Bundled FC Priority Score	Total Cost B	P&D Cost	Construction Cost P&D Cost	Cost_Total (Cost_Design	Construction Cost	Description
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				Asset and Project Costs	Asset a		

		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
nlet	\$ 13,775.00 \$	\$ 6,612.00	\$ 20,387.00 \$	\$ 1,173,106.71 \$		563,091.22 \$ 1,736,197.93	788266.8063
nlet	\$ 13,775.00 \$	\$ 6,612.00	\$ 20,387.00 \$	\$ 1,173,106.71 \$		563,091.22 \$ 1,736,197.93	788266.8063
nlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,173,106.71 \$		563,091.22 \$ 1,736,197.93	788266.8063

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		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Inlet	\$ 13,775.00 \$	\$ 6,612.00	\$ 20,387.00 \$		807,140.03 \$ 387,427.21 \$ 1,194,567.24	\$ 1,194,567.24	917990.7646
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 807,140.03 \$		387,427.21 \$ 1,194,567.24	917990.7646
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 807,140.03 \$	\$ 387,427.21	387,427.21 \$ 1,194,567.24	917990.7646

		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Inlet	\$ 13,775.00 \$	\$ 6,612.00	\$ 20,387.00 \$	\$ 807,140.03 \$		387,427.21 \$ 1,194,567.24	917990.7646
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Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 807,140.03 \$		387,427.21 \$ 1,194,567.24	917990.7646
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		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$		1,623,433.18 \$ 779,247.92 \$ 2,402,681.10	\$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13 775 00 ¢	\$ 661200 \$		01 387 00 \$ 1673 433 18 \$ 779 747 92 \$ 140 681 10	\$ 779,247,92	\$ 2402 68110	1215599 74

		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
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		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13,775.00 \$	\$ 6,612.00 \$	\$ 20,387.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Inlet	\$ 13.775.00 \$	\$ 6.612.00 \$	\$ 20.387.00 \$	\$ 1.623.433.18 \$		779.247.92 \$ 2.402.681.10	1215599.74

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			Asset a	Asset and Project Costs				
			Asset Costs			Pro	Project Costs	
	Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost P&D Cost	P&D Cost	Total Cost	Bundled FC Priority Score
J	Cleanout	\$ 11,600.00 \$	\$ 5,568.00	10	17,168.00 \$ 1,623,433.18 \$ 779,247.92 \$ 2,402,681.10	\$ 779,247.92	\$ 2,402,681.10	1215599.74
	Cleanout	\$ 11,600.00 \$	\$ 2,568.00		17,168.00 \$ 1,623,433.18 \$ 779,247.92 \$ 2,402,681.10	\$ 779,247.92	\$ 2,402,681.10	1215599.74

		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Cleanout	\$ 11,600.00 \$	\$ 2,568.00	\$ 17,168.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Cleanout	\$ 11,600.00	\$ 5,568.00	\$ 17,168.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74
Cleanout	\$ 11,600.00 \$	\$ 2,568.00 \$	\$ 17,168.00 \$	\$ 1,623,433.18 \$		779,247.92 \$ 2,402,681.10	1215599.74

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		Asset a	Asset and Project Costs				
		Asset Costs			Pre	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Storm Drain Pipe	\$ 51,405.68 \$	\$ 24,674.73 \$	\$ 76,080.41 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Storm Drain Pipe	\$ 315,160.81 \$	\$ 151,277.19 \$	\$ 466,438.00 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Storm Drain Pipe	\$ 248,807.98 \$	\$ 119,427.83 \$	\$ 368,235.81 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Storm Drain Pipe	\$ 135,423.37 \$	\$ 65,003.22 \$	\$ 200,426.59 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Storm Drain Pine	\$ 917878 \$	\$ 4 405 57 \$		13 583 85 \$ 6 774 455 26 \$ 3 251 738 52 \$ 10 026 193 78	\$ 3.251.738.52	\$ 10 026 193 78	6249534 222

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		Asset a	Asset and Project Costs				
		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
Cleanout	\$ 11,600.00 \$	\$ 2,568.00	\$ 17,168.00 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Cleanout	\$ 11,600.00 \$	\$ 2,568.00	\$ 17,168.00 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Cleanout	\$ 11,600.00 \$	\$ 2,568.00	\$ 17,168.00 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Cleanout	\$ 11,600.00 \$	\$ 2,568.00	\$ 17,168.00 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
Cleanout	\$ 11,600,00 \$	\$ 558.00		17 168 00 \$ 6774 455 76 \$ 3 251 738 52 \$ 10 026 193 78	\$ 3.251.738.52	\$ 10026 193 78	6249534 222

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Cleanout	\$ 11,600.00	\$ 5,568.00	\$ 17,168.00 \$		5.26 \$	3,251,738.52	6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	6249534.222
Cleanout	\$ 11,600.00	\$ 2,568.00	\$ 17,168.00 \$		5.26 \$	3,251,738.52	6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	6249534.222
Cleanout	\$ 11,600.00	\$ 2,568.00	\$ 17,168.00 \$		5.26 \$	3,251,738.52	6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	6249534.222
Cleanout	\$ 11,600.00	\$ 2,568.00	\$ 17,168.00 \$		5.26 \$	3,251,738.52	6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	6249534.222
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		Asset Costs			Pro	Project Costs	
Description	Construction Cost	Cost_Design	Cost_Total	Construction Cost2	P&D Cost	Total Cost	Bundled FC Priority Score
leanout	\$ 11,600.00	\$ 2,568.00	\$ 17,168.00 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
leanout	\$ 11,600.00 \$	\$ 5,568.00	\$ 17,168.00 \$		6,774,455.26 \$ 3,251,738.52 \$ 10,026,193.78	\$ 10,026,193.78	6249534.222
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CITY OF LEMON GROVE

CITY COUNCIL STAFF REPORT

Item No. 4

Meeting Date: February 18, 2020

Submitted to: Honorable Mayor and Members of the City Council

Department: City Manager's Office

Staff Contact: Mike James, Assistant City Manager / Public Works Director

mjames@lemongrove.ca.gov

Item Title: Lemon Grove Homelessness Partnership Plan

Recommended Action: That the City Council receives the report and provides direction to staff regarding the Lemon Grove Homelessness Partnership Plan.

Summary: The passage of Senate Bill 850 (SB 850) in July of 2018, provided \$18.8 million to the San Diego County region to provide immediate assistance to people experience homelessness. A portion of that total grant amount, equal to \$1.9 million, was allocated specifically to those partners that would increase the level of homeless services in the East San Diego County Region.

This staff report details what partnership activities have occurred in the City and what are some of the impacts to City workload. Lastly, staff seeks direction from the City Council regarding options to fund or consider moving forward. This plan is dynamic in that staff recommends that at least every six months it should be brought back to the City Council to evaluate its progress, funding thresholds, and progress. Staff recommends that during the next City Council goal setting workshop, staff returns with an update and further requests.

Background: The Homeless Emergency Aid Program (HEAP) authorized by Senate Bill 850 (SB 850) and signed into law on July 27, 2018, provided \$18.8 million of one-time block grant funds to be distributed by the San Diego Regional Task Force on the Homeless (RTFH) for distribution within San Diego County over a two-year period. The deadline to expend all grant funds is June 30, 2021. That funding intended to provide immediate emergency assistance to people experiencing homelessness or who are at imminent risk of homelessness within San Diego County.

On November 6, 2018, the Lemon Grove City Council adopted Resolution No. 2018-3617, which declared a shelter crisis in the City. This declaration was necessary to allow the

City's participation in an East San Diego County request for community based organizations to receive HEAP funds to fund homeless services. That Resolution of Support and Declaration was provided to the RTFH, which staff believes helped to strengthen the amount of funds that were allocated to the four (4) entities that committed to serving the East County Region. A summary of the partners that received funds to support East San Diego County is shown below.

Exhibit 1: HEAP Funded Partners

Entity	Sub recipients	Funds Received	Area of Focus
Crisis House	N/A	\$300,000	Outreach, Rapid Rehousing, Client Flex Funds
Family Health Centers of San Diego (FHCSD)	N/A	\$285,000	Housing Navigation, Client Flex Funds
Home Start – East County Collaboration	PATH	\$500,000	Street Outreach, Rapid Rehousing, Client Flex Funds, Youth (Prevention/Diversion, Outreach, Client Flex Funds, Youth Housing Navigation)
Home Start – East County Youth Homelessness Project		\$123,916	Prevention and Diversion, Outreach, Client Flex Funds, Youth Housing Navigation.
Salvation Army	211, Alpha Project, Home Start, Interfaith Shelter Network, The Center, VVSD, VCS	\$886,491	Prevention/Diversion, Client Flex Funds

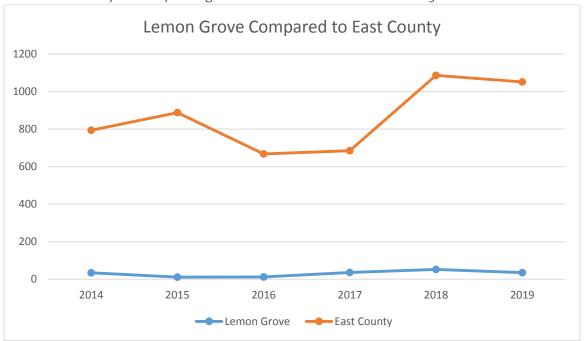
Collectively, there was \$1.9 million awarded to entities that committed to focus specifically on the East County Region in their application to the RTFH for HEAP Funds. These funds were allocated for the first year only, and there is no guarantee that the entities will continue to receive funding into the second year of the HEAP Grant Program. At this time, staff is still awaiting the financial update from the four (4) partners to determine if they will continue to support to Lemon Grove, as well as the East County Region's efforts, with homeless services.

Based on the Annual Point in Time Count (PIT), Exhibits 2 and 3, detail **the City's total** number of homeless individuals when compared to the East County and San Diego County as a whole.

Exhibit 2: Summary of PIT Count

Year	Lemon Grove Total	East County Total	County Total
2019	35	1,052	8,102
2018	52	1,087	8,576
2017	36	685	9,116
2016	12	668	8,692
2015	11	888	8,742
2014	34	794	8,506

Exhibit 3: Graph Comparing Lemon Grove and East County Counts



The pattern that the city has experience since 2014 is consistent with the overall East County and San Diego County trends especially during the 2017 and 2018 years.

At the time of the report, staff did not have the results from the 2020 Point in Time count that occurred on January 23, 2020. However, based on the 2019 count, 35 individuals surveyed were experiencing homelessness. Like past counts, each number is a snapshot of one morning's work with volunteers made up of both City and County residents. The primary reason for the count is help identify those that are experiencing homeless with a secondary goal to establish a measurable number in which future grant funds may be used to allocate amounts throughout the County.

Discussion: On September 27, 2019, staff met with three of the four partners outlined in Exhibit 1. From that meeting, staff learned that each partner awarded HEAP funds had a specific role in the East County region. While some of the tasks may overlap, each partner is focused on a different type service.

1. *Crisis House*: Based out of El Cajon, Crisis House focuses on urban homelessness while providing housing navigation, case management, expanded street outreach, meals, rapid rehousing, and client flexible assistance, which includes but not limited to application fees, moving deposits, and utility payments. Crisis House received \$300,000 of HEAP funds for Year 1: \$150,563.70 allocated for staff and operations, \$135,000 for rapid rehousing, and \$14,436.30 for flex client funds.

At the time this report was finalized a summary of **Crisis House's** activities in the City was not available.

- 2. Home Start East County Collaboration: Based out of San Diego, Home Start works closely with its sub recipient People Assisting the Homeless (PATH) who provides an Enhanced Outreach Team, together this partnership provides coordinated and targeted street based outreach to individuals experiencing homelessness in East County, including families, those with severe mental illness, and transitional age youth. Home Start also has a memorandum of understanding with Crisis House to provide outreach and rapid rehousing in the East County. HEAP funds are used for street outreach services, rapid rehousing assistance and client flexible assistance which includes but not limited to short term motel/hotel vouchers, transportation assistance, small amounts of food, rent, utilities, deposits, car repairs, one-time move in assistance, impound fees, application fees, prescription assistance, credit repair if credit issues are jeopardizing the housing or application process, and expungement through the Clean Slate Clinic. This project received \$500,000 of HEAP funds for Year 1: \$237,126 allocated for staff and operations, \$255,000 for rapid rehousing, and \$7,874 for flex client funds.
- 3. Home Start East County Youth Homelessness Project: Employs a youth housing navigator to provide housing prevention, diversion, housing navigation, and street outreach services. The program dedicated to unaccompanied minors and transitional age youth between the ages of 18 and 24 in East County, which includes Lemon Grove. Client flexible assistance includes short-term motel/hotel vouchers, transportation assistance, small amounts of food, rent, utilities, deposits, car repairs, one-time move in assistance, impound fees, application fees, prescription assistance, credit repair if credit issues are jeopardizing the housing or application process, and expungement through the Clean Slate Clinic. This project received \$123,916 of HEAP funds for Year 1: \$85,916 allocated for staff and operations, \$4,000 for prevention client funds, \$28,000 for diversion client funds, and \$6,000 for flex client funds.

Home Start has been very active in the City. Earlier this month staff received a summary of their activities, which is summarized below:

- Placed one household in permanent housing through rapid rehousing and is working with four other households.
- Outreach team has engaged with twenty-four (24) individuals and is providing ongoing case-management to six (6) of them.
- Distributed hygiene packs/socks to nineteen (19) people.
- Assisted twelve (12) people with obtaining free California Identification Cards.
- Provided additional referrals for services to ten (10) people.

Additionally, there are three specific examples that highlight the Home Start's successes in Lemon Grove.

- a. After receiving information from the City about a family living at the Lemon Grove Avenue Trolley Station, Home Start's outreach staff engaged with the family to develop trust and build rapport. They were able to enroll the household into its active outreach caseload and start working with them closely to connect them to resources. The outreach staff placed the household in a motel while they started working with Home Start's Rapid Rehousing Case Manager. After being entered into the Coordinated Entry System in two weeks, the family was matched to Home Start's Rapid Rehousing Program. The household faced many barriers during the housing search because of a lack of income and prior evictions. However, in less than a month Home Start was able to get the family approved for an apartment and they moved into their new permanent home shortly thereafter.
- b. During regular outreach in Lemon Grove, Home Start staff engaged with two transitional aged youth living in a car. The outreach staff developed rapport with the youth and enrolled them onto our active caseload. Both referred to Home Start's Youth System's Navigator and placed in a motel. Currently, both youth are searching for employment. In addition, the individuals received California Identification Cards, created resumes and are learning job-searching skills.
- c. Home Start outreach staff encountered a person at the park who was at risk of being evicted due to non-payment of rent. The person received a three-day notice to pay or quit from the property owner. The outreach staff immediately connected this **person to Home Start's Homelessness** Prevention Program. Through the program Home Start was able to pay the past due rent to prevent the client from being evicted. Home Start also provided additional case management to ensure the client had the knowledge and resources to avoid this situation in the future.

- 4. Salvation Army: Based out of El Cajon, the program focuses on prevention and diversion collaborations with a multitude of partners. This project received \$886,491 of HEAP funds for Year 1: \$161,491 allocated for staff and operations, \$494,375 for prevention client funds, and \$230,625 for diversion client funds. The partners that were listed in the HEAP Grant Application included:
 - a. 211 San Diego A free source of information to access community, health, social and disaster services by dialing 211. The call is free, confidential and available in more than 200 languages.
 - b. Alpha Project Focuses on assisting severe mental illness (SMI), terminally ill/end of life clients, including illness such as Cancer, Parkinson's, ALS etc.
 - c. *Home Start* Similar services previously described.
 - d. *Interfaith Shelter Network* Coordinating efforts of participating congregations, social service agencies and governmental programs to provide shelter and other resources to homeless individuals and families with the goal of moving them toward self-sufficiency.
 - e. San Diego LGBT Community Center (The Center) Provides assistance and services to the lesbian, gay, bisexual and transgender community and their families, and those living with or affected by HIV/AIDS.
 - f. Veterans Community Services Focus on helping military service members and veteran's transition successfully into civilian life. Committed to reducing the risks of homelessness, drug abuse, violence, and family disruptions that have accompanied inadequate transitional programs for wounded and disabled veterans in San Diego County.
 - g. Veterans Village of San Diego (VVSD) Committed to leaving no one behind, VVSD is focused on serving homeless military veteran's within San Diego County with housing, homeless court, employment & training, rehabilitation and mental health services.
 - h. A Way Back Home A reunification program that has been very successful in El Cajon, by reuniting individuals experiencing homelessness with their family that are living outside of California.

At the time this report was finalized, a summary of Salvation Army's activities in the City was not available.

The partner that staff did not meet with in September was Family Health Center of San Diego (FHCSD). At the time that staff met with the other three providers, staff was not aware that there was a fourth partner who had agreed to support the East County. It was not until December 2020, when staff asked the RTFH for a list of all East County Service Providers did it realize there was another homeless outreach/service partner that would serve the City. The details of what the FHCSD provides are listed below.

Family Health Centers of San Diego (FHCSD): Focus on housing navigation services for individual adults and families, especially the chronically homeless suffering from mental health issues, substance use disorder, and/or chronic medical concerns (e.g. HIV+ HCV, diabetes) in East and South County.

The health needs population will benefit from housing navigation, cross referrals to other housing services such as prevention and diversion, and access to FHCSD - provided wraparound services including primary and dental health, substance abuse and mental health counseling, benefits assistance, and intensive case management, trauma informed care, and other evidence based practice interventions as appropriate to the client's specific situation, needs, and personal values and goals.

Satellite Resource Centers (SRC) and Housing Navigators (HN) will support the expansion of coordinated, timely, and impactful housing navigation services leading to housing placement, beyond what is currently available in San Diego, through the establishment of two (2) SRC's in areas of highest need and near two FHCSD clinic sites. In addition to the primary goal of obtaining housing, HN's will promote quality of life and self-sufficiency by assessing client needs for other supportive services on an ongoing basis, providing assisted and unassisted referrals, and helping schedule and attending appointments (as requested by the client) for medical, dental, mental health, SAT, vocational training, legal, and other services.

This project received \$285,000 of HEAP funds for Year 1: \$212,365 allocated for staff and operations and \$72,635 for flex client funds.

Since meeting with the partners in September, staff has primarily worked with Home Start's case manager during field responses. Using the example from the Home Start discussion on pages 4-5 of this report, staff contacts a Homeless Outreach Specialist who will respond in the field by contact families or individuals experiencing homeless. That differs from the services that Crisis House provides, because Crisis House focuses on established service locations where homeless individuals frequent to receive some form of service, food, clothing or shelter. In either instance, Home Start continues to serve as the City's primary point of contact. Any follow up referrals, from Home Start to the other three partners or vice versa, occurs automatically based on the type of service needed.

Lastly, staff is also aware of the presence of the Interfaith Shelter Network, which is heavily supported by the Lemon Grove faith based community, that provides assistance to those experiencing homelessness in the City. While not coordinated by the City, staff understands that food pantries, providing clothing, supporting a rotational winter shelter, and mobile showers are available in the City.

With the presence of these partners, staff has still seen an increase for City resources that are required to mitigate the homeless encampments, as well as respond to calls for service from the businesses and residents. The next section details the impacts that the City manages as they directly relate to Public Works, Sheriff's Department and Fire Department activities.

Impacts to the City Services: The majority of the homeless calls for service emanate from the businesses, residents and guests in the City. On average, the Public Works Department receives five (5) calls per week regarding requests that are directly related to homelessness (e.g. camps, illegal dumping, shopping carts, and debris in the right-of-way, blocking the right-of-way, or creating a disturbance in public). While some of the calls are relayed to the Sheriff's Department to respond, and vacate the individuals from the area; there are those calls that involve camps on private property, camps and debris near the underpasses of State Route 94 and 125 or in San Diego MTS right-of-way, and camps in vacant lots, shopping carts and debris in open channel creeks in the City.

In most cases, a two-person Public Works field team will respond to manage the call for service. However, in instances when a homeless encampment is found to be in the public right-of-way, it requires a significant amount of work to remove the camp. Typically, the steps include posting a public notice at the camp notifying of the date and time of the cleaning, coordinating with the Sheriff's Department for assistance, mobilization of Public Works heavy equipment, wearing the property personnel protective equipment during the work, delivery of an EDCO provided dumpster(s), and the presence of the majority of the Public Works field team which often exceeds 3-5 people for at least four (4) hours. In order to provide a cost estimate to clear a small camp Exhibit 4 was created to show the fiscal impact. Keep in the mind that this estimate does not account for administrative staff time to coordinate the clean up because that role can vary from Front Counter Personnel to Department Directors, the cost for Sheriff's presence since they are patrol deputies on duty at the time, nor the cost for the dumpster because it is provided by EDCO.

Exhibit 4: Three Employees for a Four-Hour Camp Clean Up

Description	Fully Burdened	Quantity	Number of	Total
	Cost Per Hour		Hours	Cost
Supervisor	\$54	1	4	\$216
Tech II	\$42	1	4	\$168

Tech I	\$28	1	4	\$112
Vehicles/Equipment	\$65	3	4	\$780
Total Cost				\$1,276

Staff currently responds to a minimum of three (3) larger encampment clean-ups per quarter. Taking into account the information in Exhibit 4 staff estimates a total annual cost of \$15,312, to respond and clean up smaller homeless encampments. The other service area impacted by homelessness is public safety. A summary of homeless relate activities related to the Sheriff's and Fire Department summarized is shown below.

Sheriff's Department: Since 2017, the Sheriff's Department has seen a noticeable increase in the number of homeless related contacts occurring in the City. Exhibit 5 shows the history of only those contacts that resulted in a crime or arrest report.

Exhibit 5: Transient Related Crimes (by type) Per Year (Jan. 2015 through Feb. 2020)

	()))	· /				
Crime Type	2015	2016	2017	2018	2019	2020
Property						
Larceny Theft	1		20	28	41	5
Non-Residential Burglary			1	1	2	
Residential Burglary			1	1	1	1
Theft From a Vehicle				2	2	
Vehicle Theft				4	7	
Property						
Assault	3			9	11	5
Rape				1		
Robbery				6	8	
Total	4	0	22	52	72	11

The **Sheriff's Department began to focus more on** recording incidents that involve homeless individuals because the City began to receive more calls for service and City staff began attending local and regional homeless meetings to learn more about what are some solutions available. Based on the direction from the **City, the Sheriff's Department began** to log all cases/crimes that involved homeless individuals. Some additional observations include:

- Calls for service involving homelessness has increased over time.
- An estimated 90% or more of the homeless calls for service involve a mental illness, being under the influence of alcohol, drugs or both.
- There is no methodology in place that tracks daily radio calls for homelessness, however, general observation concludes that those calls have increased over time.
 That conclusion supported by a trend that is very clear when looking at Exhibit 5, there are increasing incidents occurring annually since 2017. If the current trend

continues in 2020, the estimated number of incidents may increase to as high as 88.

It is very apparent that the Sheriff's Department must be involved in the solutions that the City considers moving forward but it should not be sole solution to solve homelessness. Often times, the calls for service that require the Sheriff's Department to respond are related to homeless individuals committing a crime, being under the influence of drugs or alcohol, trespassing on to private property, or causing disturbance in the public. During each of the examples, our Sheriff's Department responds, tries to provide information about services that are available nearby, but those offers are often rejected, hence there is no other recourse for the Sheriff's Department to take when a crime is not committed, because being homeless in and of itself is not a crime.

It is important to note that there have been legal changes, which influenced the Sheriff Department's ability to respond to residents calls for services that involve homelessness. The most notable occurring in December 2019, when the United States Supreme Court denied a petition by the City of Boise to review the case Martin v. Boise. This left in place by an earlier ruling of the 9th Circuit that homeless persons cannot be punished for sleeping outside on public property in the absence of adequate alternative shelter. That means if there were no options of sleeping indoors, the City could not criminalize homeless people for sleeping outdoors or on public property. This directly affects the City because there are no homeless shelters within City limits; therefore, there are no alternative shelters, and ultimately cannot be a citable action. However, there are two distinct circumstances when the City may cite individuals that may or may not be homeless. First, per Lemon Grove Municipal Code 12.20.050 states in part, "It is unlawful to remain upon the grounds of any city park, or any part thereof, except between the hours of dawn to dusk." This applies to all individuals and is mutually exclusive of their housing status. Second, 647(C) of the California Penal Code, states, "every person who willfully and maliciously obstructs the free movement of any person on any street, sidewalk or other public place or on or in any place open to the public is guilty of a misdemeanor." This situation may occur when a camp blocks a sidewalk and force pedestrians to walk into the street or on to private property.

Fire Department: The Fire Department began the same tracking process for their calls for service as they relate to homeless individuals beginning in 2017. In Exhibit 6, a summary of homeless calls for service summarizes the total calls for service and homeless calls for service.

Exhibit 6: Fire Department Call For Service Comparison

Fire Engine	2017	2018	2019	Total
Homelessness Calls For Service	128	259	167	554
Percentage of Total Calls	5%	6%	4%	5% (average)
# of Total Calls	2,236	4,163	4,054	10,453

The percentage of total calls related to homelessness has remained relatively constant when compared to the total number of calls for service.

<u>Options Moving Forward</u>: Understanding the fiscal impacts that the City currently has, there are no available discretionary funds available to support the Homelessness Partnership Plan. However, staff included the following options for the City Council to discuss and provide feedback to staff. If the City Council wishes to pursue some of these options staff will return with options to reducing funding to other programs in order to fund these options.

Option #1: Continue to Participate in the ECHTF. Staff recommends continuing to participate in the meetings with the East County Homeless Task Force (ECHTF), which operates under the East County Chamber of Commerce, to share information and participate in regional discussions. As a reminder, the ECHTF requested that the City participate in a \$33,100 annual cost-sharing model in 2017, which was before the HEAP funds were allocated. At that time, no items were selected for funding. Those items included:

1. <u>Hire an ECHTF Director</u>: This position will identify and prioritize key problem areas based on the 11 teams that are a part of the ECHTF.

Lemon Grove: \$5,000. Total Need: \$40,000.

2. Marketing Program:

Signage: Adopt the idea that there are better ways to support homeless individuals rather than giving directly to them. The sign has already been created and the City of El Cajon already posted them in frequently known homeless panhandling areas.

Lemon Grove: \$42 per sign. Total Need: Unknown.

3. *Posters*: Allow businesses to place posters in storefront windows that educate businesses and residents about the drawbacks to giving directly to panhandlers. The benefits of businesses participating is that the poster will not count towards the advertising space limitation.

Lemon Grove: \$0 (funded by the business community). Total Need: \$0

4. <u>Access to Services</u>: This is a new app solution for homeless individuals to access available services from their mobile phones. ConnectEC.org was produced by the East County Leadership Team and will work with text only or smart phones. Bracelets with numbers to text and cards for wallets will also be provided.

Lemon Grove: Unknown. Total Need: Unknown.

5. <u>Portable Showers</u>: For the east county region, the showers will be supported by the faith & service community. These showers will be used in conjunction with additional services for the homeless.

Lemon Grove: \$2,600. Total Need: \$26,000.

6. <u>Reunification Program</u>: East County Salvation Army supported program that will connect homeless with family members that are willing to accept them at their destination.

Lemon Grove: \$2,000 (\$500 per individual). Total Need: Unknown.

- 7. <u>Housing Navigator</u>: This request is to fund a housing navigator for Lemon Grove to assist with case work and to help with long term housing. It will be managed through Crisis House and will focus only on homeless individuals in Lemon Grove. Lemon Grove: \$7,500. Total Need: Unknown.
- 8. <u>Rental Assistance</u>: Request support for rental assistance for up to five homeless family's coordinated by Crisis House. This will assist families with the first three months of rent.

Lemon Grove: \$16,000. Total Need: Unknown.

Option #2: Continue to Partner with East County Cities and the County of San Diego. Since 2017, the East County Cities (El Cajon, La Mesa and Santee) and the County of San Diego have met to discussion various partnerships that would be beneficial to the entire East County Region. By collectively voicing the concerns specific to the East County Region, this partnership may result in the City receiving assistance, service or funding from the RTFH, the County, and the State of California.

Cost: \$0.

Option #3: Update the City's Website. The City Council directed staff to host a Homeless Services Workshop on November 20, 2019. One of the primary requests from the residents and business owners that attended was there is no readily accessible information available. Staff can create a webpage on the City's website that can share information about the City partners and the priorities for the City Council concerning homelessness within the City.

Cost: \$0.

Option #4: Offer Workspace for Home Start to Operate within City Hall. After having additional discussions with Home Start, City staff learned that they are interested in expanding on its current partnership to increase its presence in the City. City staff has reviewed the current workstation layout in City Hall and concluded the feasibility of adding an additional workstation in City Hall that can accommodate a Homeless Outreach Specialist from Home Start. City staff estimates that Home Start require minimal resources from the City. Staff can return to the City Council with a no-fee lease agreement with Home Start to occupy a workstation in City Hall.

Cost: \$0.

Option #5: Contract Clean Up Services to a Contractor. The estimated city staff cost to cleaning up homeless camps each year east equals \$15,000. There are third party companies that respond to illegal camp cleanup projects as well as monitor "hot spot" illegal camp locations. However, that cost will likely exceed what staff is currently estimating. The greatest benefit to exploring this option is enable the streets division employees to focus on other city priorities rather than responding to clean up homeless camps.

Cost: \$9,000 for one day/one encampment clean up (estimate provided in 2018).

Option #6: Explore Grants and Other Funds. When researching the programs that other San Diego County cities have implemented to assist with homelessness there are other funds that have been used in this manner as well as the possibility of new funds that may be allocated to the region. Those funds include:

- California State Budget FY 2020-2021 (\$1.4 billion of new money for homeless services and housing),
- Community Development Block Grant Fund,
- General Fund.
- Reserve Fund, and
- Regional Task Force on the Homeless (San Diego Continuum of Care).

If this is an option that the City Council would like to further explore it can return with options during the FY 2020-2021 budget process.

Cost: Unknown.

Option #7: Contract with Home Start for an Outreach Specialist. A full time Outreach Specialist would work exclusively in Lemon Grove and would be the most responsive tool to address homelessness in the City. Under the current model, Home Start staff is allocated to the entire East County Region. A dedicated Outreach Specialist could consistently and intensively work with people experiencing homelessness in Lemon Grove while also leveraging all of our other resources to connect those in need with housing and support services.

Cost: \$80,000 per year.

Conclusion: The single greatest reason why the staff is not recommending a more robust partnership at this time is lack of unallocated discretionary funds to pay for services or staffing. Without additional funds, the only two ways to support these options are to use the General Reserve Fund or reallocated funds from other City services. For example, Community Development Block Grant funds may be used to fund homeless services, however, that would reduce the amount of funds available for street rehabilitation.

Staff seeks feedback from the City Council on which of the options presented the City Council would like staff to pursue or not. Additionally, if there are other activities that the City Council desires, staff could incorporate that analysis into the annual goal-setting workshop for further discussion.

Environmental Review:	
Not subject to review	☐ Negative Declaration
Categorical Exemption, Section	☐ Mitigated Negative Declaration
Fiscal Impact: There is no direct fiscal impacted feedback from the City Council, staff will return of each option selected for implementation.	
Public Notification: None.	
Staff Recommendation: That the City direction to staff regarding the Lemon Grove H	•
Attachments: None.	



CITY OF LEMON GROVE

CITY COUNCIL STAFF REPORT

Item No. 5

Meeting Date: February 18, 2020

Submitted to: Honorable Mayor and Members of the City Council

Department: City Manager's Office

Staff Contact: Lydia Romero, City Manager

Rod Greek, Interim Admin Services Director

lromero@lemongrove.ca.gov and rgreek@lemongrove.ca.go

Item Title: Fiscal Year 2019-20 Mid-Year Budget Update

Recommended Action:

Adopt a resolution (Attachment C) approving the Fiscal Year 2019-20 City of Lemon Grove Mid-Year Budget

Adopt a resolution (Attachment D) approving the Fiscal Year 2019-20 Appropriations Limit.

Authorize the transfer of \$804,924 from the FY 18-19 Fund balance to the City's 115 Trust for investment towards future CalPERS obligations.

Summary:

On June 18, 2019, the City Council adopted the Fiscal Year 2019-20 Lemon Grove Consolidated Operating and Capital Budget. In keeping with best financial practices, mid-way through the fiscal year the City Council shall adjust the adopted budget to reflect revised revenue and expenditure projections, and the results of the prior year financial audit. Besides improving the accuracy of the approved budget, this procedure is designed to provide the City Council and the public with a review of City's financial health.

Discussion:

Proposed mid-year adjustments are included for budget line items that are projected to be over/under the original adopted budget by at least \$5,000 or represent new line items that were not previously in the budget.

General Fund:

The following table compares a summary of the adopted FY 2019-2020 General Fund Budget with the proposed mid-year adjustments.

	FY 2019-2020			
	Adopted	Proposed		
General Fund				
Balance Forward	\$ 6,280,923	\$ 6,280,923		
Revenue	14,054,324	14,506,228		
Expenditures	(14,606,428)	(14,832,428)		
Reserve Revenue	-	-		
Transfers	126,072	107,302		
Ending Balance	\$ 5,854,891	\$ 6,062,025		

The following discussion of mid-year adjustments will present the adjustments in terms of their net impact on the budget, rather than what the new total for each specific line item or account will be.

Staff recommends that General Fund revenues be increased in total by \$451,904. See attachment A for the detailed breakdown of adjustments. The main drivers are:

- Additional \$190,000 of Property Tax, due to rising property values.
- Additional \$186,904 due to a reimbursement from SDG&E for Lemon Grove Avenue Realignment costs incurred in FY2019.
- Additional \$68,000 in Permit Fees, due to increased activity.
- Additional \$28,000 of Rent Revenue as original projection did not include CPI adjustment.
- Reduction of (\$62,000) Passport processing fees as there is lower activity than anticipated.
- Reduction of \$(20,000) in Administrative Citations as anticipated proceeds from a settlement were shifted to FY2019 from FY2020.

Transfer activity is reflected in the budget book at the end of the revenue section. This section of the budget includes any inter-fund transfer to or from the General Fund. The proposed mid-year transfer adjustment is in attachment A, and has to do with the Successor Agency for the Redevelopment Authority. Staff recommends that General Fund transfers be decreased by \$18,770 for Administrative costs related to the 2019 A&B Bonds which were issued to redeem the outstanding 2007 and 2010 bonds. These costs were expensed directly to the Successor Agency rather than to the general fund as originally budgeted.

Staff recommends that General Fund expenditures be increased by \$216,000. See attachment A for details on each line item included in the adjustment. The most significant changes are:

• Increase of \$150,000 in Fire JPA costs due to reorganization of Heartland Fire & Rescue Joint Powers Authority.

- Increase of \$33,000 in Public Works for emergency repairs on vehicles, HVAC, lighting and plumbing; and for additional workload related to storm response, dropbox, and opening/closing of public facilities.
- Increase of \$28,000 for election costs.
- Increase of \$10,000 for costs related to FLSA litigation, investigations and a CalPERS audit.
- Increase of \$5,000 for SANDAG membership dues.

After the proposed mid-year budget adjustments, total General Fund resources total \$14,613,530, while total General Fund expenditures total \$14,832,428. Estimated expenditures exceed estimated resources by \$218,898, which means the General Fund is still expected to end the fiscal year in a deficit. The original budget had projected a \$426,032 deficit. We've made every effort to hold positions vacant, trim costs where absolutely necessary. The increases we are requesting are necessary to continue to provide minimum service levels to the community. Fortunately we were able to offset the increase in costs with projected increases in revenue which is closing the gap in our original budget deficit.

This is an indicator that the City's long-term structural deficit is continuing. The City has implemented cost cutting measures by underfunding needs on the expenditure side. Deferring investment in capital replacement and staff is not a long-term solution. In addition, general economic projections show a recession or slow-down coming in the next few years. Therefore, the City needs to continue to prioritize generating new sources of revenue.

FY18/19 General Fund Surplus

The General Fund ended FY18-19 with a surplus of \$804,924. In accordance with the City's adopted General Reserve Policy, half is required to be transferred to reserves and the other half is to be used for one-time expenditures per direction from the City Council. In December 2019, Council directed staff to investment the entire surplus of \$804,924 in the City's 115 Pension Trust. Council's direction is consistent with the existing general reserve policy as the 115 trust is a reserve account.

As a reminder, investing the cash in a 115 Trust, rather than in an extra payment directly to CalPERS or keeping the funds in the District's and City's pooled cash investments, maintains local control of the investment while providing the opportunity for investment in options that have the potential to generate higher interest earnings. The District's initial deposit into the 115 Trust was made in October 2018. Over the last year (Oct 2018 – Oct 2019), the 115 Trust has returned net interest earnings of 9.3%.

General Fund Current Year Finance Report:

Since the General Fund has been the focal point of the City's on-going financial worries, staff thought it was important to provide the City Council and general public with additional financial reporting on a regular basis. Attachment C is review of the General Fund revenue and expenditure activity between July 1, 2019 and December 31, 2019 and a comparison to the prior year's activity. Once the proposed mid-year budget is adopted, the budget column on the report will be updated. Staff will provide this report to Council on a quarterly basis.

Other Funds

In addition to the General Fund, a few of the other funds have line items that are projected to be more than \$5,000 different than the original budget.

Supplemental Law Enforcement Services Fund (07)

The City received an additional payment from the County beyond the contracted \$100,000 annual amount.

Transportation Development Act (TDA) (10)

The original budget will be decreased for a reimbursement amount for FY2019 due to actual costs coming in lower than anticipated and a reduction in cost estimates for allowable street repair expenditures. These changes result in a \$10,000 decrease to the fund balance.

Sanitation District: Operating (15)

Received refund of \$550,899 from City of San Diego Metro JPA for annual expense reconciliation. This reduces our annual expenditure budget for Metro Capacity and Treatment by the same amount. Funds were placed in the 115 Trust per direction from District Board in December 2019.

Sanitation District: Capital (16)

Continued Rehabilitation of sewer mains is resulting in an increase of \$270,000 in expenditures for this fund.

Appropriations Limit

As mentioned during the discussion of the Annual Financial Report for FY18-19 at the December 17, 2019, City Council meeting, the audit found that last year's adopted Appropriations Limit (or Gann Limit) was understated by \$240. Each year's limit is calculated from the prior year's limit, therefore, the FY19-20 Appropriations Limit Council adopted in June 2019 is also incorrect. Attachment E is the amended FY20 Appropriation Limit to adopt based on the corrected calculation.

Environmental Review:	
Not subject to review	☐ Negative Declaration
☐ Categorical Exemption, Section	☐ Mitigated Negative Declaration
Fiscal Impact:	
Approving the Mid-Year Budget update	authorizes expenditures within those budget
limits.	
Public Notification:	
None.	
Staff Recommendation:	
Adopt a resolution approving the Fiscal Y	Year 2019-20 City of Lemon Grove Mid-Year
Budget;	
Adopt a resolution approving the revised F	iscal Year 2019-20 Appropriations Limit.

Authorize the transfer of \$804,924 from the General Fund to the City's 115 Trust for

Attachments:

Attachment A – Proposed FY2019-20 Budget Adjustments

investment towards future CalPERS obligations.

 $Attachment \ B-July \ 1, \ 2019-December \ 31, \ 2019 \ Finance \ Report$

 $Attachment \ C-Resolution \ Approving \ FY 2019-20 \ Lemon \ Grove \ Budget$

 $Attachment\ D-Resolution\ Approving\ FY 2019-20\ Appropriations\ Limit$

City of Lemon Grove FY 2019-2020 Budget Adjustments

Exhibit 1 of Budget Resolution

General Fund

Adopted Budget \$ 6,280,923

REVENUE

Description	Adjustment	Reason
Property Tax Secured and Unsecured	190,000	Higher growth than anticipated
Rent Revenue - Long Term	28,000	Original projection didn't include CPI adjustment
Fire Plan Review & Inspection	5,000	More activity than projected
Fire Cost Recovery	24,000	More activity than projected
Building Permits	40,000	More activity than projected
Planning Permits	20,000	More activity than projected
Engineering Permits	8,000	More activity than projected
Passport Processing Fees	(62,000)	Less activity than projected
Cost Recovery	186,904	Reimbursement from SDG&E for LG Realignment costs incorred in FY19
Other Revenues	12,000	Received reimbursement for staff time on Successor Agency Bond Refunding
Administrative Citations	(20,000)	Proceeds from settlement with property owner counted as FY19 revenue
Interest Revenue - LAIF	20,000	Interest rates staying slightly higher than estimated
Increase in Revenue	451,904	

TRANSFERS

Description	Adjustment	Reason
Interfund Transfer - Successor Agency	(18,770) Paid some admin costs directly from Fund 60
Decrease in Transfers	(18,770	

EXPENDITURES

Description	Adjustment	Reason	
City Council	_		
Membership and Dues	5,000	SANDAG Dues increased \$4,535 from FY19	
Human Resources	_		
Professional Services	10,000	Costs related to FLSA litigation, investigations and a CalPERS audit	
Fire			
Fire			
Quarterly JPA Reconcilation	150,000	Costs related to reorganization	
Public Works			
Repair & Maintenance - Vehicles		Emergency repairs on aging fleet	
Overtime - Public Works	10,000	Additional work required due to storms, dropbox and opening/closing facilities	
Lighting Maintenance	8,000	Emergency parking lot lights for recreation center	
Repair and Maintenance - Facilities	10,000	Emergency HVAC, lighting and plumbing repairs	
Non-Departmental			
Election Costs		LG specific measure added to March ballot	
Increase in Expenditures	226,000		
·			
Original Revenue	14,054,324	-	
Increase in Revenue	451,904		
Original Transfers	126,072	_	
Decrease in Transfers	(18,770)		
Original Expenditures	(14,606,428)	<u> </u>	
Increase in Expenditures	(226,000)	<u></u>	
Increase in Reserve Revenue	-	=	
Revised Budget	\$ 6,062,025		

Supplemental Law Enforcement Services Fund

Beginning Fund Balance \$ 37,462

REVENUE

Description	Adjustment	Reason
Supplemental Law Enforcement Services	55,948	Received additional payment
		_
Original Revenue	100,000	_
Increase in Revenue	55,948	_
Original Expenditures	(130,000)	
Ending Fund Balance	\$ 63,410	_

Transportation Development Act (TDA)

Beginning Fund Balance \$ (12,349)

REVENUE

Description	Adjustment Reason
Revenue - TDA	(30,794) Reimbursement for FY19 based on actuals

EXPENDITURE

Ending Fund Balance

LAPLINDITORL	
Description	Adjustment Reason
Street Repairs	(21,000) Outside of allowable TDA expenditures
Original Revenue	121,220
Decrease in Revenue	(30,794)
Original Expenditures	(142,494)
Decrease in Expenditures	21,000

\$ (64,417)

Sanitation District: Operating

Beginning Fund Balance \$ 9,056,502

EXPENSE

Description	Adjustment	Reason
Metro Annual Capacity & Treatment	(550,899)	METRO JPA Annual Reconciliation refund
Original Revenue	8,411,389	
Original Expenditures	(8,830,008)	
Decrease in Expenditures	550,899	
Ending Fund Balance	\$ 9,188,782	
-		

Sanitation District: Capital

Beginning Fund Balance \$ 10,363,583

EXPENSE

EXPERSE		
Description	Adjustment	Reason
FY 17-18 Sewer Main Rehab - Construction	270,000	Projected in FY19, but work continued into FY20
Original Revenue	1,545,000	-
Original Expenditures	(2,356,495)	-
Increase in Expenditures	(270,000)	-
Ending Fund Balance	\$ 9.282.088	

As of Dec 31, 2019 ATTACHMENT B

General Fund Revenue & Expenditure

*Expect total % expended to be approximately 50%

Revenue	Budget	YTD	% Collected	PY YTD	Variance
Sales Tax	5,547,721.00	2,064,967.60	37%	2,435,685.10	-15%
Property Tax	2,716,430.00	1,133,792.32	42%	1,020,437.59	11%
Property Tax In Lieu	2,742,418.00	-	0%	-	#DIV/0!
Franchise Fees	1,070,100.00	307,855.54	29%	318,106.53	-3%
Building Permits	250,000.00	228,639.95	91%	228,196.60	0%
Other Rev	2,036,031.00	1,150,534.35	57%	1,091,275.75	5%
TOTAL REV	\$ 14.362.700.00	\$ 4.885.789.76	34%	\$ 5.093.701.57	-4%

GF Revenue		
	\$4.9M	
\$0M		\$14.4M

Expenditures	Budget	YTD	% Expended	PY YTD	Variance
City Council	115,186.00	61,306.65	53%	40,081.38	53%
City Manager	283,646.00	134,679.39	47%	127,331.34	6%
Human Resources	102,531.00	60,526.90	59%	45,435.54	33%
City Clerk	111,459.00	53,553.22	48%	32,060.71	67%
City Attorney	195,000.00	79,215.69	41%	92,946.23	-15%
Finance	388,663.00	196,049.73	50%	137,725.43	42%
Public Safety	6,590,770.00	2,168,535.68	33%	2,103,020.30	3%
Fire	4,547,556.00	2,512,805.56	55%	2,464,332.59	2%
Community Development	626,876.00	335,379.32	54%	330,888.99	1%
Public Works	1,580,741.00	807,538.31	51%	699,072.27	16%
Non-Departmental	64,000.00	6,493.50	10%	18,855.18	-66%
TOTAL EXP	\$ 14,606,428.00	\$ 6,416,083.95	44%	\$ 6,091,749.96	5%



Narrative:

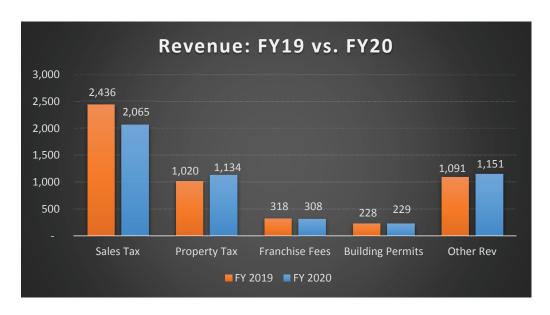
Above is a brief overview of the City's General Fund activity from July 1st through December 31st of the 2019-2020 fiscal year.

Highlights:

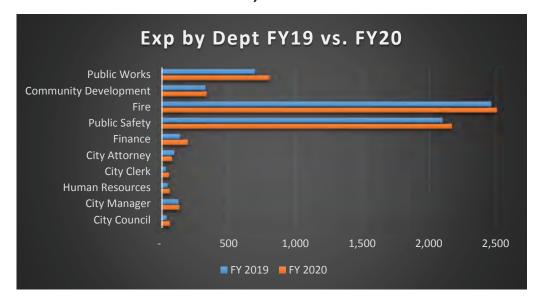
Sales tax revenue is lagging last year by 15% but is up an average of 2.9% over the past 2 fiscal years. The first few months of FY2019 were high due to systems issues at the State. Property tax revenue is up 11% halfway through the year. Other revenue is over 50% mainly due to receipt of the LG Realignment reimbursement. Building Permit activity is consistent with last fiscal year at this time reflecting consistent economic activity for Lemon Grove.

Halfway through the fiscal year expenditures should be around 50% of the budget. Overall, we are under that percentage (44%) mainly due to the Sheriff's Department being one month behind in their billing. Fire is at 55% expended mainly due to increased use of overtime to backfill for absences due to injuries.

Salaries and Benefits for the General Fund are about 3.4% over where we would expect them to be at mid-year. This is mainly due to Overtime in both Fire and Public Works, and Retirement across the board.

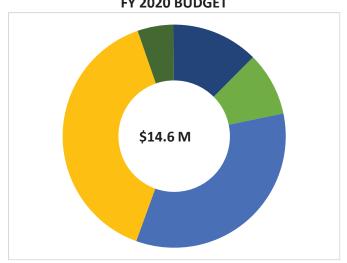


REVENUES AND EXPENDITURES
AS OF
DECEMBER 31, 2018 AND 2019



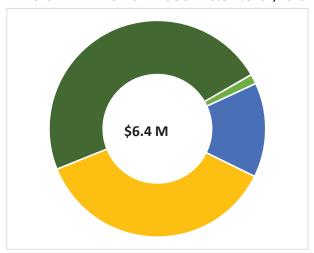
Department	FY 19/20 Budget	% of Total
Administration	1,260,485.00	9%
Public Safety	6,590,770.00	45%
Fire	4,547,556.00	31%
Community Development	626,876.00	4%
Public Works	1,580,741.00	11%
Total Budget	14,606,428.00	100.00%

FY 2020 BUDGET



Administration **Public Safety** Fire Community Development Public Works

FY 2020 EXPENDITURES THROUGH December 31, 2019



Capital Expenditures Op Supplies & Services **Contracted Services** Salaries & Benefits

RESOLUTION NO. 2020-

A RESOLUTION OF THE CITY COUNCIL OF THE CITY OF LEMON GROVE, CALIFORNIA, APPROVING THE CITY OF LEMON GROVE MID-YEAR BUDGET FOR FISCAL YEAR 2019-2020 AND AUTHORIZING EXPENDITURES THERETO

WHEREAS, on June 18, 2019 the City Council adopted Resolution No. 2019-3666 approving the Consolidated Budget for Fiscal Year 2019-20; and

WHEREAS, said Budget warrants revision to reflect new information regarding revenue and expenditure projections; and

WHEREAS, said Budget warrants revision to reflect actions taken by the City Council since its adoption that impact the Budget; and

WHEREAS, the City Council has reviewed the proposed revisions.

NOW, THEREFORE, BE IT RESOLVED that the City Council of the City of Lemon Grove, California, hereby

- 1. Approves the Lemon Grove Fiscal Year 2019-20 Mid-Year Budget (Exhibit 1); and
- 2. Authorizes expenditures thereto.

Attachment C

PASSED AND ADOPTED on B	February 18, 2020, t	he City Council of the City of
Lemon Grove, California, adopted Resol	lution No. 2020	, passed by the following
vote:		
AYES:		
NOES:		
ABSENT:		
ABSTAIN:		
	Raquel Vasquez	, Mayor
Attest:		
	_	
Shelley Chapel, MMC, City Clerk		
Approved as to Form:		
Kristen Steinke, City Attorney		

City of Lemon Grove FY 2019-2020 Budget Adjustments

Exhibit 1 of Budget Resolution

General Fund

Adopted Budget \$ 6,280,923

REVENUE

Description	Adjustment	Reason
Property Tax Secured and Unsecured	190,000	Higher growth than anticipated
Rent Revenue - Long Term	28,000	Original projection didn't include CPI adjustment
Fire Plan Review & Inspection	5,000	More activity than projected
Fire Cost Recovery	24,000	More activity than projected
Building Permits	40,000	More activity than projected
Planning Permits	20,000	More activity than projected
Engineering Permits	8,000	More activity than projected
Passport Processing Fees	(62,000)	Less activity than projected
Cost Recovery	186,904	Reimbursement from SDG&E for LG Realignment costs incurred in FY19
Other Revenues	12,000	Received reimbursement for staff time on Successor Agency Bond Refunding
Administrative Citations	(20,000)	Proceeds from settlement with property owner counted as FY19 revenue
Interest Revenue - LAIF	20,000	Interest rates staying slightly higher than estimated
Increase in Revenue	451,904	

TRANSFERS

Description	Adjustment	Reason
Interfund Transfer - Successor Agency	(18,770) Paid some admin costs directly from Fund 60
Decrease in Transfers	(18,770	

EXPENDITURES

Description	Adjustment	Reason
City Council	<u> </u>	
Membership and Dues	5,000	SANDAG Dues increased \$4,535 from FY19
Human Bassumas		
Human Resources		
Professional Services	10,000	Costs related to FLSA litigation, investigations and a CalPERS audit
Fire		
Quarterly JPA Reconcilation	150,000	Costs related to reorganization
Public Works		
Repair & Maintenance - Vehicles	5,000	Emergency repairs on aging fleet
Overtime - Public Works	10,000	Additional work required due to storms, dropbox and opening/closing facilities
Lighting Maintenance		Emergency parking lot lights for recreation center
Repair and Maintenance - Facilities	10,000	Emergency HVAC, lighting and plumbing repairs
Non-Departmental		
Election Costs	28,000	LG specific measure added to March ballot
Increase in Expenditures	226,000	
Original Revenue	14,054,324	-
Increase in Revenue	451,904	-
Original Transfers	126,072	-
Decrease in Transfers	(18,770)	_
Original Expenditures	(14,606,428)	
Increase in Expenditures	(226,000)	
Increase in Reserve Revenue		-
Revised Budget	\$ 6,062,025	=

Supplemental Law Enforcement Services Fund

Beginning Fund Balance \$ 37,462

REVENUE

Description	Adjustment	Reason
Supplemental Law Enforcement Services	55,948	Received additional payment
		_
Original Revenue	100,000	_
Increase in Revenue	55,948	_
Original Expenditures	(130,000	
Ending Fund Balance	\$ 63,410	_

Transportation Development Act (TDA)

Beginning Fund Balance \$ (12,349)

REVENUE

Description	Adjustment Reason
Revenue - TDA	(30,794) Reimbursement for FY19 based on actuals

EXPENDITURE

Ending Fund Balance

Description	Adjustment Reason
Street Repairs	(21,000) Outside of allowable TDA expenditures
Original Revenue	121,220
Decrease in Revenue	(30,794)
Original Expenditures	(142,494)
Decrease in Expenditures	21,000

\$ (64,417)

Sanitation District: Operating

Beginning Fund Balance \$ 9,056,502

EXPENSE

Description	Adjustment	Reason
Metro Annual Capacity & Treatment	(550,899)	METRO JPA Annual Reconciliation refund
Original Revenue	8,411,389	
Original Expenditures	(8,830,008)	•
Decrease in Expenditures	550,899	•
Ending Fund Balance	\$ 9,188,782	
-		

Sanitation District: Capital

Beginning Fund Balance \$ 10,363,583

EXPENSE

EXI ENGE	
Description	Adjustment Reason
FY 17-18 Sewer Main Rehab - Construction	270,000 Projected in FY19, but work continued into FY20
Original Revenue	1,545,000
Original Expenditures	(2,356,495)
Increase in Expenditures	(270,000)
Ending Fund Balance	\$ 9.282.088

RESOLUTION NO. 2020-

A RESOLUTION OF THE CITY COUNCIL OF THE CITY OF LEMON GROVE, CALIFORNIA, ESTABLISHING THE APPROPRIATIONS LIMIT FOR FISCAL YEAR 2019-2020

WHEREAS, on June 18, 2019 the City Council adopted Resolution No. 2019-3668 establishing the Appropriations Limit for Fiscal Year 2019-20; and

WHEREAS, each year's appropriation limit calculation begins with the prior fiscal year's appropriation limit; and

WHEREAS, each year the City hires an independent accountant to perform agreed-upon procedures applied to the Appropriations Limitation prescribed by Article XIIIB of the California Constitution to assist the City in meeting the requirements of Section 1.5 of Article XIIIB of the California Constitution; and

WHEREAS, during the independent accountant's review of the adopted fiscal year 2018-2019 Appropriations Limit, they found the limit to be understated by \$240; and

WHEREAS, the fiscal year 2019-2020 Appropriations Limit has been recalculated using the information from the State Department of Finance listed in Resolution No. 2019-3668 and the corrected FY2018-2019 limit; and

WHEREAS, the fiscal year 2019-2020 Appropriations Limit adopted by this Resolution supersedes the limit adopted by Resolution No. 2019-3668.

NOW, THEREFORE, BE IT RESOLVED that the City Council of the City of Lemon Grove, California, hereby establishes the Fiscal Year 2019-2020 Appropriations Limit at \$52,075,183.

Attachment D

PASSED AND ADOPTED on 1	February 18, 2020, the City Council of the City of
Lemon Grove, California, adopted Reso	lution No. 2020, passed by the following
vote:	
AYES:	
NOES:	
ABSENT:	
ABSTAIN:	
	Raquel Vasquez, Mayor
Attest:	
	
Shelley Chapel, MMC, City Clerk	
Approved as to Form:	
Kristen Steinke, City Attorney	